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INTERCOMPARISON OF GROUND-BASED AND SPACE SOLAR FLUX MEASUREMENTS

Contract No. NASW-2568

FINAL REPORT

For Period

1 April 1974 - 31 October 1974

Prepared for: NASA Headquarters, Washington, D. C. 20546

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I INTRODUCTION

Radiation from the sun falling on the carth's surface has recently become of significant interest in the potential solution of the world's energy needs.

Although the sun represents a relatively constant source of energy, the earth's atmosphere and dirunal rotation cause continuous changes in the energy reaching the earth's surface. This research is aimed primarily at performing detailed temporal measurements of the solar flux at one location. These data are then analyzed and compared to the potential of space measurements which allow one to consider the flux falling on areas of the earth.

The most important result of the research is that the temporal charcteristics of the flux in the presence of a real atmosphere would be difficult to obtain from space and that the variations in the flux can be highly significant in regard to most solar conversion schemes.

The detailed results of the research are presented in the following section. We discuss the instruments developed to separate the direct and scattered solar flux, the computer analysis methods developed, and the results of the research, presented as both graphical and tabular data.

II TECHNICAL RESULTS

1. Introduction

In this research, we have used several instruments and analysis methods to measure the solar flux on a daily continuous basis. The basic aim of the research was to measure the temporal dependence of the direct flux and the scattered flux.

There are several instruments available today which have been designed specifically for solar insolation measurements. The line of instruments offered by Eppley Laboratories in Newport, Rhode Island, is perhaps representative of the current state-of-the-art in commercial scientific instruments. The National Weather Service has used these instruments for many years to gather data over a network of approximately 80 stations in the United States. At the NOAA/NSF Workshop on Solar Insolation, held at Silver Spring, Maryland in November 1973, there was a strong consensus of opinion that the data were both inadequate and inaccurate in most instances.

In this research, we are addressing the problem of the inadequacy of the data while maintaining reasonably high standards of accuracy. One of the main points of inadequacy discussed was a general lack of sufficiently detailed data for all weather conditions and locations. This research deals with the methodology and instrumentation needed to provide more adequate data for the user.

Several highly accurate absolute radiometers have been developed over the past several years. We have elected to use secondary radiometers which will allow greater ease of operation and better applicability of the data to current and future needs for solar insolation data. The instrument development task described here gives details of two instruments which are being refined for this application.

The goal was to develop instruments to measure unambiguously two of the three following quantities: 1) the total solar flux on a horizontal plane, $\Phi_{\mathbf{T}}$; 2) the direct (not scattered) flux either normal to the direction of the sun, $\Phi_{\mathbf{dn}}$, or on a horizontal plane, $\Phi_{\mathbf{d}}$; 3) the diffuse (scattered) solar flux on a horizontal plane, $\Phi_{\mathbf{D}}$. In the literature these quantities have also been called the global or G-radiation, the I-radiation, and the D-radiation respectively. To determine all three quantities, we must specify two of them since

$$\Phi_{\mathbf{T}} = \Phi_{\mathbf{d}} + \Phi_{\mathbf{D}}.$$

To accomplish this goal, two Helio Associates instruments were slightly modified to measure concurrently both the total and diffuse radiation fluxes. We have also included the use of an instrument to measure the direct normal radiation flux, $\Phi_{\rm dn}$, for comparison with data from the National Weather Service.

The research results are discussed below in three sections dealing with Instrumentation, Calibration, and Data Analysis.

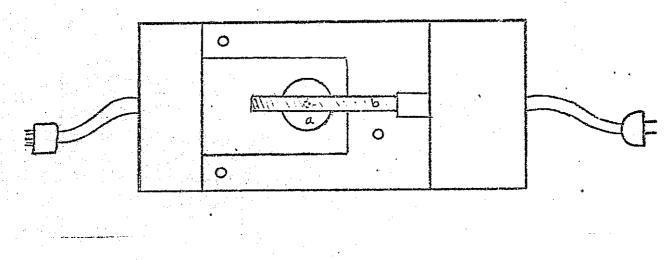
2. Instruments

The instruments used to specify the components of the solar flux are the Moving Bar Occulting Radiometer (MBOR), and the Fixed Bar Occulting Radiometer (FBOR). In addition, a widely used precision instrument with NBS traceable calibration, an Eppley Pyrheliometer, is used as a secondary comparison standard. Descriptions of these instruments follow.

2.1 Moving Bar Occulting Radiometer

A sketch of the Moving Bar Occulting Radiometer is shown in Figure 1, and a photograph of the instrument in its installed position is shown in Figure 2. This instrument has a 4.8mm diameter circular detector aperture located on the axis of revolution of a circular occulting bar. The surface of the aperture is opal glass. This surface-detector combination insures a cosine like angular response for the instrument. The occulting bar is driven at a rate of 1/3 RPM, and approximates a cross section such that a sharp shadow is cast on the aperture once per revolution of the bar in the field of view. To minimize the error in the diffuse flux caused by the presence of the bar, its width is specified by

$$W = d + 2R \sin(\frac{1}{2}^{0})$$
 (1)



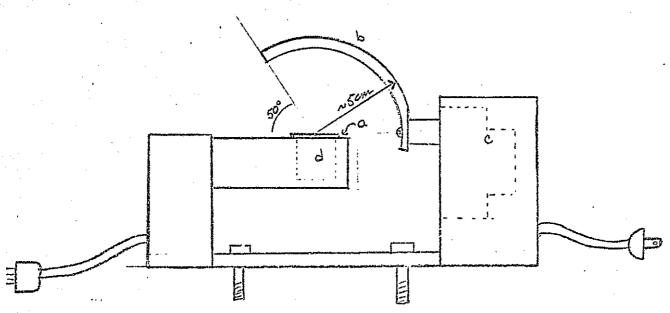


Figure 1 Sketch of the Moving Bar Occulting Radiometer (MBOR)

- a Aperture plate
- b Shade bar
- c Motor housing
- d Detector



Photograph of the Moving Bar Occulting Radiometer (MBOR) Figure 2

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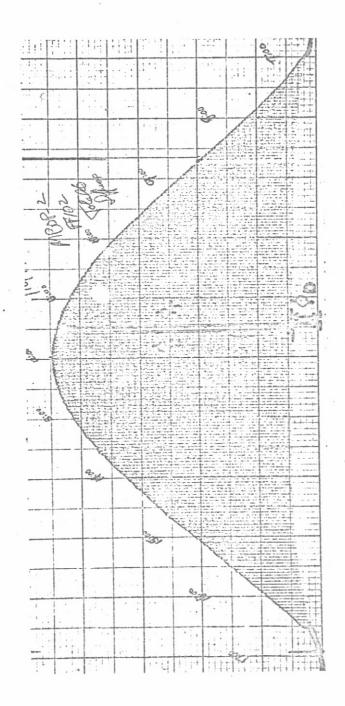
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where d is the aperture diameter and R is the radius of curvature of the bar. The bar is also cut so its arc length is sufficient for the maximum solar altitude. A correction factor has been calculated which takes into account the diffuse radiation lost to the detector due to the presence of the bar in the 2π steradian solid angle of view. When the bar is not in line with the sun, the detector produces a signal proportional to the total flux (Φ_T) . When the bar occults the sun, the detector signal is proportional to only the scattered light intensity (Φ_D) . The difference in these two quantities is the direct radiation Φ_d . The resulting output vs time is shown on the chart record in Figure 3. The values of Φ_T , Φ_D , and Φ_d , as obtained from these data are labeled for easy identification.

The overall size of this instrument is about 20 x 6.5 x 7 cm. It is, therefore, a compact package which is suited to field operation. The detector is mounted beneath the aperture plate as shown in Figure 4. The area immediately above the aperture plate, houses a neutral density filter required to keep some detectors from saturating at the maximum flux levels. One of the features of this simple instrument is that the form of the analog output renders a good visual representation of the relative amounts of the three flux quantities. However, a digital readout of the data from this instrument is difficult. It is necessary for this



Typical clear-day output from the Moving Bar Occulting Radiometer (MBOR) Figure 3

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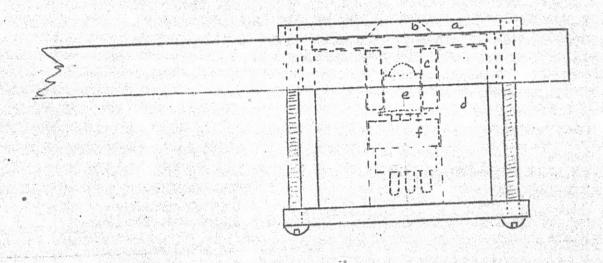


Figure 4 Detector cell design for the MBOR

- a Aperture plate
- b Diffuser
- c Detector locating sleeve
- d Cell cylinder
- e Detector (TO-5 can)
- f Transistor socket

ORIGINAL PAGE IS OF POOR QUALITY study to be able to process the data for calibration and statistical analysis. Computer compatible digital readouts reduce the labor required for these analyses. The MBOR presents a problem regarding digital readout due to the difficulty in specifying the position of the occulting bar when measuring Φ_D . There is no simple way to specify whether a change in the output is due to an occultation by the bar or by a cloud.

2.2 Fixed Bar Occulting Radiometer

An alternate design which does allow a digital output format is the Fixed Bar Occulting Radiometer (FBOR). This instrument, shown in the sketch in Figure 5, and in the photograph in Figure 6, consists of a circular ring occulting bar oriented East-West around the detector plane. The ring slides along an axis tilted with respect to the horizontal by an angle equal to the local lattitude (32.2° The motion of the bar along this axis adjusts for Tucson). for the seasonal variation of solar declination. The occulting bar has a diameter of 30.5 cm, and its width, from Eq.(1) is 5.6mm. The occulting bar is placed so that at the equinoxes, its center of curvature will coincide with the center of the aperture over one of the detectors. A second detector is mounted close to the first, but always out of the shadow. The first detector, therefore, measures only the diffuse or sky radiation, while the second measures the total flux. instrument has also been fitted with detector heads which

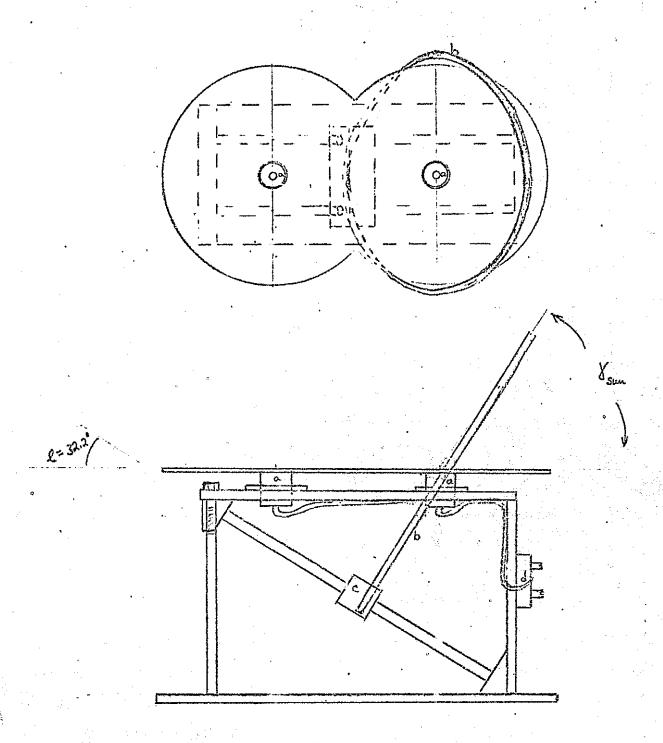


Figure 5 Sketch of the Fixed Bar Occulting Radiometer (FBOR)

- a Detector cells
- b Occulting bar
- c Slider assembly
- d Terminal block, electronic outputs

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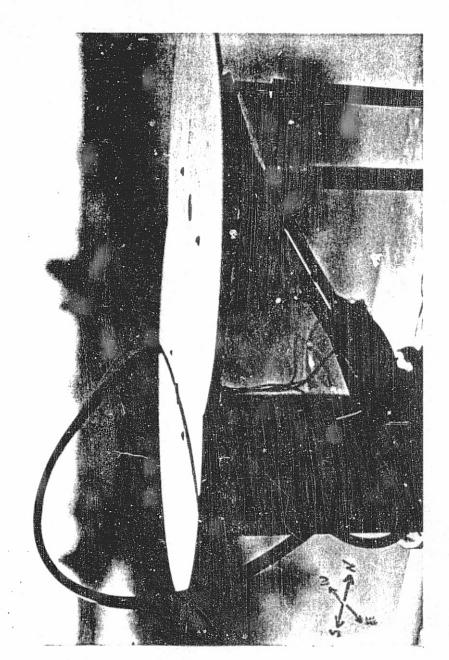


Figure 6 Photograph of the Fixed Bar Occulting Radiometer (FBOR)

ORIGINAL PAGE IS OF POOK QUALITY allow for measurement of the solar flux in four distinct spectral ranges. These multi-detector heads are arranged as shown in Figure 7. Light incident on the nearly lambertian surface of the diffuser plate is reradiated into four fiber optic light guides. These guides conduct the light down to four filter chambers symetrically placed around the vertical normal to the center of the diffuser. Four photodiodes look at the ends of the light guides through one empty chamber and three different Schott filters. The filters have sharp cutoff characteristics as shown by the transmission curves in Figure 8. The combination of light pipe, filter, and detector, are calibrated against a thermal pile detector plus the appropriate filter. The result is a device that measures the total and the diffuse energy incident on the glass screen integrated over all wavelengths larger than the cutoff of the filter. The filters chosen are commonly used by the National Weather Service and others for this type of measurement. An instrument tower was designed and constructed as shown in the photographs in Figure The 6 meter high instrument platform allows nearly unobstructed view of the horizon for the instruments. the instruments is by ladder to a lower landing, placed so that the equipment is chest level. The tower has been found to be stable enough to insure accurate tracking for the pyrheliometer.

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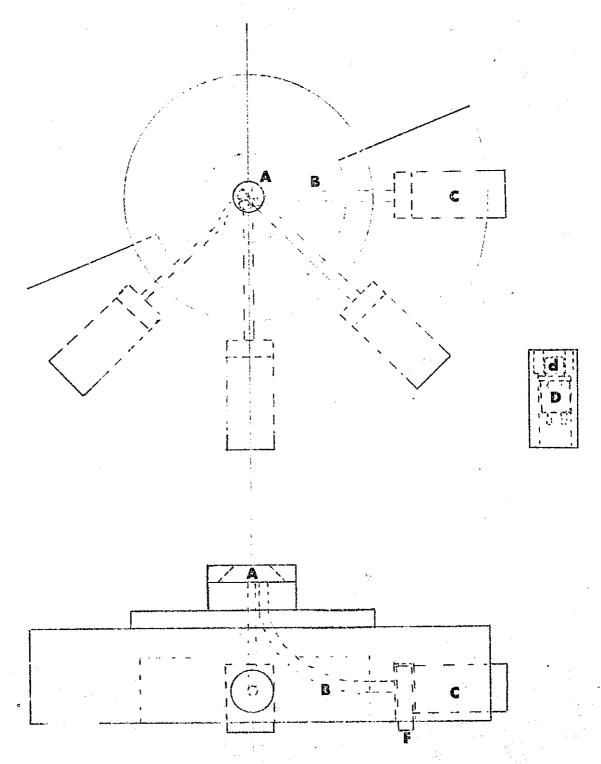
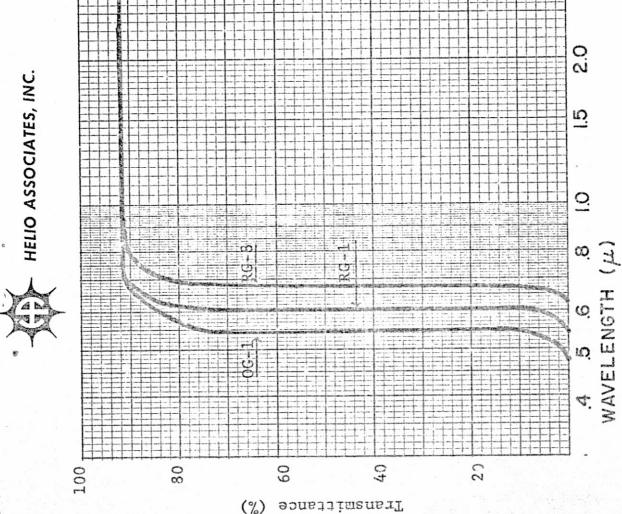


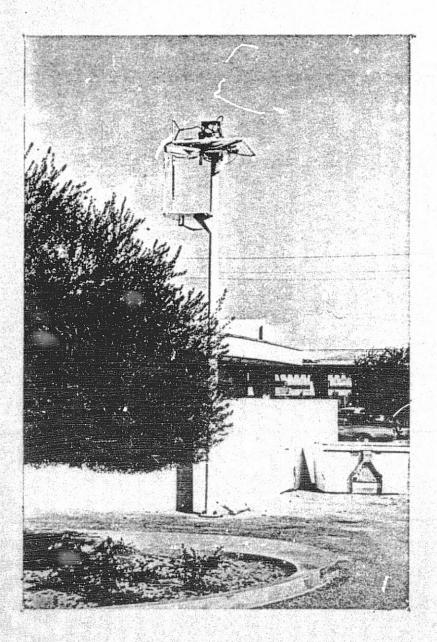
Figure 7 Sketch of the Multi-detector head for the FBOR showing:
A - the diffuser screen; B - the light pipe; C - the detector cell; d - the detector and its socket -D; and F - the filter and filter chamber.

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Transmittances vs Wavelength for the Filters used in the FBOR. Figure 8



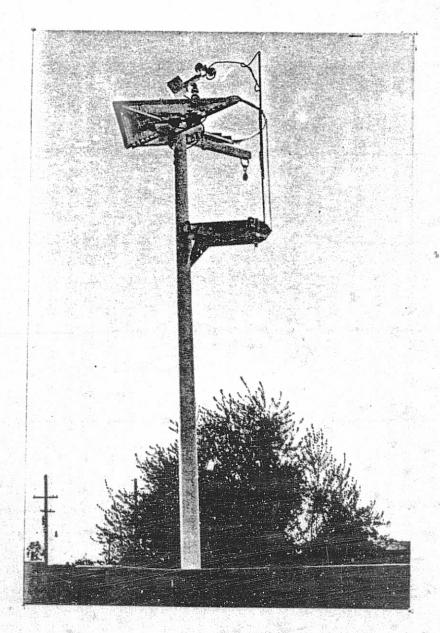


Figure 9 Photographs of instrument tower

The accuracy of the measurements, the reliability, and the simplicity of the instruments, depends on the choice of the detector. There is a wide choice of types of detectors suitable for radiometric use. In general, detectors fall into two categories that typify the mode of operation:

1) photoelectric devices such as photodiodes, photomultipliers, phototransistors, and photoresistors, and 2) thermal devices such as thermal piles, pyroelectrics, and thermistors.

The selection criteria for an ideal detector should include the following: 1) quality and long service life; 2) operating temperature range from -10 to $+70^{\circ}$ C; 3) high sensitivity over the range $0.3\mu \text{m} < \lambda < 1.5\mu \text{m}$, 4) flat spectral response over the same range; 5) suitability to radiometric use; 6) reasonable cost; and 7) simplicity of use. When available detectors are judged on the basis of these criteria, there are advantages and disadvantages for each detector type.

Among the photoelectric devices, either photodiodes or phototransistors offer the most advantages for use in our instruments.

Photodiodes have two modes of operation. In the photocurrent mode, the diodes generate outputs that are either linear or logarithmic depending on the load resistance. If the load resistance is near zero, the current vs light level is linear over several decades. The photodiodes have an advantage because of the low null drift in the zero bias photovoltaic mode due to the absence of dark current. Photodiodes can also be used as photoconductors but show temperature

drift when used in this manner. The sensitivity of photodiode-operational amplifier combination described below is well matched to solar measurement applications. Photodiodes come in small, simple packages such as TO-5 transistor cans, and can be fitted with lenses. One disadvantage for photodiodes is the characteristic spectral response for the silicon device. The peak sensitivity is usually in the near infrared between 0.8 µm and 0.9 µm with lower response in the near ultraviolet. It is not difficult, however, to use such a device, and compensate for the spectral response by filtering and calibration.

Phototransistors are, in general, limited to the photoconductive mode with inherent zero drift problems.

Phototransistors with base connections can also be used like photodiodes, but offer no advantages over simple photodiodes when used in this manner.

<u>Photomultipliers</u> have several disadvantages for use in our instruments. They are usually bulky to use, are delicate, and require costly auxiliary circuits in the form of power supplies and amplifiers.

The thermal devices have an advantage in their flat spectral response over wide spectral ranges. The response of these devices depends only on the type of absorber coating used to convert the incident radiation into heat. Since good

output and high sensitivity without the need for high voltages or a bulky detector. The principle reason for the op-amp is shown by the characteristic load curves for the diode shown in Figure 10. From the graph, one can see that at zero bias (photovoltaic) and zero load resistance, one can get a linear response characteristic. The use of the amplifier as shown in Figure 11 yields such a zero load condition and still maintains an adequate output signal. This is because the load on the photodiode is equal to the feedback resistance R divided by the open loop amplifier gain G.

The actual circuit used in our case is shown in Figure 12. Since the open loop gain of the LM741 is about 2×10^5 , and the feedback resistance is about $2 \times 10^6 \Omega$, the photodiode sees a load resistance of 10Ω . Figure 13 shows the deviation from linearity that can be expected for a cell that has an effective load resistance of this value. From the plot, one can see that even at currents as high as lmA, the device is linear to two parts in $10^5 (0.002\%)$. One can calculate the actual current from the photodiode according to:

$$V_{out} = R_{f_{out}}$$

or

$$i_o = V_{out}/R_f$$
.

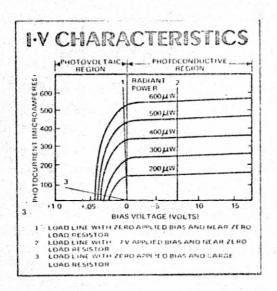


Figure 10 Load line plot for a typical photodiode (UDT3DP)

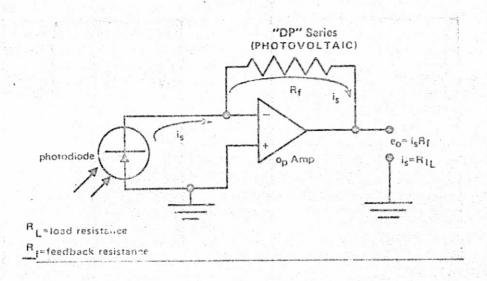
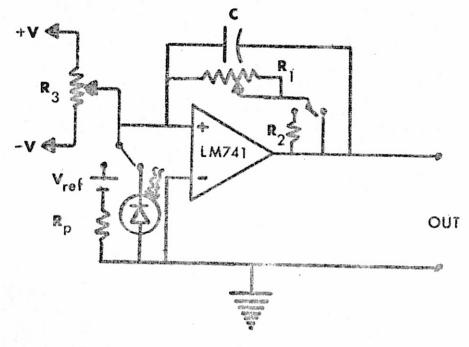


Figure 11 Circuit schematic for the photodiode - operational amplifier circuit. i_s = photodiode sensitivity x light flux, $R_l = R_f/G$ where G = open loop gain.

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 $C = 0.047 \mu f$

 $R_1 = 2M\Omega$

 $R_2 = 2M\Omega$

 $R_3 = 12M\Omega$

Figure 12 Schematic diagram of Helio circuit used for the current-to-voltage transducer.

 R_1 , R_2 feedback resistors ($R_f = R_1 + R_2$ or R_1)

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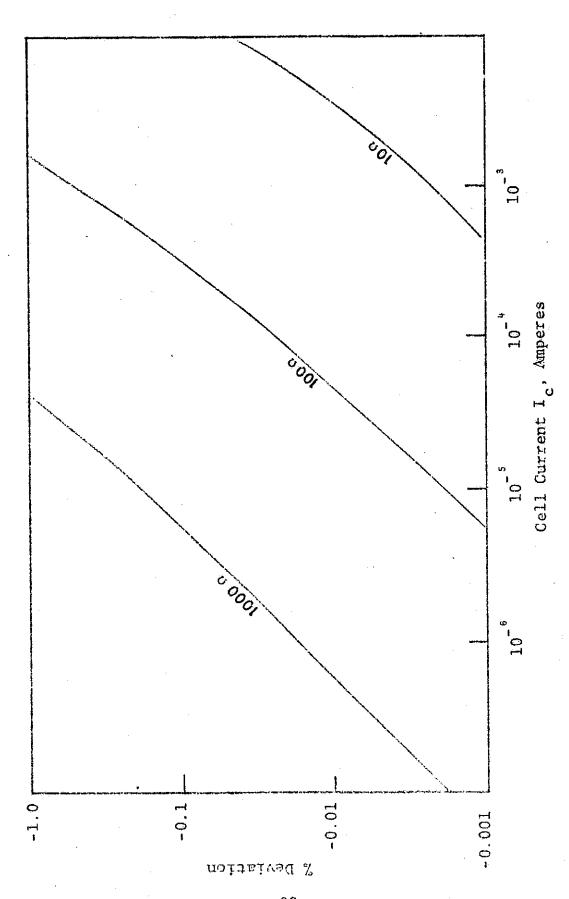
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R₃ zero offset adjustment

 ${
m V}_{
m ref}$ reference voltage for circuit gain calibration ${
m R}_{
m p}$ reference precision resistor



Deviation from linearity of the silicon cell response for short-circuit operation. Figure 13

In our case, for the maximum flux level, Vout=0.8V for $R_f = 1.6M\Omega$, so that $i_{\Omega} = 5 \times 10^{-7} A$. Referring again to Figure 13, we can see that the device is well within the linear region of operation for a 100 load. In the circuit for each detector, a reference current source or an open circuit may be applied to the operational amplifier for calibration of the gain setting, or input zero offset respectively. Adjustment of R3 in Figure 12 allows the application of a small compensating voltage to the input to counteract the output offsets inherent in the amplifier design. The temperature drift of this type of null adjustment is considerably less than that associated with the internal adjustments. A reference current is used to check gain settings. is generated by the combination of a precision voltage source V_{ref} , and the precision resistor R_{p} , as shown in Figure 12. The current is set at a level approximately equal to the photodiode current with full solar flux. This current source is stable to within 0.1%. The readings for each of the calibration runs are used as a reference to check the gain stability over a long period. Table 1 shows that the stability is better than 1%.

for each detector are mounted in a card file as shown at the top of the photo in Figure 14. The adjustments for zero and gain are attainable by screw diver only through the holes

<u>Channel</u>	1	· 2	3	4	5	. 9	6	7	8
Data Logger	17	4	4	6	7	16	13	14	15
Date:									
8-15-74	7.29	9.89	7.52	7.63	9.64	10.12	9.77	7.84	8.47
8-20-74	7.29	9.89	7.50	7.63	9.64	10.10	9.75	7.83	8.45
8-28-74	7.29	9.87	7.52	7.63	9.60	10.11	9.77	7.84	8.49
9- 3-74	7.29	9.85	7.49	7.59	9.59	10.07	9.71	7.82	8.46
9- 9-74	7.27	9.82	7.47	7.57	9.58	10.03	9.71	7.81	8.46
9-12-74	7.27	9.84	7.47	7.57	9.59	10.05	9.69	7.83	8.47
9-19-74	7.25	9.83	7.47	7.57	9.57	10.06	9.69	7.80	8.47
Average:	7.27	9.85	7.49	7.60	9.60	10.08	9.72	7.82	8.47
Down Trend Error:	. 0055	. 007	.0067	. 0079	. 0073	.007	. 008	.005	. 005

NOTE: Apparent long term drift downward <0.8%

Table 1 Circuit output readings with reference current as input. Periodic readings over one month period.

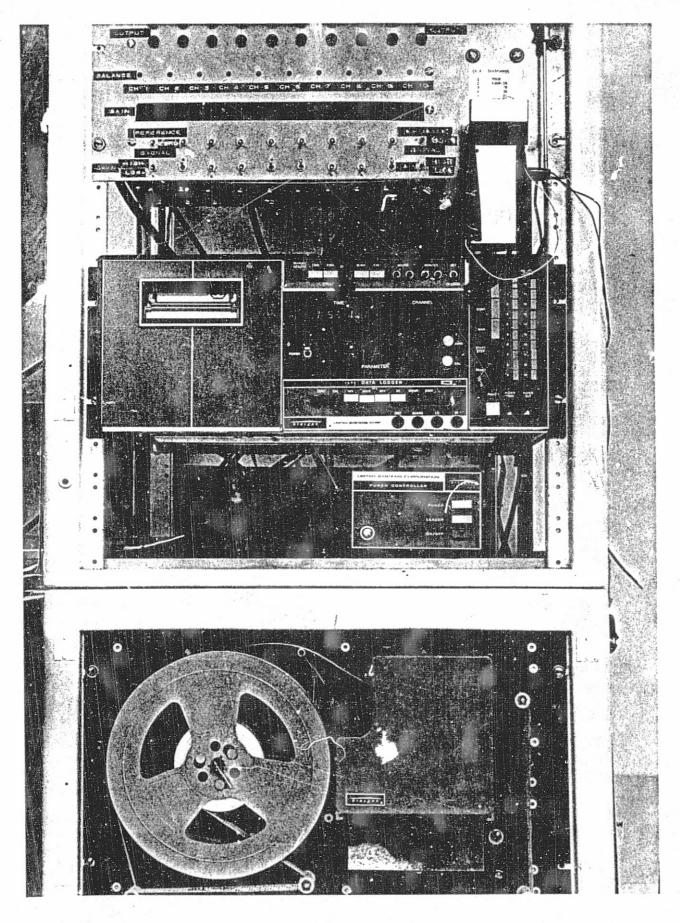


Figure 14 Photograph of circuit card bin, data logger, and tape punch.

in the front panel. Switches are provided to allow initial choice of high or low gain and choice of inputs between zero, reference, or signal. The circuits are well shielded to prevent interference from local switching circuits or AC power lines.

2.3 Data Collection

The MBOR output format as shown in Figure 13 is obtained as 10" wide hard copy from a "Brown Electronic" potentiometric recorder with a time base of 1"/hr. The resulting analog output allows a good visual representation of the solar day at a glance, but would require considerable reading time to allow a detailed mathematical analysis. We display the information as shown in Figure 15. This calendar of solar data, shows the trend in the solar flux data, and readily illustrates the type of day classification discussed below.

The FBOR output is specifically designed for computer analysis. Therefore, this system is read digitally by a data logger which punches the data directly onto paper tape. The digital logging system is shown schematically in Figure 16, and in the photo in Figure 14. The data logger is a Digited model 1268, with 20 channel capacity and the specifications given in Figure 17. The data logger is set to scan and record the 9 channels of data once every 10 minutes from sunrise to sunset. The time is read and punched before each scan. The data channels are listed in Table 2.

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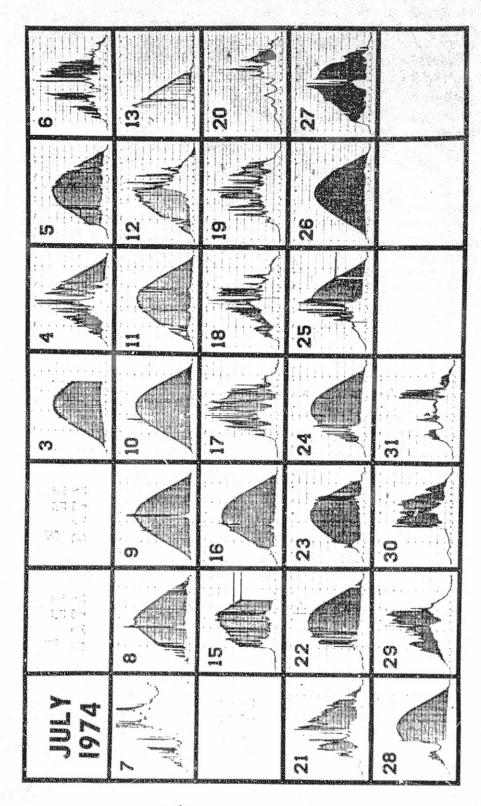
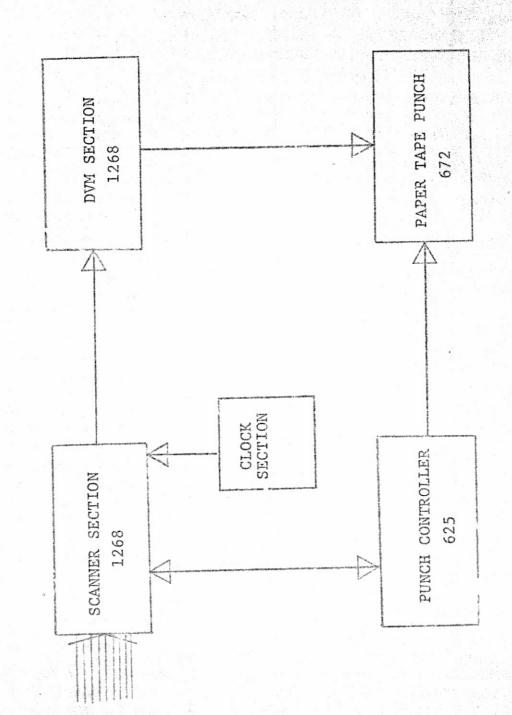


Figure 15 Data from MBOR for the month of July

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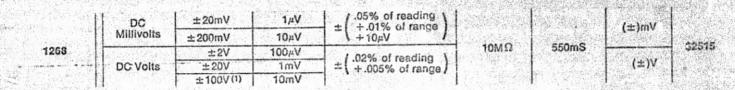
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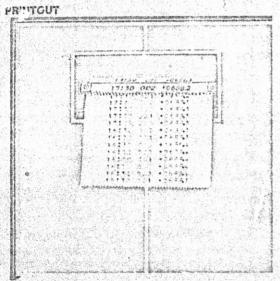
Figure 16 Schematic of Data Logger system.

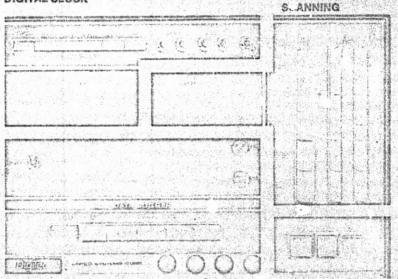
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Specifications



DIGITAL CLOCK





MEASUREMENT

MANUAL CONTROLS

THE CLOCK SECTION of DigiTec's Data Logger incorporates a convenient, separate visual display of time. Setting time is accomplished with an individual pushbutton for each digit. With the "Set/Operate" switch in the "Set/ position, internally gated pulses at 1 second intervals cause each display to count as the appropriate pushbutton is deprecised. Once the time has been set, the "Set/Operate" switch may be placed in the "Operate" position, which starts the clock timing. Fer

time interval testing, the "Set/Operate" switch may be placed in the "Set" position which stops the timing but does not reset the display.

In addition to visually displaying time and generating a print command to the Printer, the clock section contains a cycle interval feature. This feature allows the Data Logger to operate unattended at comma. d intervals of 1, 2, 10, 20 minutes and 1 hour. The cycle Interval may also be generated from a remote source by depressing the "Manual/

Remote" pushbutton. The remote cycle start is useful for time intervals other than those available internally and for coincidence recording as a result of external occurrences.

Another feature incorporated in the clock section is detection and indication of power loss. For example, should the power line fail, the clock will reset to 00:00 when power is returned. Upon return of power, the Data Logger will continue functioning in its previous mode of operation.

The first printor! upon return of power will indicate time 00:00. By observing the last time printed before power loss and computing the 00:00 to real time, it can be determined how long power was down. Visual indication, a flashing colon, is also incorporated to alert the operator that a power loss has occurred.

The clor's section serves yet another purpose as illustrated on the typical printed. The time is printed on the first and last active points for obvious block-separation of data.

Figure 17 Specifications for the 1268 Data Logger.

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**-E SCANNING SECTION

*** a separate, visual

*** prime input channel

*** the input channel

*** the input channel

*** the sextremely use
*** and including manually to a selected channel

for visual monitoring.

in scanning multiple analog inputs to the measurement section, the scanning section provides three basic mc les of operation. A MANUAL MODE is required for checking each input at the time the analog signals are initially connected. Once the Data Logger is recording data, it may be desirable to return to the manual mode for mon-Itoring a single point where unexpected conditions are occurring. The manual mode is totally manual with 10

printout unless specifically commanded to print. Most often used is the ONE CYCLE MODE, in which all points are scanned, measured and recorded, sequentially, at periodic intervals determined by the clock section, or by external command. This mode is particularly useful where parameter changes are relatively slow and constant recording is not required. The one cycle mode is controlled both by front panel and remote start/stop command. For applications where constant monitoring is desirable, A CONTINUOUS MODE is available. Once placed in this mode, the Data Logger will repeatedly measure and record all inputs until removed from this mode. The DigiTec Data Logger has

a basic scanner input capability of 20 points, which has proven to be sufficient for most applications. however, those situations requiring above 20 inputs can be satisfied by the addition of the DigiTec model 637 scanner slave frame which expands the scanning capability to 200 points.

Another very useful feature of the scanning section is ability to activate and deactivate input points by front panel control. This control is in the form of pushbutton switches, one for each point. An example of the usefulness of this feature is in a thermocouple measuring system wherein one of the inputs has opened, a common occurrence. By deactivating this point, the Data Logger will

continue to record and simply skip this input to the scanning section, therefore eliminating erroneous data recording.

MANUAL PRINTOUT

A 'Print' pushbutton allows for printing data, from the input point being monitored, on a manual demand basis.

A 'Paper Feed' pushbutton allows for spacing between printouts or blocks of printouts on a manual demand basis.

A 'Paper Out' indicator iamp illuminates when the paper supply to the printout section is too low. When this lamp is illuminated, all print commands are converted to paper advance commands, thereby avoiding damage to the print drum.

PUNCHED PAPER TAPE OUTPUT

Many applications require a computer compatible output in addition to the hard copy printout from the Data Logger. DigiTec offers the Model 672 Tape Punch and Models 624 and 625 Tape Punch Controllers to provide this output. The Model 624 provides an

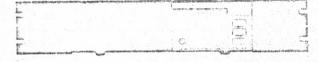
IBM odd parity code and the Model 625 provides ASCII coded outputs.

The controllers accept the BCD output from the rear connector of the Data Logger, code, serialize and drive the punch magnets of the Model 672 Tape Punch. The interface to the controllers is such that the printout and punching

functions are completely interlocked.

The format and word length of the controllers are completely programmable to satisfy a wide variety of applications. Typical cost for the tape-punch option is under \$2000. Contact the factory or your nearest DigiTec representative for a quotation on your specific requirements.





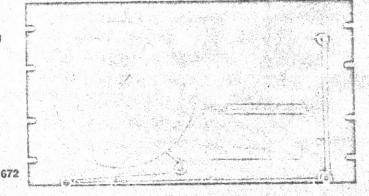


Figure 17 (Continued) Specifications for the 1268 Data Logger.

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Data Logger	Instrument	Type Measurement
Channel 3	Eppley	Direct Normal
Channel 4	FBOR-1N	Total (clear)
Channel 5	FBOR-2N	Total Thru - OG-2 Filter
Channel 6	FBOR-3N	Total Thru - RG-1 Filter
Channel 7	FBOR-4N	Total Thur - RG-8 Filter
Channel 16	FBOR-4S	Diffuse Thru - RG-8 Filter
Channel 14	FBOR-2S	Diffuse Thru - OG-1 Filter
Channel 15	FBOR-3S	Diffuse Thru - RG-1 Filter
Channel 13	FBOR-1S	Diffuse (clear)
*Channel 17	MBOR	Total, Diffuse, and Direct Analog

^{*} Not scanned for digital reading - used to set zero and check gain only.

NOTE: Due to instrument malfuncitons on this particular data logger, channels 0-2, 8, 9, 10-12, 18, and 19 cannot be scanned. For this reason, channels 3-7, and 13-16 were used for data recording.

Table 2 Data Logger Channels

3 Calibrations

of secondary standards that are traceable to the National Bureau of Standards. An Eppley Pyrheliometer is used as one substandard. This instrument is identical to the instruments in use by the National Weather Service. Three calibrations were performed on this instrument. First, the pyrheliometer was sent to Eppley for calibration against their traceable standards. The method used by Eppley is a comparison of the subject instrument and a group of reference instruments using the sun as a source. These calibrations are standardized in accord with the International Pyrheliometric Scale of 1956.

After return of the instrument, it was compared to a second pyrheliometer in current use at the Institute of Atmospheric Physics, University of Arizona. The unit was then compared again to a calibrated Eppley Thermal Pile Detector, using a calibrated Optronics Laboratory - one solar constant standard lamp as the source. These three separate calibrations were in agreement to within 2%, independent of the source used. In the latter case, care was exercised in compensating for differences in transmission of the instrument windows for the different source spectral distributions.

To calibrate the MEOR and FBOR, direct comparisons were made between the Eppley Pyrheliometer and the other instruments. Each instrument was oriented perpendicular to the

standard source, and alternate readings taken of the normal flux with each instrument at the same axial point with respect to the face of the standard lamp.

These calibrations were then repeated using the sun as the source with agreement to less than 1.5%. These calibrations are checked once each month by in-situ measurements of the normal flux with all three instruments. The MBOR and the FBOR are dismounted and aligned perpendicular to the sun and the direct normal flux is computed by differencing the total reading and the diffuse reading for each instrument. In each case the occulting bar is used to shade the detector for the diffuse measurement. The data obtained in this way is compensated for possible errors in the diffuse flux due to the presence of the bar in the field of view.

ments included relative angular response, linearity, gain drift, and zero drift. The results of the angular measurements are shown in Figure 18. The measurements indicate a departure from a perfect cosine response of less than 2.8% at large angles. The linearity of the instruments was also found to hold over 3 decades within the limits expected for the detectors used. Tests were also performed to evaluate the temperature stability of the detectors. The net change in signal level for a constant illumination was less than 1% up to 250°F. The gain drift of the amplifiers was measured

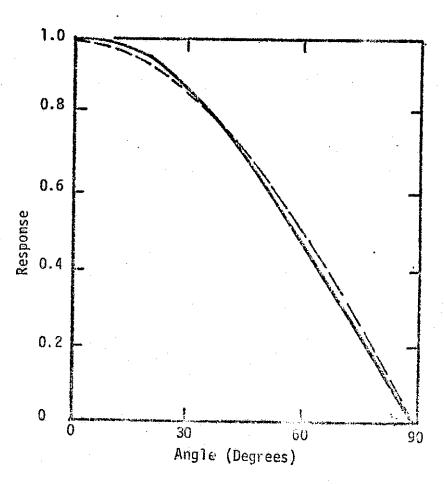


Figure 18 Angular Response of Occulting Bar Radiometer

Relative Radiometer Response

----- Cosine

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using the constant current source discussed above with the resulting error of < 0.8% over a two month unattended period. The zero drift was also found to contribute less than 0.43% error when adjustments are done daily. Over a one month unattended period, the zero drift was as much as 2.5%. The published reading and digitizing errors for the data logger are both 0.02%. On the other hand, the recording error for the Brown Electronic Recorder is approximately 1.0% of full scale due to tracking errors and line width uncertainty in reading the records.

In summary, the instruments were found to be stable, easily maintained, and reliable. The principle errors in the measurements are small and attributable to three sources: 1) the calibration uncertainty of 2%, 2) the zero drift in both the MBOR and the FBOR circuits of approximately 2.5% for unattended operation, and 3) the 1% reading accuracy of the recorder for the MBOR. All other errors are negligible.

In the total operating period of six months, only 7 days of data have been lost due to poor data quality or instrument malfunction. This means reliable data has been obtained 97% of the time. In fact, the only contributions to the 3% data loss were due to recorder or data logger malfunctions such as paper runout, pen failure, or power failure on the data logger. The only required maintenance on the instruments and their circuits has been the daily

cleaning of the optics, alignment of the occulting bar, and zero setting if necessary. The long term zero drift problem can be reduced by use of the more expensive precision amplifiers, if the instruments are to be used for unattended operation.

4 Data Analysis

The data analysis task is to translate the observations into the specific quantities useful for solar flux utilization studies. Below we discuss the several forms of data, data reduction methods, and analysis of the data.

4.1 Definitions of Observed and Calculated Quantities

We perform three basic measurements of the solar irradiance. First, the <u>direct normal flux</u> is determined from the Eppley Pyrheliometer. The direct normal flux is, therefore, the radiation passing through a unit area oriented normal to the sun and limited in angular response to a cone with a full angle of approximately 5°. This instrument, therefore, measures only the unscattered component of the flux with a small amount of forward scattered radiation from the circumsolar disk. During the day and year, the direct normal flux is diminished by only the atmospheric transmission. Under cloudless conditions, the approximate expression for the flux would hold:

$$\Phi_{\rm DN} \approx \Phi_{\rm o} e^{-B/\cos z} \tag{1}$$

where Φ is the extraterrestrial flux or solar constant, B is an atmospheric attenuation constant, and z is the zenith angle. This expression varies only slowly with small zenith angles, a 20% change in flux occurring between zenith angles of 0° to 75° . Thus, for a clear day, the direct normal flux is nearly constant except at sunrise and sunset, and the midday flux values change little during the year. This is readily observed since the sun always appears bright on clear days winter and summer.

The second measurement we perform is the total horizontal flux. This is the radiation passing through a unit area with a fixed orientation normal to the zenith direction on the earth. The detector senses radiation from the entire hemisphere above the detector. Thus, in addition to the direct flux, the scattered flux from the sky and clouds is measured. The direct flux component is that measured by the Eppley Pyrheliometer, except that it is diminished by the cosine of the zenith angle owing to the geometrical change in effective area. Thus, one can compute the zenith angle dependence by multiplying the direct normal flux Eq.(1), by the cosine of the zenith angle and adding the scattered radiation. The desired variations of the total horizontal flux on a clear day thus resembles a cosine function, and the diurnal maximum flux changes throughout the year. In the summer, when the zenith angle at noon is small, the flux is a maximum and in the

winter falls to a minimum value as the zenith angle becomes large.

horizontal flux. This is defined as the flux from the sky and clouds measured by a horizontal detector in which the solar disk is obscured from view. The scattered horizontal flux is thus a measure of the brightness of the sky. On a clear day, this is nearly a constant function sunce the Rayleigh scattering is, to a first approximation, isotropic. At large zenith angles, the scattered flux falls since the irradiance of the atmosphere falls.

Coupled with these basic measurements, filters are used to determine the approximate spectral dependence of the total horizontal flux and scattered horizontal flux.

These two quantities are measured using colored glass filters.

The observed quantities are measured as voltages at particular times. We convert these voltages to flux units by multiplying by the calibration factors. The units used for the flux are given in watts/meter². Two other sets of units are commonly used. The conversion factors are given below:

To Convert from:	<u>To</u> :	Multiply by:					
Watts/m ²	Btu/ft2/hr	0.317					
Watts/m²	Langleys/min (cal/cm ² -min	1.434×10^{-3}					

Typically, the maximum direct normal flux on the earth is of

the order of 1000 W/m2 or 300 Btu/ft2hr, or 1.4 langleys/min.

The next important quantity we measure is the energy available in a certain period of time. The energy determination is done by numerical integration over the appropriate period of time. The data are presented in terms of watt-hours/ m^2 , rather than Joules/ m^2 to allow a more direct comparison with the flux measurements since a flux of 1000 w/ m^2 falling for one hour produces an energy equivalent to 1000 w-hrs/ m^2 , rather than 3.6 x 10 6 Joules/ m^2 .

4.2 Data Reduction Methods

The measured data are operated on twice. First, the raw voltages are converted to flux units and second, the numerical integration and averages are computed.

The raw data are available in the form of serial punched paper tape in ASC II Code. Each voltage has an associated channel indentification code followed by the sign and five digits (4½) for the voltage and a l digit exponent code. The first punch in the data string is a four-digit code representing the hours and minutes at the start of the scan. Occassionally, unrecognizable characters are included in the string and channels are missing due to momentary equipment malfunction.

The procedure we have developed is to first make a file containing all of the requested data. These data are scanned and converted to voltages. Missing data are identified by a -99 code. In addition, the day, end, and

start are identified by the change in hours shown by the reset clock. The interactive mode is used to allow an operator to recognize bad data in a string or other malfunction of the equipment. The net result of the processing at this point is to divide a file containing several days of data into several files each containing one day of data. The program listing is given in Appendix A-1.

The operator may, at this point, enter the files to correct data or delete duplicate lines. Generally, this has been found to be unnecessary. On several occasions, it was necessary to correct the timer. No additive changes were made to the data.

The next phase of the data reduction is to enter the calibration factors and perform the averaging operations. First, the data are further screened for missing data, wrong times, etc. The interactive mode is used to allow operator decisions to decide whether or not to include the first and last lines of data and intervening lines with missing data. Once the data were accepted by the operator, the processing followed without intervention.

The data are presented in four forms. First, the flux for each channel is computed and tabulated. It is important to note that the values presented are an instantaneous value as opposed to an integrated value. This is important because the values show the degree of variability more accurately than integrated values. Since the input data

are scanned sequentially, there is a possibility that the correlations between measurements may be inaccurate since the first and last measurements are separated in time by about 10 seconds. This is more of a problem on partly cloudy days when the flux changes rapidly in the measurement interval.

The second level of data reduction is to perform the integrals to produce values of the energy at hourly intervals and the daily total. This format is more typical for presentation of results and reduces the volume of data significantly. Since readings are taken at 10 minute intervals, the integral is given by

$$E_{j} = \sum_{6} \Phi_{j}/6$$

where Φ_j are the flux measurements for the j th instrument. E, is, therefore, in units of watt-hrs/m².

The third level of data reduction involves channel-to-channel comparisons of the houndy integrals. First, we calculate the percentage of total energy which is scattered. This is given by

$$F_{scat} = \frac{E_{SH}}{E_{TH}} \times 100$$

where $E_{\rm SH}$ and $E_{\rm TH}$ are the scattered and total energy computed for the hour respectively. Next, we calculate the amount of energy in each spectral band as a fraction of the total, by

computing the ratios of the filtered to unfiltered channels for both the total energy and the direct component of the total energy. The direct horizontal components are found by substracting the scattered horizontal from the total horizontal components.

Finally, we compute the cumulative energy available above a parametric flux level. That is,

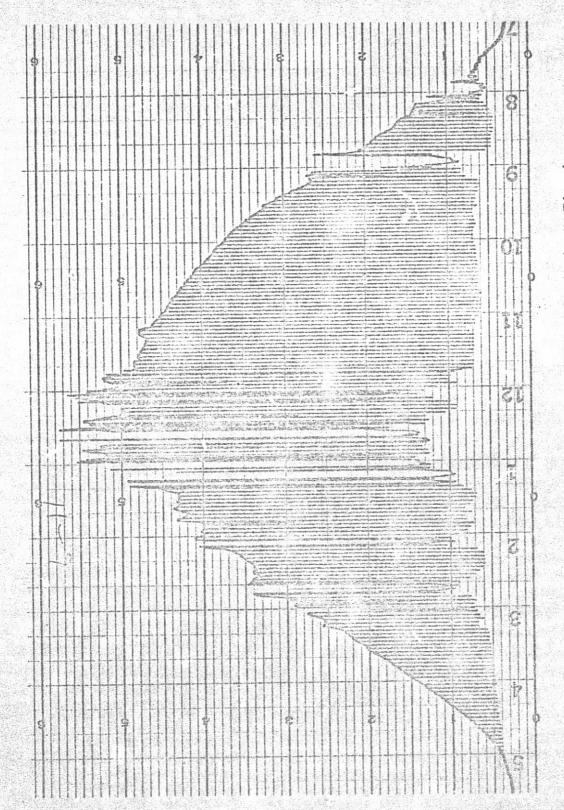
$$E(\Phi) = \sum_{\Phi \geq \Phi} \Phi \Delta t$$

where ϕ is an individual flux measurement for the time interval Δt , and is a variable ranging from zero to 1000 watts/m². The listing for this computer routine is presented in Appendix A-2.

4.3 Analysis of Data

In this section, we present a general analysis of the data, examples of the data, and interpretation of the results. Listings of the detailed data in tabular form are presented in Appendix A-3.

First, we discuss the data measured by the MBOR instrument. These data are given by quasi-continuous records of the total horizontal and scattered horizontal flux. Figure 19 shows a detailed record for a partly cloudy day. The top and bottom curves give the total horizontal and scattered horizontal flux respectively. The length of the line caused by the motion of the shadow bar



Time increases partly cloudy day. ø A sample of the MBOR flux data for from right to left. Figure 19

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is proportional to the direct flux on a horizontal surface.

We have found these records to be most useful for identifying clear, partly cloudy, and cloudy periods. In addition, they provide a clear indication of the variability of the flux as a function of time. We have also found it helpful and instructive to assemble the charts to make a calendar so that trends and sequences can be observed on a day-to-day basis.

We have done little numerical analysis of the records, however. Human reading errors and time involved in digitizing the data make such analysis difficult. The accuracy of the measurements and correlation with the data recorded digitally has been found through several spot checks to be within about 5% or less.

The monthly records for the period of July through October are presented in Appendix A-3. Climatological data for these months are shown in Table 3, where one can see that there was about 40% more rain than usual and 15% more clouds which decreased the percentage of possible sunshine by 2%. Generally speaking, it was not an atypical period from a climatological point of view.

Reviewing the monthly records of the solar flux, it is somewhat surprising to note the large number of days with significant cloud cover. One is generally prejudiced by the tourist promotions that advertise exceptional weather

in this area. On this basis, one might expect to observe much more clear weather than is shown. Although it it true that these months are the "traditional rainy season", the records still show more cloudiness than one would expect. One is also prejudiced by long term averages that show this area as one with significant sun and clear skies. It is important to compare the averages with the detailed records, however, to be able to obtain even a qualitative "feel" for the meaning of the statistics. Reviewing the month of August, for example, there is a large amount of sunshine available as shown by the shaded area in the records. But, the percent of possible sunshine average for the month shows that it was "clear" 92% of the time. Although the detailed records bear this out, the inadequacy of a single number and the nature of the measure ent of the percent possible sunshine is obvious.

TABLE 3 Climatological Records for Tucson, actiona

<u>Month</u>	Rainfo	alı (in)	% Possi	<u>ble Sun</u>	Swarise-	Sumrise-Sumset Sky Cover			
	1974	<u>Avg</u> .	<u>19</u> 74	Avg.	<u>1974</u>	Avg.			
July	4.44	2.38	84	77	5. 9	5.2			
August	1.04	2.34	92	80	2.8	4.5			
Sept.	1.69	1.37	81	87	4.0	2.8			
Oct.	2.12	0.66	68	89	4.7	2.7			
Cum. Avg	. 2.32	1.69	81	83	4.4	3.8			
% Depart	une	+37	य -	-2	+	16			

It is also obvious from these data that it would be impossible to provide a detailed record of this nature from space. First, it would be operationally difficult to produce this quantity of detailed data. Second, many of the strongly time-dependent phenomena arise from small clouds and changes in cloud depth. Reproduction of these records would require high resolution equipment that is not generally feasible for meteorological applications. Finally, we do not have sufficient data to correlate the down-welling flux to the albedo to allow data reduction with sufficient accuracy. Optical imagery from space is well suited for determining cloud-cover trends over large areas; a task beyond the reach of most terrestrial instrumentation and measurement programs.

Let us now review the detailed numerical results. A limited amount of data are presented here because of equipment malfunctions and delay in having defective equipment repaired and replaced. The data presented are representative of a small cross-section. Additional data will be presented in reports of a subsequent research study.

First, we consider the detailed flux records presented in Appendix A-3. These records produce the detailed numerical results at ten-minute intervals. The gross features discussed above are reproduced in the numerical records. The

The rapid changes of several orders of magnitude in any flux measurement over a ten-minute interval can be seen by scanning the data. Two other features of the data should be noted First, it is common to observe small fluctuations in the flux throughout the day, even on clear days. phenomenon may be due to small changes in the depth or density of the atmosphere that change the atmospheric transmittance by about 10% at the most, but more typically, less than about The phenomenon is nearly periodic. Since this is ob-2%. served in all of the instruments, we can rule out the possibility that it is related to instrumental tracking errors or sway in the instrument tower. The second feature we wish to note from these data is that near sunrise and sunset, the absolute accuracy of the measurements becomes low, resulting in descrepancies in the data such as reading more scattered flux than total flux. It should be kept in mind that the accuracy limit is approximately + 7 Watts/m2.

Next, we proceed to the hourly energy tables in Appendix A-3. Here again, we observe the effect of integration and averaging of data on loss of resolution. From an engineering point of view, the temporal variations can be extremely important to solar energy applications. Presentation of integrated or averaged measurements has been common practice in the past and can be misleading if not properly interpreted. They serve a definite value in allowing an individual to



consolidate large amounts of data for better recognition.

To illustrate some of the features of the averaged data, we present several examples of averaged data for comparison with expected results. First, in Figure 20. we show average hourly flux for the days with complete data in August. This graph corresponds to the output of the MBOR instrument. First, we note that the average is far more regular than the actual data. If one were asked to roughly sketch a "typical day", without necessarily following strict mathematical rules, he would probably include some of the large fluctuations in the afternoon. From Figure 20, one can see that this should be done since the scattered flux reaches a maximum at 15 hours.

The next level of data consolidation is the daily or monthly total energy. Naturally, we loose more information in this consolidation. It is of interest, however, to compare the daily total energy with other climatological data. The percentage of possible sunshine is measured with an instrument that counts the number of hours that the solar disk is visible. When we compare the number of hours that the direct normal flux is greater than 100 w/m², we obtain the same results. When we plot the daily total direct normal energy against the percent of possible sunshine, we obtain the fesults shown in Figure 21. One might expect a linear relationship between the two quantities. From the limited data here, however, one would expect no direct flux for less than about



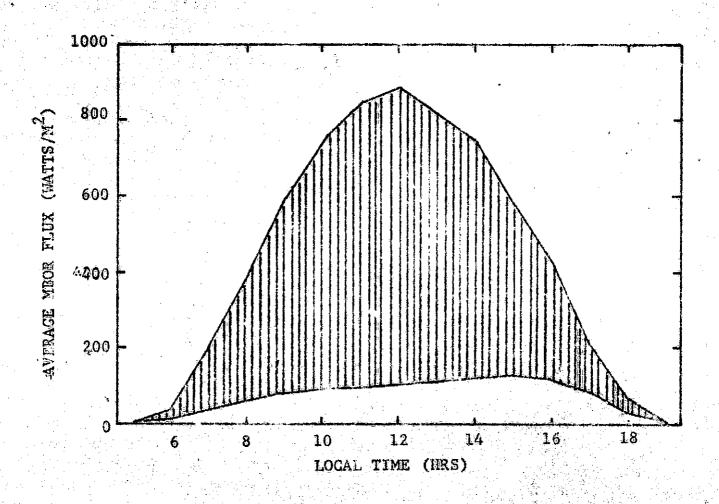


Figure 20 The Hourly Average Flux. August 1974



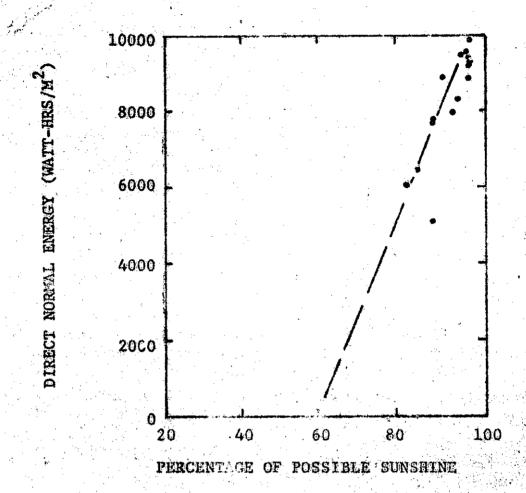


Figure 21 A Comparison between the direct normal energy and the percentage of possible sunshine

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absorbing surfaces are available for the ultraviolet through the far infrared, thermal devices are usable at almost all wavelengths. Thermistors are among the more expensive devices considered. They are also limited in their operating temperature range and often require cooling. Pyroelectrics. on the other hand, can operate at temperatures up to the curie point of the pyroelectric material which is usually about 50-70°C. These detectors also have a flat spectral response, but require chopped imput light signal for proper operation. Of the thermal detectors, the simplest is the thermal pile. This detector can operate without chopping and at temperatures up to 125°C, and is frequently used for solar measurements. The use of such a detector, however, requires care to exclude unwanted infrared radiation from surfaces around the detector. The flat spectral response is a highly desirable characteristic.

Silicon photodiodes were selected as a first choice for our application because of their numerous advantages. The lack of a flat spectral response is easily correctable and not judged to be a serious disadvantage. The United Detector each-nology 3DP pin photodiode was selected as the primary detector after comparative testing of other similar detectors. Silicon photodiodes of this type have become more widely used with the development of improved output electronics. Recent articles 1,2,3 discuss the equivalence of silicon photodiodes, combined with an operational amplifier (op-amp) output circuit to photomultipliers. This diode/op-amp combination gives a linear

60% possible sunshine. It is obvious that since the total energy depends both on when the cloudy period occurs and on the nature of thin clouds, the percentage of possible sunshine should be regarded as only an approximate measure of solar energy.

Next, we compare in a similar manner, the average cloud cover with the scattered energy. We observe that the scattered flux increases in the presence of clouds. The sunrise to sunet cover index is meant to provide cloudiness data. This data is an estimate made by the meteorologist of the amount of cloud cover determined visually to the nearest tenth of the sky. Although based on qualitative observations, it is an amozingly good index. We plot the results in Figure 22, where the spread in the data can easily be seen. As in the case of the percentage of possible sunshine, we would expect that the correlation would be low since the measurements are not exactly similar. That the sky-cover index is as good as it appears is somewhat remarkable.

There have been a number of studies that try to relate direct, scattered, and total solar energy. During this study, we have learned that this is nearly an impossible task on a short-time base. There are an infinite number of possible cloud locations, thicknesses, our angles, etc., that can alter the measured parameters. An example of such a study is that by Liu and Jordan where they have analyzed solar energy measurements from several locations to determine average



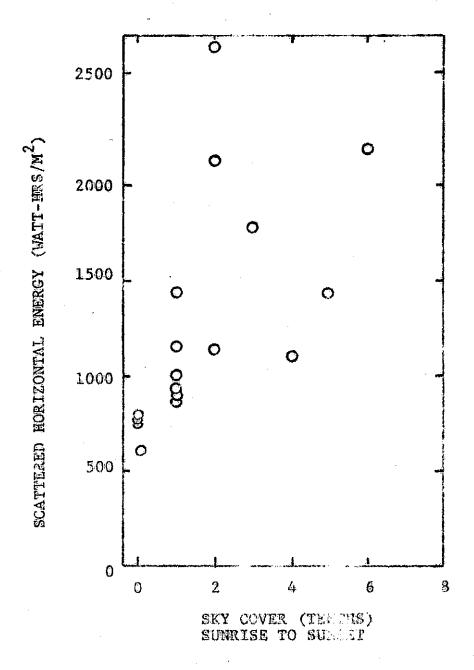


Figure 20. A comparison between scattered energy and sky cover.

transmission factors and average ratios for the solar flux.

We have found that these factors hold well for clear days
and for an average of a large number of cloudy days, but
in general, they do not describe even the daily total energy.

It is of considerable interest and importance to be able to specify the fraction of the total energy which is scattered. The amount of scattered energy depends both on the presence of clouds and the position of the sun in the sky. On clear days the scattered flux is generally less than 100 w/m². At sunrise and sunset, nearly all of the flux is from the sky overhead. Thus, on a clear day, the scattered flux is minimim near midday and represents less than 10% of the energy. The fraction rises to the limit of 100% at the beginning and end of the day. When averaged over the entire day, the scattered flux is about 10% of the total on clear days and increases to nearly 100% on overtest days.

We have used our data to estimate the fraction of energy lost in the direct beam which is scaltered back into space, increasing the albedo. On partly cloudy days, the fraction is equally divided. On heavy overcast days, about 25% reaches the earth.

The spectral distribution of the energy is of intovest also. In this study, we use three filters to determine the spectral distribution. These filters transmit the light longer than .53, .61, and .70pm. For an air mass of 2, we

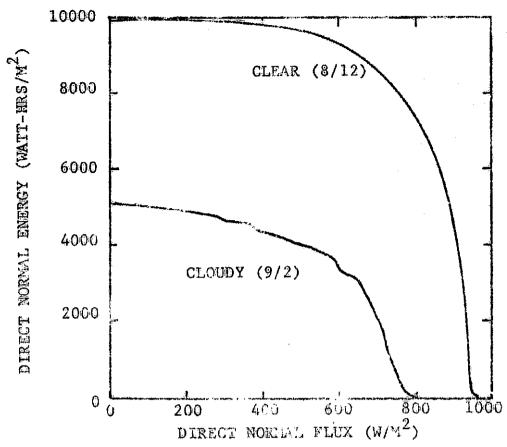
, t :

ORIGINAL PAGE IS OF POOR QUALITY would expect that the three bands would give 79.5%, 66.8%, and 53% of the total. The average values we observed for all air masses were 71%, 65%, and 59%. The differences can easily be explained by variations in the humidity and turbidity of the atmosphere at various locations.

Probably the most important aspect of solar flux measurements is to describe the quality of the flux in some manner. The final set of tables giving the energy content as a function of the flux level is one method of presenting this information. In Figures 23 and 24 we present a comparison of clear and partly cloudy day information for direct normal and total horizontal mases. The two sers of data are representative of a trend we have noted consistently. losses in the direct flux on cloudy days are always three significant than the losses in the total horizontal flux in two regards. First, since the flux loss in the direct beam is partially restored by the scattered radiation, the procentage loss in the direct normal energy is less than is the total horizontal case. This can easily be seen as the zero flux incercepts on the guada. This observation is not too surprising. It is, however, somewhat surprising to find that the maximum total horizontal flur rate is not seriously diminished for partly cloudy conditions, but is for the direct flak. The effect of clauds on the total thux is smaller than we had originally thought.

One problem still remains unsolved. The unount of data

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Fi are 23 Direct normal energy as a function of flux

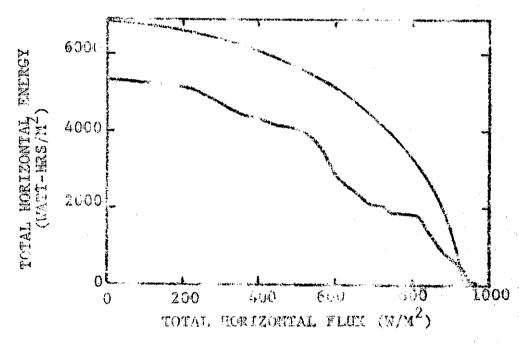


Figure 24 Total horizontal energy as a function of flux.

required to fully characterize the flux is much larger than one would ideally like. One of the more promising tools we investigated is the use of Fourier analysis.

The basic principle of the analysis of solar flux using Fourier analysis is that the incident flux $\phi(t)$ is a function of time that can be transformed to a function of frequency. The numerical processes are well known, detailed theorems being found in most college text books. The flux can be represented as

$$\Phi(t) = \sum_{n=0}^{\infty} \left[A_{n} \cos(n\pi t/\tau) + B_{n} \sin(n\pi t/\tau) \right] + A_{0}/2$$

where A_n and B_n are the Fourier sine and cosine coefficient: and τ is the period. The coefficients are determined from the flux using the Fourier sine and cosine integrals:

$$\Delta_{n} = 1/\tau \int_{-\tau}^{\tau} \Phi(t) \cos(n\pi t/\tau) dt$$

and
$$B_n = 1/\tau \int_{-\tau}^{\gamma} \Phi(t) \sin(n\pi t/\tau) dt$$
.

A preferred expansion, in this case is

$$\Phi(t) = A_0/2 + E C_n \cos(n\pi t/\tau + \gamma_n)$$

where

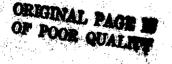
$$c_n = \sqrt{A_n^2 + B_n^2}$$

and

 $\gamma_n = \arctan(A_n/B_n)$.

Here, we speak of the coefficients A_0 and C_n as being the frequency spectrum of the flux. The larger the value of one of the coefficients, the more energy there is in the flux that can be characterized by that frequency. The frequency is give by n/γ .

The Fourier coefficients for the two days are compared in Figure 25, where the discrete points have been joined for the reader's convenience. Two features are readily observed. First, since the form of the clear day data is not a pure sinusoidal function, there are higher frequency component: that make up the Fourier series. The cloudy day data shows that there is considerably more energy at the higher frequencies, as one would expect. It is interesting to note that in the data we have reviewed to date, that the spectra for similar weather conditions are remarkably similar, even though the flux traces are somewhat dissimilar. Apparently there are characteristic frequencies in the solar insolation.



(1)

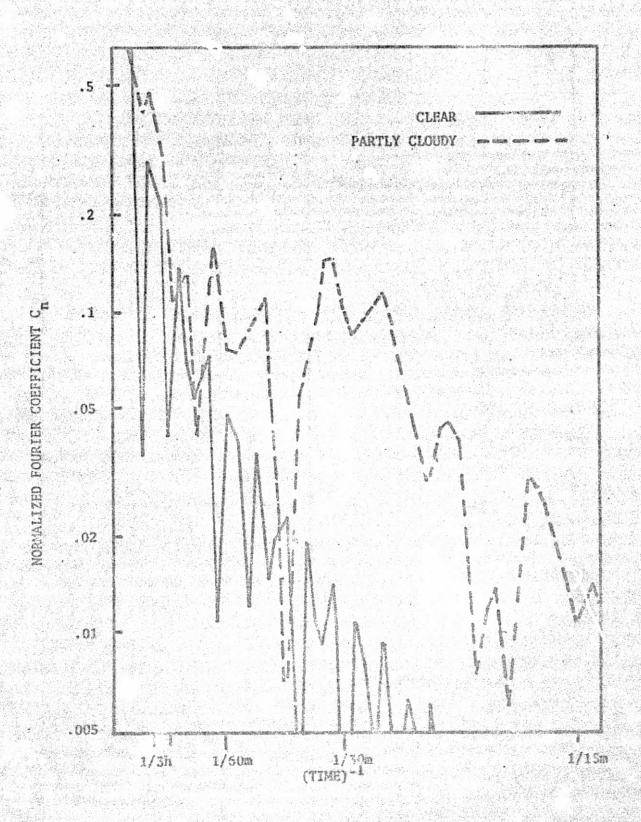


Figure 25. The Fourier Spectra for clear and partly cloudy days.

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III CONCLUSIONS AND RECOMMENDATIONS for FURTHER RESEARCH

The instruments developed proved to be well-suited for making the measurements of the solar flux. They were able to discriminate between the direct and scattered radiation. The data showed the expected general features with regard to relationships between scattered, direct, and total flux. The nature of the temporal variations of the flux was a somewhat unexpected result. Also unexpected was the number of days that were cloudy or partly cloudy.

Two recommendations for further work can be made. First, in addition to the temporal characteristics of the flux, it would be of considerable value to be able to define the spatial characteristic such that size and velocity determinations can be made, thereby completing the dimensional aspects of the characterization of the sclar radiation. The second recommendation would be to find better means of statistically analyzing the flux measurements such that certain temporal aspects of the flux could be preserved.

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ORIGINAL PAGE IS OF POOR QUALITY

APPENDIX A-1

TAPE READ PROGRAM LISTING

```
100 DIMENSION X(2), D(10)
 110 REAL NX(10)
 120 ALPHA C(12), A(14), ANS
 130 FILENAME DI.DO
 140 DATA C/"0","1","2","3","4","5","6","7","8","9","-","+"/
 150 DATANX/3-,4-,5-,6-,7-,13-,14-,15-,16-,17-/
 160 JS=1
 170 TL=0 .
 180 PRINT," INPUT & OUTPUT FILES"
. 190 INPUT.DI.DG
 200 1 READ(DI-100-END=$9)A
 210 100 FORMAT(18A1)
 220 K=1
 230 X(1)=0.;X(2)=0.
 240 DO 7 I=1.14
 250 D04J=1.12
 260 IF(A(I).EQ.C(J))GOTO5
 270 A CONTINUE
 280 GOTO7
 290 5 Jau-1
 300 IF(J.GT.9)GOTOS
 310 X(K)=10 **X(K)+9
 320 GOTO7
 330 6 K=2
 340 S=1.+2.*(10-J)
 350 7 CONTINUE
 360 IF(X(1).LE.20.)GOT010
 370 IF (US .EG .1 ) GOT 09
 380 D081=1.9
 390 IF(D(I).NE.-99.)GCTC15
 400 8 CONTINUE
 410 GOTC9
 420 15 TL*T
 430 WRITE(DO,103)T.(D(1),1=1,9)
 440 103 FORKATIFE .P. 9F7 .ST
 450 9 JS=JS+1
 460 Nyx(1)/100 &
 490 K(1)rX(1)-8-100.
 480 TeN/100 ..
 490 90111-1.9
 500 11 D(I)=-99.
 510 IF (T *GE *TL)GOTO10
 520 PRINT," PROCESSING COMPLETE FOR", DO." LENGTH=" , JS
 530 PRINT," TIME IS",T
 540 PRINT," HEAD MORE"
 550 INPULANT
                                    ORIGINAL PAGE IS
 560 IF (ANS.EG."NO") GO TO 25
                                    OF POOR QUALITY
 570 PRINT," NEXT FILE"
 550 TL=0.
```

590 INPUTATO

```
600 JS=2
610 10 D0131=1.10
620 IF(X(1).EQ.NX(1))GOT014
630 13 CONTINUE
640 GOT01
650 14 D(1)=S*(X(2)-2.)/10000.
660 GOT01
670 25 PRINT," BALANCE FILENAME"
680 INPUT.D0
690 WRITE(D0,100)A
700 26 READ(DI,100,END=99)A
710 WRITE(D0,100)A
720 GOT0 26
730 99 STOP;END
```

APPENDIX A-2

DATA ANALYSIS PROGRAM LISTING

```
100
          DIMENSION X(10,85),C(10),R(10,16),XL(10)
 110
          DIMENSION ES (2,50), RA (10,16)
 120
          FILENAME DI
          ALPHA ANS
 130
          DATA C/O-136-4-97-59-73-8-93-95-62-01-107-07-78-83-65-04-
 140
 1504
                 77.83/
          PRINT," INPUT FILE".
 160 1
170
          INPUT.DI
 180
          J=2
 190 2
          READ(DI, 100, END=8)(X(I,J), I=1,10)
 200 100 FORMAT(F6.2,9F7.3)
 019
          PRINT," FIRST LINE"
 220
          PRINT 100, (X(I,J), 1=1,10)
 230
          PRINT," USE / DUMP"
 240
          INPUT ANS
 250
          IF(ANS -NE ."USE")GO TO 2
 260 3
          YL=X(1,J).
 270
          J=J+1
 280 4
          READ(DI, 100, END=8)(X(I, J), I=1, 10)
 290
          Z=10 . * X(1, J)
 300
          IF(X(1,J),LE,YL)GO TO 6
 310
          Z=AINT(Z)/10.
 320
          IF(Z+LT+X(1+J))60 TO 4
 330
          DO 5 I=2.10
 340
          IF(X(I,J))80,5,5
 350 5
          CONTINUE
 360
          GO TO 3
 370 80
          PRINT 100 (X(I,J), I=1,10)
 380
          PRINT," USE / DUMP".
 390
          INPUT, ANS
          IF (ANS . NE . "USE" )GOTO 4
 400
 410
          GO TO 3
 420 6
          PRINT," TIME WRONG LINE 2:"
 430
          K=J-1
 440
          PRINT 100, (X(I,K), 1=1,10)
          PRINT 100, (X(I,J), I=1,10)
 450
          PRINT," USE / DUMP"
 460
 470
          INPUT, ANS
 480
          IF (ANS . NE ."USE" )GO TO 4
 490
          PRINT," TIME >", X(1,K)
          INPUT, X(1,J)
 500
                                           ORIGINAL PAGE E
 510
          GO TO 3
 520 8
          ا-ل≖ل
                                           OF POOR QUALITY
 530
          PRINT," IS LAST LINE"
          PRINT 100 (X(I,J), I=1,10)
 540
 550
          INPUT ANS
          IF (ANS .EQ ."NO")GO TO 8
 560
 570
          JT=J+1
 580
          DO 7 1=2,10
 590
          · Oa(I+I)X
```

```
600 7
         X(I,JT)=0.
         DO 21 J=1.JT
610
620
         YL=X(10,3)
630
         X(10,J)*X(9,J)
640
         X(9,J)*X(8,J)
650
         X(8,J)=X(7,J)
660 21
         X(7.J)=YL
670
         N=JT-1
680
         DO 74 J=2.N
690
         F = (X(1, J) - INT(X(1, J))) / .6
         X(l,J)=INT(X(l,J))+F
700 74
710
         2≖ل
720
         T0=X(1,J)-1./6.
730
         X(1,JT)=X(1,N)+1./6.
740 70
         1+ل≖ل
750
         IF(J.GE.JT)GO TO 73
760
         TJ=T0+(J-1)/6.
770
         LT-(L,I)X=AT
780
         IF (ABS(TR).LT.0.166)GOTO 70
790
          JT=JT+1
800
         U-TL=N
810
         DO 71 K=1.N
820
         JK#JT#K
835
         JL=JK+1
840
         DO 71 1=1-10
         X(I,JL)=X(I,JK)
850 71
860
         LT=(L,I)X
870
         DO 72 1=2.10
880
         JK = J + 1
890
         JL = J-1
900
         X(I,J)=X(I,JL)+(X(I,JK)-X(I,JL))/(6.*(X(I,JK)-X(1,JL)))
910
         IF(X(I,J).LT.-5.)X(I,J)=-99.
920
    72
         CONTINUE
930
         GO TO 70
940 73
         X(1,1)=X(1,2)-1./6.
950
         DO 9 I=1,15
960 9
         H(1,1)=4.+1
970
         DO 25 I=1.2
980
         DO 25 J=1.50
990 25
         ES(I,J)=0.
1000
          D0 12 J=1.15
1010
          DO 12 1=2:10
1020 12
          R(I,J) 100 .
1030
         DO 17 J=1,JT
1040
          DO 13 I=2.10
1050
          IF(X(I,J).LT.-10.)GO TO 13
1060
          IF(X(1,J).LT.0.)X(1,J)=0.
1070
          CI) D*CU_I) X¤(U_I)X
1080 13
         CONTINUE
1090 22
         DO 15 I=2,10
                                            ORIGINAL PAGE IS
                                             OF POOR QUALITY
```

```
IF(X(I,J).LT.0. GO TO 15
1100
          IT=INT(X(1-3))-4
1110
          R(I_{\bullet}IT)=R(I_{\bullet}IT)+X(I_{\bullet}J)/6
1120 20
1130
          IF(I.GT.3)GO TO 15
          LM=50-IFIX(X(I,J))/20
1140
1150
          IF(LM<1)LM=1
1160
          K=1-1
          ES(K,LM) =ES(K,LM)+X(I,J)/6.
1170
1180 15
          CONTINUE
          CONTINUE
1190 17
          DO 16 I=2.10
1200
1210
          R(I,16)=0.
          DO 16 J=1,15
1220
1230 16
          R(I,16)=R(I,16)+R(I,J)
1240
          REVIND DI
          D0 18 J≈1.JT
1250
          WRITE(DI,101)(X(I,J),I=1,10)
1260 18
1270 101 FORMAT(F6.2.9F7.0)
1280
          DO 19 J=1.16
1290 19
          WRITE(DI,101)(R(I,J),1=1,10)
1300
          DO 30 J=1,16
1310
          DO 31 1=1.9
          XL(1)=0.
1320 31
1330
          IF(R(3,J).LE.0.)GO TO 33
          XL(1)=100.*R(7,J)/R(3,J)
1340
          DO 32 1=4.6
1350
1360
          L=I-2
          XL(L)=100.*R(1,J)/R(3,J)
1370 32
1380 33
          YL=R(3,J)-R(7,J)
1390
          IF(YL.LE.O.)GO TO 30
          DO 34 I=5.7
1400
1410
          LL=I+3
1420
          L=I-1
          XL(I)=100 .*(R(L,J)-R(LL,J))/YL
1430 34
1440 30
          WRITE(DI,101)R(1,J),(XL(1),I=1,7)
1.450
          DO 40 K=1.2
          DO 40 L=2.50
1460
1470
          LM=L-1
1480 40
          ES(K.L)=ES(K.L)+ES(K.LM)
          PRINT," IS THIS FIRST DAY OF WONTE"
1490
1500
           INPUT, ANS
           IF (ANS . EQ . "YES")GO TO 52
1510
          REWIND "AVE"
1520
1530
          READ("AVG", 104)NT
1540
          DO 50 J=1.16
          READ("AVG",105)(RA(1,J), I=1,10)
1550 50
1560
          NT = NT + 1
1570
          DO 51 1=2.10
                                                ORIGINAL PAGE IS
 1580
          DO 51 J=1.16
                                                 OF POOR QUALITY
 1590 51
          RA(I,J)=R(I,J)+RA(I,J)
```

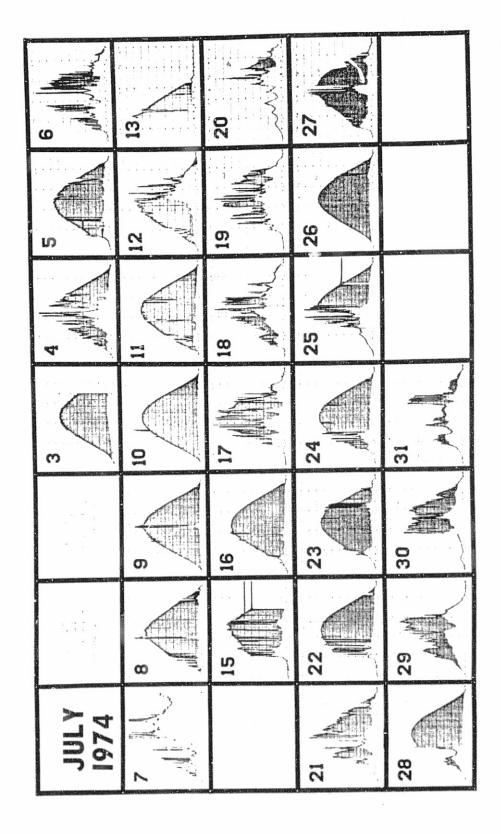
```
REWIND "AVG"
1600
         GO TO 54
1610
1620 52
         NT = 1
         DO 53 I=1:10
1630
1640
         DO 53 J=1.16
         RA(I,J)=R(I,J)
1650 53
1660 54
         WRITE ("AVG", 104)NT
         DO 55 J=1,16
1670
         WRITE("AVG",105)(RA(I,J),I=1,10)
1680 55
1690 104 FORMAT(14)
1700 105 FORMAT(F5.1.9F7.0)
         DO 41 L=1,50
1710
          I = (51 - L) * 20
1720
1730
          J=(50-L)*20
         WRITE(DI,103)I,J,(ES(K,L),K=1,2)
1740 41
1750 103 FORMAT(215,2F7.0)
         PRINT," MORE DATA"
1760
1770
          INPUT, ANS
          IF (ANS .EQ ."YES")GO TO 1
1780
          STOP; END
1790
```

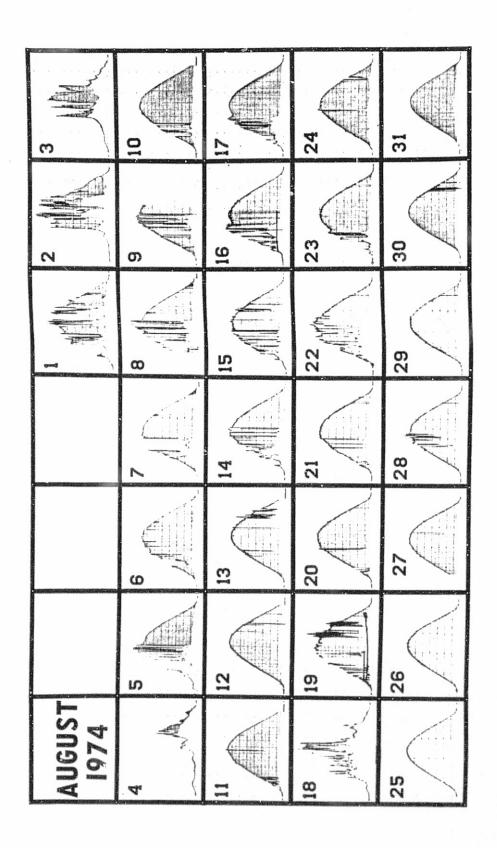
ORIGINAL PAGE IS OF POOR QUALITY

APPENDIX A-3

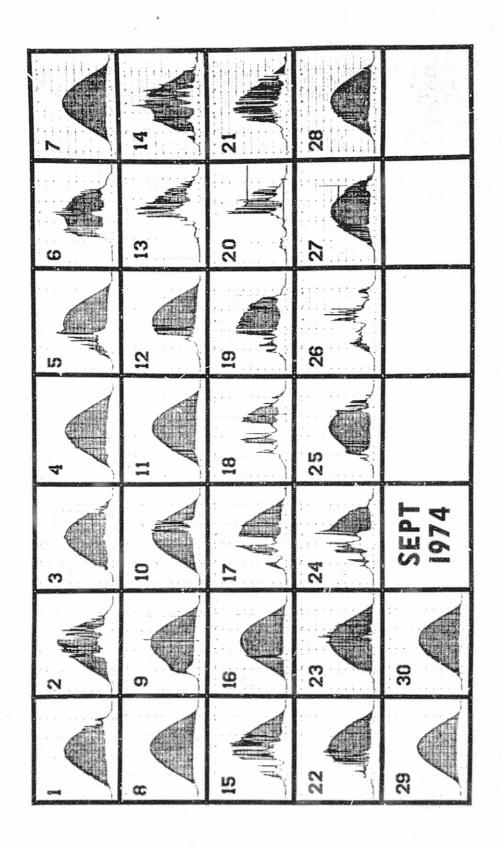
DATA

Con	tents: '										
	MBOR Data.		•			•		•	•	•	. 69
	Flux Data.				 •	•				٠	. 74
	Hourly Ave	rage	F	lux	 •		•	*			. 91
	Hourly Rat	ios.	•			•	•		•	•	. 97
	Energy vs 1	F1ux						٠			103

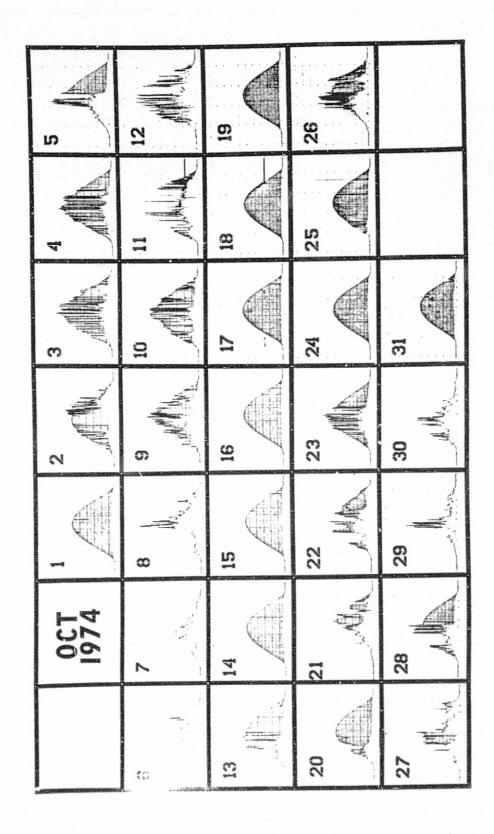




ORIGINAL PAGE IS OF POOR QUALITY



ORIGINAL PAGE IS OF POOR QUALITY



ORIGINAL PAGE IS OF POOR QUALITY

FLUX DATA

Legend:

0

TIME: Local time in hours and decimal fractions

of hours

DN: Direct Normal

TH: Total Horizontal

TH-1: Total Horizontal with OG1 Filter

TH-2: Total Horizontal with RG1 Filter

TH-3: Total Horizontal with RG8 Filter

SH: Scattered Horizontal

SH-1: Scattered Horizontal with OG1 Filter

SH-2: Scattered Horizontal with RG1 Filter

SH-3: Scattered Horizontal with RG8 Filter

All data in units of watts/m²

	DATE	10 AUG	1974	LOCATI	ON: 857	10A				
	TIME	DN	TH	THI	THE	TH3	SH	SHI	2HS	SH3
	6.50	· O •	0.	0.	. 0.	.0.	0.	0.	0.	0.
	6 - 67	488.	кз.	61.	53.	43 -	37.	21.	15.	13.
	6 . 83	549 .	116.	83.	73.	60.	44.	24.	17.	15.
	7.00	598. 638.	143 .	103.	91 •	76.	45 •	27.	18.	16.
	7.33	669.	207.	126.	109.	93 •	44.	25.	19.	15.
	7 .50	697 •	242.	173	148.	109.	, 50 .	89.	80.	16.
	7 - 67	717.	274 .	195.	168.	144.	50 • 49 •	30 ·	20.	18.
	7 . 83	741 .	312.	580.	189.	164.	54.	30.	88.	17.
	8.00	756 .	346 .	246.	808.	183.	55.	33.	24.	19.
	6.17	774 .	378 .	269.	228.	199.	55	33.	23.	19.
	8.33	789.	414.	294.	250 •	218.	61 .	37.	25.	82.
	8.50	798.	446.	315.	268.	236.	59.	36 .	25.	.08
	8 - 67	810.	482 .	339.	288.	253.	64.	36.	26.	55.
•	8 • 83	823 •	515.	368.	308•	271.	64.	37.	27.	21.
	9.00	838.	547.	384.	327.	288.	66.	37.	28.	85 •
	9.33	854.	575 ·	405 •	346 •	305.	67.	39.	28.	23.
	9.50	868.	632.	445.	364.	320. 336.	63 •	37.	27.	88.
	9.67	874 .	661 .	464.		330.	64. 63.	38 ·	27. 27.	51.
	9.83	889.	690:	485 .	416.	367.	71 .	42.	32.	20 ·
1	10.00	887 .	710 .	499.	426 .	378.	63 •	39.	27.	21.
1	10.17	885 •	731 .	516.	439.	391 .	68.	38.	.29.	21.
	0.33	887 .	755 •	531 •	454.	402.	67.	41 .	88.	24.
	10.50	909.	779.	546.	458.	414.	67.	40 .		21.
	10.67	923 •	804 •	567.	485 •	429.	68.	40.	28.	22.
	0.83	914.	819.	575 •	493 -	435.	64.	37.	88.	* 02
	11.00	921.	834.	387.	501 •	445 •	66 -	37.	27.	50.
	1.33	935.	870 •	598 ·	514.	454.	63 •	36.	25.	20.
	1.50	934.	886 .	621.	524 ·	463. 473.	65 •	37.	25.	. 50 •
		931 •	885 .	623.	533.	473.	65.	37. 36.	25.	50.
. 1	1 .83	924 .	888.	624.	534 •	474.	64.	37.	.86.	51.
	S .00	934.	899.	632.	541 .	479.	62.	36.	25.	20.
	2.17	929.	908.	636 •	548.	483 .	. 69.	40 .	29.	55.
			913.	642.	550.	488.	69.	40 .	29.	23.
	2.50	943.		644.	555.	490 •	69.	40 .	30.	23.
	2.67	934.	917.	644.	554.	489.	68.	40.	. 28.	23.
	2.83	958 •	903.	635.	546 .	482 .	71 •	41 .	30.	23.
	3.00	926 •	902 •	634 •	545 •	482.	-99.	42.	-99.	-99.
	3.33	930 •	901 •	634 -	544 •	481 .	-99.	42.	-99.	-99.
	3.50	949.	891 •	625. 627.	537 •	474 .	68.	41.	30.	22.
	3.67	947.	888	621.	541 · 534 ·	476.	65.	36.	26.	. 21.
	3 . 83	940 .	863 .	608.	523.	461 .	66 • 63 •	39.	28.	24.
	4.00	925.	850 +	598.	515.	453 •	69.	42.	29.	20.
	4.17	914.	819.	577 .	495 .	437.	66.	40 .	27.	81.
	4.33	909.	805 .	568.	487 .	430 .	70 .	43 .	29.	55.
	4.50	898.	788 •	555•	475 .	419.	73.	45.	31.	24.
	4 - 67	889.	778.	549.	471 .	415.	87.	55.	39.	31 .
	4 • 83	909.	771 •	544.	466.	411.	89.	58.	40 .	31.
	5.17	794.	732.	. 517 •	443 .	390 •	81.	53.	35.	27.
	5.33	11.	104.	73.	265.	185.	-99.	67.	49.	-99.
	5 • 50	858.	655	464.	398.	60. 351.	99.	69.	51 •	39.
	5 . 67	857.	601 .	454	390 •	342.	106.	72 • 82 •	45 · . 52 ·	36 •
	5 . 83	8.	83 .	56 •	47.	47.	88.	55.	42.	41 · 34 ·
î	6.00	660.	506 .	359.	309.	72.	136.	104.	67.	55.
	6.17	791 .	575 .	408 .	350 .	305.	153 .	121.	77.	62.
	6.33	770 -	542	385 .	330 •	288.	153.	127.	78.	62.
		50	95.		56 •	58.	97.	63.	50 .	41.
	6 - 67	0.	75.	52.	43.	41.	84.	55.	42.	32.
	6 - 83	3.	69.	49.	41.	39.	81.	51.	40 •	32.
	7.00	467. 690.	250.	239.	154.	136.	104.	88.	49.	38.
	7.33	680 •	289.	239	206.	180.	114.	111.	49.	40 •
	7.50	673 .	256.	184.	177. 159.	154.	97.	101.	40.	31 •
	7.67	640%	818.	153 .	132.	115.	95 ·	89.	37. 32.	30 •
	7 . 83	609.	172.	125.	109.	93.	71.	76.	25.	20.
1	6.00	596 .	140 .	103.	88.	77.	63.	69.	50.	17.
	B . 17	555.	108.	81 .	69.	60 .	57.	58	18.	14.
	8.33	517.	e1.	61.	52.	45 .	49.	47.	15.	11.
	B • 50	422 •	51 •	39.	35.	30.	38.	38.	13.	11.
	R • 67	365 •	36.	27.	23.	80.	3:2 •	25.	10.	8.
	B • 83	860.	18.	16.	13.	18.	23.	17.	8.	7.
	9.00	159.	10.	10.	10.	6.	16.	11.	6.	6.
	9.33	10.	3.	3.	3.	4.	12.	5	4-	3.
	9.50	0.	0.	0.	3 · 0 ·	0.	9.	3.	1.	8.
	10			,,,,	٠.	٠.	٠.	0.	0.	0.

	DATE	11 AUG	1974	LOCATION	85710	A				
	TIME	DN	TH	THI	TH2	тнз	SH	SHI	5Н2	SH3
-	6.50	υ.	.	Q +	U٠			ں. 17•	٥. 11.	ى. 10•
	6.67	501 •	77 •	57 •	49.	41 • 60 •	31. 43.	25.	18.	16.
	6.83	556 •	113	81.	72 . 89 .	75.	44.	24.	18.	15.
	7 -00	508 •	142 •	184.	104.	91	45.	94	18.	15.
	7.17	643 ·	207	146 •	127.	108.	48.	87.	19.	16.
	7.50	700 •	240.	169.	147.	125	48.	28.	19.	15.
	7.67	787 .	873 .	194 •	165.	144 •	51 -	27.	19+	16.
	7.83	751 •	309.	. 817.	187.	161	51 •	29. 27.	80 • 80 •	18. 15.
	Ř •00	776 •	344 •	243.	.207 •	181 • 201 •	50. 52.	29.	20.	16.
	P 17	795 •	382.	292 •	247	216	51 .	28.	21.	17.
	₹+33 # 60	607 • 621 •	413 - 446 -	314.	267.	234	54.	29.	21.	16.
	8.50 8.67	635	481 •	339•	289.	253 -	57•	31 •	22.	17.
	8 . 83	844.	512.	361 .	307.	271 •	58+	31 •	22.	17.
	9.00	B55 •	544 •	384.	327•	287•	60 •	33 +	88	18. 17.
	9.17	863 •	576 •	404 •	347 •	304+	59. 62.	32. 34.	23· 24·	20
	9.33	875 •	608 •	428.	365.	323. 336.	61 •	33.		18.
	9.50	883 •	633.	447 • 464 •	381 • 399 •	351 •	64.	37.	24 •	21 -
	9.67	886 •	663 • 690 »		416.	367.	66.	36.	26.	`so• •
	9.83	889 • 896 •	716 •	503	431 •	381	67.	38.	27•	22.
	10:17	890 •	738	517	446 .	393.	72•	40 •	30 •	23 ·
	10.33	908	767 .	541 •	464.	-408 ·	77 -	45.	31.	25. 23.
	10.50	906 •	786 •	552 •	473 •	417.	76 •	45. 36.	30. 27.	20•
	10.67	910 -	800 •	563 •	483 -	425 •	67• 73•	41 •	28.	.21•
	10.83	907 •	811.	572	489. 502.	432. 443.	78.	42 •	29.	22.
٠	11.00	918•	834. 849.	586 • 597 •	511.	453	74.	41 -	28.	55.
	11.17	916 • 924 •	863 •	607 -	582	460 ••	73 •	42 •	26.	20+
	11.50	924	874 -	614-	527.	466 •	72.	42.	29:	81.
	11.67	923	883 ·	519.	535•	471 -	77.	44 •	30 •	24. 21.
	11.83	927 •	893 -	630 -	540 -	477 •	71 •	40 • 45 •	28. 31.	25.
	18.00		902 •	635.	546	481 +	78. 804	46+	31.	86.
	12.17	923 •	908+	638•	549 ·	483 • 489 •	79	46.	31 -	24 .
	12.33	938.	917. 920.	648 •	555+	490 •	87	54 .	37.	30 -
	18.50 18.67	930 • 920 •	980 •	647.	557 •	491 •	93	58.	39•	30 •
	12.83	920 •	905 •	635 •	545	481 -	77•	48.	31 •	24.
	13.00	924	900 •	633.	546 •	460 •	81 •	49.	32 •	26+
	13-17	915	691 •	626 •	540	476 •	79•	49. 51.	30. 31.	23 · 24 ·
	13.33		877 •	61.6+	530	467 •	61 • 87 •	54 +	33 •	26.
	13.50		875 •	614÷	527 • 520 •	465 • 459 •	86.	57 •	35 -	27.
	13.57		663 • 846 •	595•	512	452	90 •	61 -	36.	29.
	13.63 14.00		839.	598 -	508	447 •	99.	69.	41 -	38•
	14.17			582	500		108 •	74.	43 -	33 •
-	14.33			567•	488	429.	109.	61.	45∙ 56 <i>•</i> ~	36 • 45 •
	14.50		789.	556+	479 •	419.	129. 140.	97. 111.	63 •	50
	14.63			564	484 • 451 •	425 • 396 •	116		47.	38.
	14.83				432	380 .	111.	96 •	44.	34
	15.00			~	415	365	111.	99•	48.	34.
	15.33				398.	350 •		100	39.	30 •
	15.50		535		385.	338.	103 -	108	37 • 36 •	28. 27.
	15.57				367.	383	104. 113.	113. 124.	37.	30
	15 - 83				348. 330.	307 · 289 ·	117	134	39.	30 •
	16-09				313.	274		104	43 •	33+
	16 • 17 15 • 33				845	219	125.	135.	40 •	35 •
	16.55				277 •	242.	130 -	155.	40.	35 •
	16.6			52.0	259.	886 •	139.	157 •	.45	37.
	16.83				237•	207 •	141 •	156 • 155 •	40 •	34. 31.
	17.00				516+	186. 170.	138. 141.	153	40.	33 4
	17.1				195. 116.	105	97.	99	31 •	24.
	17.3				112.	99	106	101 •	28.	55 •
	17.59				181.	105 -	115.	110.	28.	21.
	17-8				109.	98 •	118.	106.	3.7	25.
	18.0			. 105.	91•	79		92.	31 •	24. 14.
٠	18.1	7 5	. 30	23.	19-	50.	43.	25.	18.	12.
	16.3	3 5			15.	15	34- 41+	19. 27.	13.	10.
	18.5				24 • 20 •	82. 17.	34.	88.	11.	8.
	12.6				11.	_ '	50.	12.	7.	R .
	18.8 19.0				е.		18.	9.	6.	6.
	19.1				5.	S •	10 -	4.	1.	3.
	19.3	•	_	. 1.	밥 •		5.	8.	1.	2.
	19+5				0.	0.	.0.	0.	0.	0 •

DATES	18 AU3	1974	LOCATIO	N: 8571	DA .		•			
7 J HÖE	DN	TH	THI	THR	TH3	SH	SHI	SH2	SH3	,
6+50	0.	o.	.0•	0.	0.	0 -	٥.	0.	0.	1
6-67	493	61 •	46.	36+	31 •	88.	6.	4 • 20 •	17.	
6 • 83	547 •	114.	62. 109.	75 • 95 •	61 • 80 •	53 • 60 •	29. 34.	25.	ei.	
7.00 7.17	601 ·	151 •	125.	107	91 -	52.	27.	18.	15.	
7.33	679	203 •	146.	128.	108.	57 •	27.	18.	15.	1
7.50	715.	240 •	170 •	145.	125+	55•' 57•	28. 27.	17. 18.	16. 14.	
7 - 47	740+	273 • 307 •	193. 818.	165.	143.	63.	84.	18.	16.	
7 • #3 8 • 00	175K+ 176+	336.	239.	205	178.	60+	28.	19.	15.	
8.17	797	378 •	263 .	225	196 -	65 •	29.	19.	16.	
B • 33	811.	407 •	286 •	247.	214.	69. 72.	32. 33.	21.	17.	;
R+50	830 •	442 ·	312 ·	866 •	234 · 251 ·	78.	35.	23.	20	
8 • 67 .8 • 83	831 • 843 •	502	354.	303 -	266.	76 •	33 •	22.	17.	
9-00	854	537.	378.	324	884.	81 •	36.	24.	20	
9.17	855.	562 •	395•	339•	298• 321•	82. 94.	37• 44•	24. 28.	18. 25.	•
9.33	886	602 • 634 •	426 • 446 •	367 • 386 •	337.	100.	46.	31.	28.	•
9•50 9•67	884 • 889 •	55B•	460 •	399	354.	93 •	47.	32.	86.	
9 - 83	R70 •	704 •	493 •	426 •	376.	113 -	57.	45.	37. 23.	
10.00	892.	708.	194.	427.	378. 389.	98.	46. 48.	30 · 31 ·	24.	
10-17	907 • 898 •	730 • 752 •	510. 525.	439 - 454 •	402	99.	51.	33 •	24.	
10.33 10.50	897.	772	539.		412.	102.	53•	33 -	25.	
10.67	898.	791 •	554 •	478 -	423 •	104-	56•	37+	29. 28.	
10.83	892 •	807 •	563 •	486.	430 • 440 •	112.	60 • 61 •	38. 37.	28.	
11.00	900 • 904 •	823 • 839 •	576 • 586 •	496 • 506 •	440	112.		37.	27.	
11.17 11.33	903 •	854	597 •	516.	458	114.	65 •	36.	29.	•
11.50	911.	868	697 -	525 .	465	117.	67•	38.	29.	-
11.67	914.	878	615.	531 •	470 •	114.	69 . 67	39• 38•	30 ·	
11 - 83	910.	683 • 697 •	617.° 625.	533 • 539 •	473. 478.	114.	66	37.	28.	
12.00	920 • 918 •	896	627	543 •	479+	107.	68	36.	27.	
18 33	923	902	631 •	544.	483 •	105-	69 •	37•	28.'	
12.50	929.	905 •	632	547 •	484 •	108. 107.	74. 75.	38. 37.	28. 28.	
12 - 67		903 • 897 •	628•	546 • 541 •	483 • 477 •	109.	77.	37.	27.	
12.53	- 915 • 907 •	884	619.	535•	473 •	110.	82 •	38.	88.	
13.17	911.	882 •	618.	533 •	472.	114-	87 •	40 •	31.	
13 - 33	911 •	878 •		529•	470	116. 124.	94.	39. 43.	28. 32.	
13.50	910 •	672 • 851 •		528. 516.	467 • 457 •	125	104	40 •	31 •	,
13.67 13.83	903 • 899 •	835		505 •	448	127.	111.	41 -	31 •	•
14-00	894•	619.	575 •	496 •	439 -	131 •	119.	40 •	29.	
14.17	890 •	801 -		484 •	428 418	135. 137.	130. 136.	41 • 40 •	27.	•
14.33	885. 877.	782 • 762 •		473 • 459 •	407	140 -	146.	41 -	28.	
14.50		746		452 -	399	144.	.154 •	42 •	30 •	
14+83	873 -	727.	508	438.	388•	154	169.	44 •	33.	
15.00		704 •		425+	377 •	166+	182.	45. 42.	32. 32.	
15 - 17		675 • 647 •		409• 393•	362 • 348 •	171 •	202	42.		
15.33 15.50		616.		374.	338	180 •	808.	48.	32.	
15.67	849.	589•		358.	315+	182.	216.	39.	31. - 29.	
15.83		565 •		342. 325.	304 • 287 •	192. 202.	223. 223.	38. 38.	29.	
16 • 00 16 • 17		534. 501.		305.	269	204	ssu.	37.		
16.33		465 •		285.	250 •	209.	227.	35.	28.	
16.50	607			265•	53%•	810.	583.	34.	26•	-
16 - 67				244.	215. 195.	215.	217.	34.	25. 25.	!
16 - 83 17 - 00	771.		2	503 ·	178.	205	194.	32	23.	i
17-17	719			178.	158.	190 •	175 •	31.	23.	
17:33	711	263	184	162.	140 •	182.	162	31.	20 •	
17.50	691			141.	126.	164 • 148 •	128.	29• 28•		-
17 - 67				121.	107. 88.	128	107.	25.	16.	ė.
17.63 18.00			_	64.	73.	109.	89.	25.	17.	•
18-17			. 74.	47.	58•	88.	72.	23.	16.	
16.33	518	77		50 •	43 •	- 66 • 43 •	55. 39.	20. 17.	12. 11.	
18.50				34 • 21 •	30 • 19 •	27.	56.	13.	9.	
18.47 18.43				13.	- 11.	16.	- 16.	9.	8.	
19.00		11	. 6.	FF.	5 •	4.	7.		4.	
19-13	7 4			3 -	3 · 0 ·	0.	4.	3 0	e .	í
IS19.33	3 0	. 0	• 0.	. 0.	. "				. Yes	,
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	DATE:	13 AUG	1974	LOCAT 10	N: 85710)A	•			
	TIME	DN ⁻	TH	THI	THE	TH3	SH	SHI	\$142	5H3
	5 • 50	0.	0.	٥.	0.	0.	0.	0.	0 •	0.
	K • 67	ABA.	κο.	55.	50 •	43 .	44.	88.	16.	13.
	6.63	541 .	107 •	75 •	67 •	59.	53 •	26.	1P.	15. 15.
	7.00	593•	137.	97.	85 •	74.	63 • 69 •	28. 28.	19.	15.
	7 - 17	453.	17.6.	117.	101:	87. 107.	£0.	31	81	16.
	7.13	668 •	800 •		121 • 141 •	124	86	32.	22.	17.
	7 - 50	449. 706.	233. 245.		160 -	140	96 .	37 -	23 •	17.
	7.67		304 -		182.	160 .	110.	. 42 •	28.	21.
	8 00	738.	363.		217.	191 •	45.	64 •	44.	35• 35•
	8.17	746.	391 .		235•	206	150 •	65 •	44 • 70 •	58.
_	8.33	205 •	235•		135 •	119.	157 • 176 •	90 · 124 ·	101 -	83 •
	R+50	49•	505•		93 • 150 •	110 ·	121	77.	61 -	45.
	8-57	205 •	177.		310.	274	183 •	77.	49.	39.
	P #83	793 - 796 •	520 • 553 •		331.	294	198.	67 •	55 •	43 •
	9-00	794	557		395+	349.	263.	129.	90+	73 -
	9.33	255	417		886.	863•	312.	167.	186+	104
	9.50	77.	3 85 0		358•	349+	398.	216. 157.	159. 110.	89
	9.57	800 •	773		468 •	412.	-99. 217.	89.	45	34 .
	9 • 63	٤43 •	641		405 •	361. 375.	881.	89	41 .	32 •
	10.00	865+	704		420 · 435 ·	388	229	95 -	41 .	31.
	10-17	845 -			451 •	401 -	233 •	99.	43 •	34.
	10.33	872 - 881 -			461 .	410 .	238.	100 -	42 •	38•
	10.57	887	i		473.	428	244.	107.	42 •	32. 32.
	10.83	892		. 563 •	484 •	438 •	248.	113.	43 - 45 -	34
	11.00	682 4			490 •	437 • 444 •	249 • 253 •	118.	44.	33
	11-17	892			500	452 -	24R	123.	43.	33.
	11.33	901			508• 516•	460 •	252 •	.127 .	41 .	31 -
	11.50				522.	465 .	255 •	134-	42 •	33 -
	11.67	902 · 916			526	472 .	255.	137.	42 •	32.
	11.63				529•	473 .	246.	140 -	40 -	32
	18-17	_			529•	472.	241	144.	43. 43.	32• 31•
•	12-33				532 -	474 •	242.	149. 155.	41.	. 33.
	12.50	915			533 •	475.	242• 236•	159	41.	32 -
	15.44				530 • 532 •	473. 472.	241	170 -	43 •	31 -
	12-83				526	. 472.	248.	179.	43.	31 +
	13.00				525 -	468 .	253.	194 .	42.	34 •
	13.17				522 •	464.	260.	205•	43.	36+
	13.50					458.	863 •	217.	46 •	34. 33.
	13.57					452 .	271 •	225. 243.	45 •	341
	13.83					446 • 438 •	282 •	249	44.	38
·	14.00					427.	295.	267.	44.	35.
٠	14-17			_		420 .	308+	560 *	44.	34+
	14.30					407 •	318 •	292 •	44.	34 •
	14-6				444•	393.	381 •	299+	43.	34. 33.
	14-8			1. 505.	433	362.	332	310 · .	46. 49.	40 •
	15.00					369 ·	341 - 343 -	317.	45.	35.
	15-1					348.	364 •	326		40 •
	15.3					328	357	319	45.	35.
	15.5					315	361 •	321 -	45.	30,
	15.8					295 •	358+	311	45 •	33 ·
	15.0	/ ·				277.	355•	301 •	45.	32·
	16.1	7 820				266	352. 339.	296 • 279 •	44.	31 •
	16.3					. 245 · 231 ·	331.	268	an.	31.
	16.5						317.	252 •	46.	31 •
	15.5						898.	234.	49.	35.
	15 · 8		-	2.2.			276 •	216.	52 •	34.
	17-1				. 174.		246.	1 90 .	50 •	32 · 31 ·
	17.3		g. 25	io. 176				168.	50 ·	28.
	17.5		• • • • • • • • • • • • • • • • • • • •	5. 152				126.	45.	86.
l	17.6							105	44	24.
, I	17.1			19. 105 23. F6				87 •	41.	* ES
١.	18 0			94. 65				66 •	34.	19.
	18-1 18-3			9. 25		. 24.	34.	28.		16.
	18.			56. 41	. 35			40 •		19.
	1846		1. 8	25. 14				15.		8.
	18.0	K3 15		20 • 13				14.		4.
	1940		7.		5 5 4			3 .	-	3.
	19-1		2	-	2	_			l.	0.
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	DATE	EUA OS	1974	LOCATIO	M1 6531	UA				
	TIME	DN	TH	THL	2HT	TH3	SH	SHI	SH2	5H3
	6.00	0.	0.	0•	0.	0.	0.	0.	0.	٥٠
	6.17	127.	9.	6.	ě٠	8.	11 •	10.	6 •	₽ •
	6.33	869.	19.	15.	15.	14.	16.	18	7.	8.
	6 - 50	379.	39.	27.	86.	83.	18.	13.	\$. 30.	5.
	6 - 67	478 •	63 •	44.	39.	36+	25. 29.	16• 18•	12.	5.
	6 - 63	545.	92 •	65.	56.	50 • 64 •	86 •	18	12.	6.
	7.00	599.	117. 158.	54. 106.	72 • 93 •	81 -	29.	17.	18.	6.
	7 • 1 7 7 • 3 3	644• 657•	185	132 -	118.		32.	20.	14.	10.
	7 - 50	722.	223	157 •	133.	117.	34 -	80.	14.	10 -
	7.67	741 -	258	161.	154.	136 •	36+	22.	14.	6 •
	7 - 83	761 -	292 .	206•	175 •	153 •	36.	23.	15.	10.
	8∙00	780 •	321.	226•	191 •	170 -	37•	25.	17.	9.
	8-17	508	361 •	255•	216.	190 •	41 •	25• 23•	17. 16.	18. 11.
	5.33	615.	393+	276.	237 • 256 •	207 • 22 5 •	35° 48 •	24.	18.	ii.
	8 - 50	83 5 • 543 •	431 • 468 •	304. 324.	277.	244.	44.	25.	. 15.	11.
	8+67 8+63	858•	499	349.	297.	268	42.	25.	15.	12.
	9+00	880 •	529.	372.	317.	. 089	36.	84.	16.	9.
	9.17	682 -	561 .	395 •	334.	295 •	40 •	24.	18.	11.
	9.33	893 •	592 •	415.	355+	314.	43 •	25.	<u>≨B</u> +	12.
	9.50	906 •	624+	436.	375 •	333•	48+	29.	15.	13.
	9 - 67	898.	643 •	451 •	357 -	343•	46+	25. 31.	20 • 19 •	16. 15.
	9 • 53	908•	672 •	472 •	405	356 • 375 •	47 · 49 •	32.	19.	16.
-	10.00	924•	709.	497 • 512 •	427• 437•	387•	51 -	31.	21.	13.
1	10-17	"922• 941•	727 • 755 •	530.	453 •	399	43 •	26.	18	13.
	10.50	932	767.	536.	460 •	405	52 •	29.	. 08	15.
	10.67	945	794 •	559 •	461 •	425.	50 •	31.	21.	15.
	10 - 83	944.	B10 .	570 -	469.	430 •	46+	254	17.	11.
	11.00	951 •	828•	562.	500•	440 •	44.	86.	17.	11.
	11.17	957•	847 •	595.	511.	451	42.	27.	15. 20.	14.
	11.33	966 •	865 •	608•	523 • 525 •	461 •	45 • 43 •	30 • 26 •	17.	iī.
	11.50	964	875 • 882 •	615• 620•	533.	470	50 •	29.	21.	14.
	11.67 11.63	961 • 961 •	886 ·	624	536 •	474		87.	19.	12.
	12.00	962	696 •	630 •	541 .	478.	46 •	25.	19.	13.
	18 - 17	96B+	903 •	634 -	547 •	488 +	46 •	28.	ış.	18-
	12 -33	954 •	896 •	630•	542 •	480 •	46.	25.	19.	13.
	12.50	964 •	904•	637	545 -	483 •	45-	29.	16.	11. 12.
	18 67	954-	697 •	633 •	540 •	479	43 •	26. 30.	17. 18.	13.
	18 - 53	968•	906 •	639•	547• 537•	484 • 475 •	48- 47•	31.	20 •	18.
	13.00	949• 963•	893 • 900 •	628• 633•	545-	480	49.	31.	21.	13.
i	13 - 17	968 •	885	623	536	473 -	49.	30 -	20.	, 13.
	13.50	949.	885 •	628+	536 •	473 +	56.	36.	26.	18.
	13.67	915.	873 .	614-	526 •	466 •	63 •	55.	41 •	30 -
•	13 - 63	921.	881 •	68 I •	532 •	471 •	104.	.69•	54+	40+
	14.00	931 -	863 •	611.	523•	461 •	91 •	61 • 105 •	44 • 82 •	31 • 64 •
	14-17	35+	173 •	117.	100 •	94. 433.	154 • 61 •	54.	41 •	30 -
	14.33	β69∙ -99∙	-808 -	572 • 565 •	491 • 485 •	427.	64.	40 -	29.	81.
٠	14-50	922.	745•	527 •	454+	401 •	50 •	34 .	-99	15.
•	14-83	916	720 •	508	436+	385 .	51 •	30	81.	14.
	15.00	906+	697 •	492+	424	373 •	52 •	34.	£3 •	16.
	15-17	896+	680 •	480 •	412.	363•	64 •	42 •	30 +	22.
	15.33	890 •	640 •	452	388•	343 •	50 •	32.	21. 19.	14.
	15 - 50	B76 •	607+	428•	368+	364. 309.	47 • 54 •	89. 34.	83 -	16.
4	15 • 67 15 • 83	661 » 656 •	577 • . 550 •	408 355	351. 333.	895•	54.	34 -	23.	17.
	16.00	847	518.	366+	316.	279.	54.	34.	24.	17.
•	16.17	848	487	343 •	294.	261 .	49.	34.	24.	16.
	16.33	833	454 •	320 -	275 -	844	50 •	32 •	81.	15.
	16-50	816.	413.	292 -	251.	.933	45+	29.	19.	18-
	16.67	\$02 •	3 63 •	270+	232.	205.	49.	30.		14.
	16 • 83	776•	346 .	244.	810.	185 •	47 •	31 •	19.	13. 13.
	17.00	:75	72 •	42.	31.	29.	44 • 42 •	25. 25.	17. 19.	11.
	17-17	19.	42+	28. 82.	23 • 21 •	26. 22.	42	27.	16.	iii
	17.33	7• 654•	36. 204.		126	111.	43 •	38 •	20.	14.
•	17.50	627			104	98 .	41.	34.	60 •	13.
	17.63	604			95.	51 •	47 •	39.	83 •	19.
	18.00	574.	129.	94.	82 •	71 •	55 -	43.	30 •	81 •
	18-17	524	91 •	64 -	56 •	51 •	44+	31.	21.	13.
	18.33				35+	31 •	30	₽3 •	12. 10.	6. 5.
l	16.50				84+	21. 11.	23. 15.	17. 13.	9.	4.
	15.67 15.83				14. 8.	5.	13.	8.	6.	5.
	19.00			4	6.	3.	5.	5.	Ă.	1.
	19.17			4	8.	Ö.	6.	e.	0.	Į.
	19.33				. 0.	0 =	0.	0.	0+	0.

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DATE	# 21 AUG	1 1974	LOCAT	ION: 85	710A				
TIME	DN	TH	THI	THS	THS	SH	SHI	5H2	5 H3
5.67	0.	0.	0+	0.	0.	0.	0.	٥.	0 -
5 · 83 6 · 00	2. 87.	6 • 9 •	1. 5.	. 8.	5.	. 5	4.	ġ.	
6.17	147.	19.	ii.	12.	9. 12.	1. 20.	11. 15.	7 • 8 •	3.
6.33	243.	31 e	81.	20.	1.5.	27.	15.	11.	5. 8.
6 · 50 6 · 67	343. 420.	49.	35.	32.	28.	31.	18.	13.	9.
6 + 83	458.	71 • 100 •	50 •	44 • 62 •	39. 55.	38.	19.	.14.	9.
7.00	540.	188.	70 • 89 -	78.	69.	35. 39.	84. 85.	16. 15.	10. 18.
7-17	592.	159.	1 1 3	97.	87.	45.	86.	16.	13.
7 • 33 7 • 50	629. 660.	229. 198.	134. 161.	116.	103 -	44.	26.	16.	14.
7.67	684.	261	182	137. 157.	122. 137.	49. 48.	32. 32.	21. 21.	17.
7 - 63		295	182 • 208 • 230 •	176.	156	54.	34.	22	16. 16.
8-00 8-17	731. 751.	368.	830•	194.	174.	53.	32.	24.	15.
8.33	766 •	3974	254 251 303	215. 234.	190. 210.	54. 50.	35.	23.	17.
8 - 50	777.	427.	303	256.	227.	49.	35. 33.	25. 25.	20. 16.
8 • 67 8 • 63	803. 810.	463 •	327.	278.	246.	51 ·	35.	25.	17.
9.00	821.	496. 530.	349. 372.	296. 315.	• <u>8</u> § §	51.	36.	27.	16.
9.17	830 -	557.	398	332.	280 . 296 •	52 • 56 •	36. 36.	27. 28.	18. 20.
9+33	645.	588 .	414.	351 •	312.	58.	37.	29.	22.
9 • 50 9 • 67	649. 864.	614. 643.	433.	366+	385.	52.	33.	26.	18.
9 - 83	856.	674 •	453. 474.	383. 402.	341. 357.	58 • 56 •	34.	87.	18.
10.00	669.	697	490-	418.	372	61.	37. 41.	28. 32.	19. 23.
10-17	873 •	719.	506.	430 •	383 •	57.	39.	30+	80.
10 • 33 . 10 • 50	878• 890•	735 • 759 •	517• 534•	438. 455.	390	57•	37.	26.	19.
10.67	898.	779.	548.	469.	405. 418.	54 + · 57 •	39. 39.	30. 30.	19.
10 -83	894.	792.	558.	475.	485.	55.	39.	30.	20·
11.00 11.17	902 • 897 •	816. 834.	574.	490 •	436 •	58.	39.	29.	80.
11.33	902	842 •	587. 591.	501 ·	445 - 448 -	65.	43 •	33 •	25.
11.55	905	858	603	513.	456	61 • 61 •	41 • 42 •	31. 32.	81. 80.
. 11 -07	900.	866 .	607.	517.	463.	68.	44 .	32.	23.
11 -83 12 -05	902. 905.	870 • 880 •	611. 618.	581.	464 -	64.	42.	33.	83.
12.17		683 •	620.	530 • 531 •	470 • 471 •	68. 71.	45. 47.	37.	27.
18 -33	905 •	887 .	622.	534 +	474	71.	47.	38. 39.	25.
12.50 12.67	904. 899.	892 •	626.	533.	474.	73 .	51 .	40 •	27.
12.83	897.	897 • 896 •	630. 632.	536. 540.	478. 480.	62. 89.	58+	45.	31 •
13-00	897.	895 .	629.	536.	478	91 •	68 • 64 •	49. 51.	35. 36.
13.17	878.	913 •	643.	548•	486 •	119.	63 •	65.	49.
13.50	892 • 894 •	894. 910.	631. 641.	539 • 545 •	479. 464.	107.	75.	60.	44.
13-67	876 •	886	625.		471 -	128. 126.	90 • 86 •	74. 70.	57.
13 - 83	B64 •	851 .	600.	512.	454	109.	77.	60.	51 • 47•
14.00	871 • 874 •	832. 610.	586•	498	445 •	102.	68.	56.	48 .
14.33	875 .	794.	570. 559.	483 • 1 474 •	433 • 484 •	93. 91.	62 •	46.	37.
14-50	536.	604.	443.	388.	359.	87.	59.	47. 45.	36. 33.
14-67 14-83	870	757•	534.	454.	404.	95.	62.	51.	36.
15.00	875. 856.	729. 722.	517. 512.	438 •	391 • 387 • '	85.	58.	44.	34.
15-17	834 .	696 •	490.	418.	372.	108.	75. 75.	62. 59.	47. 46.
15.33	626. 828.	677•	479.	407.	368.	115.	79.	63.	50 •
15.50 15.67	808.	641. 615.	453. 437.	387 • 373 •	343 •	107.	78.	61.	45.
15-83	602.	595.	424.	359	328. 319.	116.	79. 82.	63. 68.	47.
16.00	786 •	534.	381.	323	288	95.	64.	53.	54 • 39 •
16.17 16.33	757. 776.	465 •	345.	295	259.	84 •	59.	44.	35.
16.50	764.	465. 428.	330. 301.	282 • 260 •	249. 229.	76. 73.	53 •	41.	38.
16.67	740 -	388 .	278.	236.	210.	67 •	47• 48•	39. 37.	26. 30.
16-03	732.	362 •	258.	218	196.	69.	49.	38.	30.
17.00 17.17	704. 615.	327. 279.	235. · 197.	200 ·	177.	72.	51 •	38.	31.
17.33	654.	265.	187.	163.	151 • 142 •	73. 67.	50 • 48 •	42. 41.	31 •
17.50	7•	78 +	52.	43 .	41.	69.	51 •	39.	31 • 30 •
17.67 17.83	583 • 554 •	219.	158.	136	119.	84 .	62.	53.	48 •
18.00	493	179. 128.	131. 93.	114. 84.	99. 71.	77.	59.	46.	42.
18-17	471 •	86 -	61 •	55.	49.	55. 32.	40 • 28 •	32. 21.	26. 14.
18-33	417.	55•	40.	37.	33.	20.	19.	14-	9.
18.50 18.67	344. 831.	38• 85•	25. 16.	24.	20.	16.	14.	13.	. 7.
18-83	128.	14.	11.	14. 12.	14. 10-	17. 9.	10.	11. 8.	6+
19-00	1.	6.	4.	6.	6.	4.	5.	3.	6. 2.
19.17	0.	o.	1.	0.	8.	. 0.	0.	į.	0.
	~ T	. .	0.	0.	۰.	Û ¢	0.	٥.	0.

	DATE	22 AUG	1974	LOCATIO	DN: 857	ļ OA				•
	TIME	DN	TH	ŤHI	T#2	THO	SH	SHI	SH2	5H3
	5-67	٥٠		. 0.	0+	0.	0.	0.	0.	o.
٠	5 • 53 6 • 00	8 - 3 -	7.	8 • 5 •	6. 6.	8. 6.	0 • 3 •	8 • 5 •	3 • 4 •	: ·
	6-17	63.	ıė.	11.	11.	š.	Š.	1Ö.	9.	Š.
•	UU	886-	87.	19.	17.	17.	18.	15.	10.	6.
	6 • 50 6 • 67	263 • 370 •	38• 64•	29. 45.	86. 41.	22. 35.	R1 • 97 •	16. 19.	13. 15.	9.
	6 + 53	443 -	91.	65 •	54.	50.	30.	88	16.	12.
	7.00	505+	119.	80.	71 •	64,	31 -	23 •	17.	11.
	7.17 7.33	551 • 591 •	147 • 183 •	106• 129•	91 • 110 •	78 • 97 •	37. 39.	24. 26.	19. 21.	10 • 14 •
•	7.50	615.	214.	153.	128.	97. 112. 132.	41 -	89.	23	13.
	7 • 67	641.		175.	149.	132.	45.	89.	Ž3•	16.
	7 • 63 6 • 00	671 • 696 •	260 ·	198. 225.	167. 189.	146. 166.	46. 50.	29. 34.	23. 27.	14. 15.
	5-17	723.	358•	253 •	215.	166 • 188 •	56 •	36.	28+	19.
	6 • 33	743.		278.	235•	207.	66.	36-	29.	24.
	8 • 50 8 • 67	759• 755•	425 °	298. 327.	253 · 274 •	224 · . 245 ·	64 • 66 •	34. 37.	28. 29.	22 •
	8 - 63	BO1 •	494 .	350 •	296.	259.	66.	37.	28.	21.
•	9+00 9+17	608• 519•	525•. 558•	372. 392.	314. 331.	277. 292.	71 •	41 •	29.	84.
	9.33	827	588.	415.	352 •	311	69. 69.	37. 41.	29. 31.	25. 64.
	9.50	832.	616.	435 •	369.	326+	70.	41.	31 -	24.
•	9+67 9+83	835. 836.		451 • 468 •	383. 397.	339. 351.	78. 80.	44.	33 •	27. 27.
	10.00	846 -		490-	416.	367	84 •	43 • 46 •	33• 35•	29.
	10 -17	849.		506 •	433 -	383 -	86.	48.	36.	29.
	10 •33 10 •50	657* 657*		521 • 539 •	446. 461.	396. 406.	86 • 94 •	45. 56.	38. 41.	32. 33.
	10-67	857+	793 •	556.	476	421 .	103.	59.		36.
	10 -83	862 •	817.	579.	492.	437 -	111.	67.	53•	43 •
	11.00	867 • 873 •	837. 848.	590 • 601 •	506. 511.	448. 454.	118. 115.	69. 67.	54. 54.	46. 41.
	11 -33	706.	761.	540	466	417.	131.	83 •	63 •	53.
	11.50	804.	900 •	637 -	543.	481.	192.	124.	100 •	63 •
	11.67 11.63	724 • 652 •	843 • 940 •	598. 664.	500 • 564 •	443 • 500 •	189. 184.	123 • 119 •	102. 93.	84. 7 7.
	18.00	862	949.	673 •	571.	508	179.	112.	91.	78 -
	18-17	859+	1007.	713.	608.	535.	230.	151 .	124.	102.
	12 • 33 12 • 50	792 • 832 •	972. 1073.	683 • 761 •	562 • 652 •	510. 572.	253. 308.	171 ·	143 • 173 •	116.
	12 -67	766.	1025	730	628.	551	292.	801.	165.	135.
	18 - 83	844.	985 +	696•	596•	527.	123	146.	119.	96.
	13.00 13.17	609. 666.	949. 837.	672 • \$86 •	576. 497.	506 • 433 •	222. 257.	147. 170.	119.	94. 113.
	13.33	783 -			573 .	508 •			132	108.
	13.50 13.67	620 • 102 •		669 • 667 •	574 •	503 •	220+	142.	116.	96.
	13 · 63	701	362. 781.	260 • 547 •	217. 465.	201 • 410 •	311. 196.	209. 127.	174. 100.	142 • 80 •
	14.00	B45 •	867 •	613.	525•	463 .	161.	102.	64+	67.
	14-17	839. 820.	962 •	637• 686•		482 · 512 ·		140 .	114.	
	14.50	0.	295.	206.	583 • 174 •	159	302. 302.	205 • 206 •	173.	136. 144.
	14-67	15.	305.	214.	182.	165.	287.	199.	169.	140 •
	14 • 83 15 • 00	770 • 635 •	903 • 720 •	646 • 516 •	554. 445.	477. 383.	315. 240.	219. 165.	183 • 138 •	151. 115.
	15-17	777•	858 •	610.	523 •		300	207.	173.	146.
	15.33	653 •	749.	536.	461 •	399.	287.	198.	167.	140 .
	15.50 15.67	515. 107.	886 •	434 • 204 •	372. 175.	320. 154.	264. 226.	186 • 154 •	154 • 128 •	130.
	15 - 83	£3 •	239.	170.	47	133	196 •	133	108.	91
	16.00	680+	569 •	405 •	350 •	304	166 •	125.	101 -	87.
	16 • 17 16 • 33	630. 711.	522. 561.	374 • 401 •	323 + 345 •	279. 298.	192. 203.	130. 137.	107. 114.	90 • 95 •
	15.50	697.	527.	377 •	323.	280 •	200.	136.	112.	93 -
	16.67 16.83	685	479 •	343•	296•	256.	180 •	124.	102.	84 •
	17-00	650 • 31 6 •	414. 219.	296 - 176 -	255. 150.	820 - 133 -	158. 139.	106. 93.	87• 77•	73 . 64 .
	17-17	557 •	306+	216.	188.	161.	132.	86.	69.	58.
	17.33 17.50	565 • 520 •	265 · 231 ·	169. 168.	162.	140 • 126 •	109. 108.	70.	56. 56.	47.
	17.67	236•	145.	105.	92.	180.	98.	- 72 • 66 •	50 ·	47. 44.
	17 - 63	481 •	155+	111.	97.	81 •	89 •	55•	44.	· 38•
	18-00 18-17	373.	111. 39.	80 - 27 -	7.1 • 24 •	60 • 24 •	62. 45.	48+	33 • 84 •	29. 23.
	18.33	0.	30.	22.	20.	19.	35.	30 • 24 •	20.	.09
	18.50	٥.	29.	21.	81.	17-	30.	21.	17.	× 17.
	18•67 18•63	3. 45.	14. 8.	11. 5.	11 ·	8• 4•	13. 11.	5. 4.	6 ·	7 · 7 ·
	19.00	1.	i.	i.	1.	ī.	5.	Ö.	ő.	4.
	19-17	0+	0.	. 0 •.,	0.	0.	0.	0.•	ø.	٥.

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DATE	23 AUG	1974	LOCATIO	NI 85710)A			•	
TIME	DN	TH	ŤHI "	SHT	тнз	SK	SHI	SH2	SH3
5 - 67	ō.	Q+	۰.	0.	0	Ģ. 4.	5	o. 3.	0 · 5 •
5 83	2. 3.	3 • 5 •	- 1 • 5 •	3.	5.	3.	7.	Ä.	5.
6 • 0 <u>0</u> 6 • 1 7	175.	15.	12.	11.	9.	20.	8.	5.	11.
6.33	260 •	25.	21.	19.	14.	19.	12.	11.	10 -
6+50	372 -	40 •	30 •	29.	26. 35.	27. 32.	13. 16.	9. 11.	11.
6 • 67 & • 83	445 • 504 •	64 • 90 •	47. 65.	44 • 57 •	51.	32.	80	15.	13.
7.00	554.	117.		73 •	65 •	34.	19.	15+	13.
7.17	598•	155 •	110-	93 •	82 •	37•	21.	16.	14. 13.
7 -33	633 •	186 •	133.	113.	98. 117.	37• 47•	21 ·	15. 20.	18.
7 • 50 7 • 67	665 • 696 •	221 • 255 •	156 • 180 •	153 -	135.	43 /	27.	20.	17.
7 • 63	725.	290 •	205.	171.	150 •	47 •	23.	17.	15.
6.00	755.	326 -	230•	193 •	171 •	46.	26.	19. 19.	17. 16.
5-17	771 •	354 • 396 •	251 • 280 •	210. 235.	186 • 207 •	47• 53•	24. 30.	23 •	15.
8.33 8.50	787 • 805 •	428.	302	254	225.	46 •	29.	20.	10.
8-67	812.	462 •	326 •	277.	244	51 •	29.	24.	16.
8 - 83	831 -	494.	35! •	297.	260 •	49 • 54 •	32 • 33 •	21 • 24 •	15. 13.
9.00 9.17	841 • 848 •	530 • 556 •	373 • 393 •	314. 332.	278 • 295 •	52+	3.	25.	15.
9.33	853 •	584 •	414.	350 •	308.	57 •	33.	24.	13.
9.50	866·	617.	436+	371 .	325 •	58•	34.	23 •	15.
9 • 67	875 •	640.	455	382. 398.	340 •	55 • 57 •	29. 29.	24 • 24 •	11. 12.
9.83 10.30	879. 889.	666 - 693 -	473 • 488 •	413.	355 • 368 •	53 •	30 •	21.	14.
10.17	895+	715 •	507•	429.	380+	55 •	33 •	22.	14.
10.33	903 •	738 •	524.	443 •	394.	52•	31.	23•	14.
10 -50	899•	760 •	538 •	456 •	403 -	55 • 57 •	34. 32.	23. ·	16.
10 • 67 10 • 83	903 - 916 -	780 • 500 •	550 • 567 •	467 • 481 •	427	62 •	36.	25	15.
11.00	916	818-	579	491 -	435	64 •	38•	26+	16.
11-17	916.	632 •	585+	499•	443 •	57 •	33 •	25	16- 16-
11.33	916+	642 •	592. 601.	503• 515•	449• 453•	· 59 •	33. 38.	26. 28.	17.
11.50 11.67	920 • 920 •	854 • 863 •	511.	521.	459	61	36.	29.	16.
11 - 83	921 +	871 •	617	526 •	464•	65 •	35.	27.	19.
. 15.00	906+	874 •	616+	586•	463 •	69•	41.	33 i	21 · 17 ·
12 - 17	920•	881 •	621 • 626 •	531 • 534 •	470 · 472 ·	64 • 64 •	37• 38•	31. 28.	17.
12.33 12.50	920 • 921 •	886 • 888 •	627	532 •	472	70.	41 •	30	18.
12-67	917.	887 -	626.	532 •	471 •	75 -	41 -	32.	24.
12 - 63	915	889•	626.	536 •	475.	76 • 71 •	47. 43.	36. 34.	25. 21.
13.00 13.17	913 - 911 -	877. 872.	620. 618.	531 • 526 •	468 • 463 •	70	43 •	34 -	22.
13.33	916	671 .	617.	526 •	467 .	88 •	52 •	38•	25.
13.50	914.	B58 •	607•	519.	459.	78+	46.	37•	26.
13.67	908•	861 •	608•	517 • 498 •	459 t 441 t	69 • 72 •	57 • 41 •	44. 33.	29. 24.
13.83	904 • 893 •	625 . 813 .	583 • 577 •	493 •	433 -	76 -	44.	35.	21.
14-17	599.	787 •	559 •	475 •	420 .	64 •	40 •	28.	20.
14.33		780 •		469	417.	64	39. 41.	30. 31.	21. 19.
14-50		752 • 731 •	532. 519.	452 s 443 s	401 • 392 •	63 • 70 • .	44 •	33.	82
14.67		731	516.	440 -	388.	90	54 .	42.	30 •
15.00		727.	517.	446 •	387.	112.	74 -	60 •	48.
15-17		760 -	543.	464 • 157 •	406. 156.	160 • 163 •	111.	91.	79. 71.
15.33 15.50		218 • 645 •	168. 461.	391	342 -	110.	73 •	60 •	44.
15.67		110	75.	62 -	61 •	110.	74•	59.	44.
15.83	3 •	93 •	63•	50 •	53 •	95+	62+	50	36 • 50 •
16.00		543	389 • 400 •	332 • 343 •	291 •	122 ·	80. 109.	65 • 90 •	71 •
16 • 17		555 • 163 •	116.	99	89.	160	111.	95 -	77.
16+50				100 •	89.	155•	.110 •	92 •	73 •
16 - 67	0.			70 •	64.	109 •	78• 50•	6 4 • 40 •	50 · ·
16 - 83				41 • 32 •	40 4 28 •	72 • 60 •	39.	30.	21.
. 17-00 17-17		231 •	166.	149.	123.	59•	38•	31 -	21.
17.33	1 -	48.	32•	. 26.	25.	46.	32.	87•	19.
17.50		. 59•	40.	34. 47.	32.	58. 73.	39. 51.	32 • 43 •	24. 33.
17.67 17.83				36+	42. 31.	73 • 52 •	35.	32.	24.
18.00				26.	21.	39 •	24.	£1 •	16.
18.17	29.	38.	29.	28.	₽3•	37.	28.	23.	18
18-33				24. 9.	19.	25. 9.	19.	16	13.
18•50 18•67				7.	6.	4-	6.	ž.	1.
18-63				5 •	3.	3 -	3+	3.	0.
19.00			Ç.	0.	0 0	0.	0+	0 •	0+

OF POOR QUALITY

DATE	24 AUG	1974	LOCATIO	Nt 8571	-OA				,
TIKE	DN	TH	THE	THB	ŢH3	នអ	SHI	\$#8	SHO
5 - 67	Ú.	0.	0.	0.	0.	0.	0.	0.	0.
5 - 63	2.	3.	4.	4	2.	5.	4.	3.	Ó.
6.00	3.	9.	6.	7.	6.	18.	6.	6.	1.
6.17	164.	12.	10.	9.	7 •	15-	10.	6.	3.
5 - 33	281 •	25.	18.	19.	16.	17.	13.	8.	6.
6 - 50	370 •	45•	30.	89.	26.	ei.	13.	12.	6.
6-67	445.	63+	45.	41 •	35.	22. 34.	13.	18-	7.
6 • 83 7 • 00	502 • 555 •	91 • 120 •	67• 88•	59. 73.	49. 66.	31.	20. 19.	14. 14.	10 -
7-17	599•	147.	106.	92.	60.	-	18.	13.	8
7 - 33	638.	187 •	131.	112.	100N	42 -	24.	16.	10.
7 - 50	675 •	133	156.	130 +	115.	37.	24.	18.	10 -
7 - 67	704.	254.	181 -	154.	135.	45•	24.	16.	13.
7 - 63	723.	297.	210.	177.	154.	47.	28-	21.	13.
8.00	744.	330 •	235.	198-	175.	54 •	38+	25	16.
6.17	759-	383-	271 •	226.	199.	67 •	39.	31 • 30 •	23.
8 • 33 8 • 50	772. 500.	409 • 270 •	289 • 189 •	243. 159.	213 • 144 •	62 • 65 •	38. 37.	30.	21.
B+67	126.	151 •	97.	75.	76 •	BO •	53 •	42.	28.
B • 83	814.	510	364 •	303	268.	69 •	44.	32.	23.
9.00	829.	552 +	390 .	329.	289 .	75.	46 -	35.	25.
9-17	843.	564 •	399.	337.	296.	64.	35.	27.	19+
9 - 33	854 •	590 •	416.	351 •	309.	\$7 •	34.	27.	16.
9 • 50	862 •	614.	435 •	370 •	326.	59 •	32•	24.	16.
9 • 67	868•	638	452 •	380 •	338. 353.	53 •	32.	22 • 84	16. 16.
9 • 83 1 3 • 0 0	874. 881.	669 • 691 •	471 • 487 •	401 • 413 •	367 •	56 • 56 •	34. 89.	24.	12
10.17	892 -	723	507	433 •	384	57+	33	26.	17.
10 -33	897.	738	522 •	444.	391 .	53 •	33.	22.	15.
10.50	902.	760 -	534.	456 -	405.	57.	34.	24.	17.
10 -67	904 •	761 •	550•	467 •	416.	57.	38•	25.	15-
10.83	906 •	798•	561 •	480 •	423.	62 •	36.	25.	16.
11.00	909•	B10 •	574 •	486 -	432 •	59•	32.	25•	15.
11 -17	913-	B30 •	588•	500 •	444. 448.	62.	37. 34.	27. 27.	19. 15.
11 -33 11 -50	917. 910.	840 · 852 •	592. 602.	506• 512•	453 •	61 • 63 •	38.	29.	18
11.67	909	859	608.	518.	457 •	66 •	35.	27.	18.
11.83	909	863	608	519	461 •	63 4	39	28•	17.
12.00	908.	868.	614-	524.	464.	68+	39.	.29.	19.
12-17	90,9	670 •	616.	526.	465.	69+	36.	27.	19.
15.33	909.	877 -	619.	527.	468.	71 •	40 •	30•	• 03
12.50	897•	875	619.	527.	467 •	73 •	43 •	32.	22.
12 - 67	895 •	878	621 •	530	470 .	82 • 93 •	50 a 57 •	37. 44.	26. 31.
12 • 83 13 • 00	892 • 880 •	687 • 894 •	627• 632•	534. 538.	473 • 476 •	112.	69.	54 -	40 +
13.17	876	921	653 •	557•	492.	149.	98.	78.	57.
13.33	808.	852	60B-	519.	461 .	180 .	75.	61 .	44.
13.50	870 •	849	601 -	511 •	453 .	96 •	60 ·	45.	30.
13.67	671 •	831 -	589•	500 •	448.	91.	53+	40 -	27.
13-63	866 •	820 •	581 •	494 •	437.	95 •	57•	43 •	29.
14+00	866+	791 •	562 •	479.	424 •	74 •	45. 39.	32. 25.	20 • 18 •
14-17	859 ·	776.	550 • 534 •	468. 455.	413.	70 • 65 *	38.	28.	17.
14.33	872 • 863 •	737.	523.	444.	393.	63 •	36+	27.	16.
14.67	858.	710.	504.	429.	380 •	63 •	37.	27.	16.
14-83	854+	685 •	486 -	413.	365 •	60.	34.	25.	15.
15.00	857 •	663 •	471 -	401 -	354.	60 •	34.	25.	15.
15-17	652.	644	456 •	390 •	344 -	63 •	37.	27.	17.
15 - 33	846•	615	435	370 •	327.	55•	32.	23.	13.
15 - 50	838.	585 •	417• 398•	354. 341.	313 • 300 •	58. 64.	33. 38.	24•. 28•	14.
15.67 15.83	627 ·	559. 532.	380.	324.	283 •	60.	32.	24.	16.
16.00	805.	499	356.	303	267.	60 •	36 •	26.	16.
16-17	795 •	474	339.	291 •	256	70 •	45 •	34.	24.
16.33	761 •	477 •	340 +	290 •	254,	105.	70 •	54.	40 •
16.50	762 •	428•	306•	568•	231 •	86 •	55+	43 •	31.
16 - 67	786.	370 •	266•	228.	198+	68•	39.	30 •	22
16 - 83	711.	336	242. 228.	207.	161.	67 • 80 •	42 • 49 •	32. 38.	22.
17.00	687 • 668 •	318. 288.	205,	195. 176.	152.	81 s	51 •	41.	31 •
17 33	646•	239	171 •	147.	128.	59.	39.	86.	19.
17.50	615.	201	43 •	124.	110.	59.	39.	86.	17.
17.67	563.	168	123.	107.	92.	59.	36+	28.	21.
17.83	547 -	138 •	96.	86 -	74.	48.	30 .	23.	17.
18.00	509.	102 •	76.	66.	57.	43 -	29.	19.	14-
18-17	454	77 •	54+	51 •	43•	35•	24.	50 •	12.
18.33	384 •	58*	41.	36.	33 •	38•	26.	18.	11.
18.50	295.	44.	31 • 24 •	31. 21.	25. 17.	32. 31.	23. 23.	80 • 18 •	14.
18+67 18+63	187 • 42 •	34. 19.	17.	16.	11.	86.	15.	18.	7.
19.00	0.	8.	2.	6.	5.	*8	1.	1:	i:
10.17	Ď.	ñ.	0.	ő.	0.			ů.	ů.

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DATE	25 AUG	1974	LOCATIO	N	OA .				
TIME	DN	TH	тні	THE	THS	SH	5#1	SH2	51/3
5 - 67	0.	0.	0.	0.	0.	0.	0.	0.	0.
5 . 83	ļ.	٤.	1.	8 -	٤.	ę.	1 •	Q.	0.
6.00	3.	8-	.6+	8.	.6•	9.	.4+	3.	Õ٠
6 • 1 7	143+	14.	10.	12.	10.	16.	11.	8.	5.
6 • 33 6 • 50	844. 338.	84. 41.	17. 30.	16. 27.	14. 25.	22 • 85 •	11. 16.	10. 12.	6. 7.
6 • 67	412.	64 •	46.	39.	34.	30.	16.	14.	ģ.
6 • 83	474.	91 •	65.	56 •	50.	35.	ėi.	16.	ıó.
7.00	525.		81 -	68 •	60 •	32.	15.	14.	6.
7.17	567 .	150 •	105.	68+	79.	39•	25.	18+	10.
7.33	609•	176 +	125.	106 -	93 •	38.	22.	16.	9.
7.50	637•	215.	152.	129.	113.	46 •	27.	£0.	13.
7 • 67 7 • 83	665	247 • 278 •	176. 197.	149. 164.,	131.	49. 45.	29. 28.	22.	15. 13.
8.00	690 • 715 •	316.	224.	189-	166.	49.	30:	88.	13.
8-17	735.	346.	244•	204	182	48•	29.	21.	10.
8.33	754	384 .	274 •		203 •	54+	35•	24.	18.
8 - 50	767.	416.	297•	250 •	216.	54 •	34 -	23 -	18-
6+67	779.	452 •	322.	269.	239.	56.	36.	26.	19.
8 • 63	788.	469 •	343	288.	253 •	60 •	36•	27.	16.
9.00	805	513.	364	306.	271.	58+	36.	26.	19.
9.1 <i>7</i> 9.33	816. 624.	546 • 572 •	386 • 406 •	326• 342•	288• 301•	60 • 59 •	37. 37.	27. 25.	19. :8.
9.50	833	604	406	359	320	62 •	35.	29	17.
	542	628.	445	373 •	331 .	60 •	37.	27.	15.
9 - 83	848.	658.	466 -	393 .	348.	68.	41.	29.	18.
10.00	857 •	680 •	460 •	408 •	360•	63 +	37.	30 •	18.
10 - 17	86i •	709•	501 *	423.	374.	67 •	40 •	32.	55.
10.33	868	7.26 •	515	437.	386 •	65•	38.	28.	18.
10.50	866	751 • 764 •	529 • 540 •	449. 458.	397 • 405 •	70 • 67 •	43. 40.	32 30	21. 19.
10.67	869 • 878 •	787	556 •	474.	419-	75 -	45.	34.	24
11.00	875	798.	565 •	481	424	73 -	44.	33 •	23 .
11.17	882	813.	574 .	488.	433 .	74 .	45.	34+	24.
11 -33	876 •	B27 .	584 •	497 •	439.	.70 - •	44 -	34.	82.
11 -50	876.	838.	593 •	504	445.	77•	46 •	36.	26.
11.67	863 •	845.	597 •	507.	449.	75.	45•	35•	25•
11.83 12.00	880 • 879 •	850 • 856 •	602 • 604 •	513. 517.	453 • 456 •	77. 78.	48• 46•	37. 37.	24. 26.
12.17	884	864	608.		458 •	79.	48.	37.	26.
12.33	882.	865 •	611.	520 .	461 •	77.	50 -	38.	26.
12.50	878.	664 •	612	523 -	462 .	83 -	49.	38.	28.
12.67	875 •	868 •	611 -	521 .	459.	84.	54•	42 •	28.
12.83	672	859 •	608	516.	459 •	68 -	51.	41 -	28.
13.00	876	858.	605.	519.	457 -	84+	52 •	42.	31 •
13.17 13.33	874 • 877 •	851 • 843 •	599 • 595 •	512 • 507 •	453 • 450 •	62 • 79 •	50 • 50 •	39. 37.	30 • 28 •
13.50	b. 7 •	835 •	590	501	444.	82	52 .	38.	26.
13.67	873	815.	578	495.	435.	77.	47.	37.	24.
13.83	871 .	806 •	569.	488.	430.	76.	48.	38.	25.
14.00	865	786.	555 -	473 •	420.	77•	46-	35.	23.
14-17	B65+	769•	547 •	466 •	410-	72•	47.	36-	24.
14.33	860 -	754 •	533	455	404	79.	50 •	36.	25 • 25 •
14.50	856 • 849 •	731 • 710 •	518. 505.	439 • 428 •	390. 380.	72. 71.	45. 46.	33. 33.	25.
14.83	844.	686	487 •	417.	366.	74.	46.	36 .	26.
15.00	838.	658.	468+	400	352 •	69.	48.	33.	83.
15-17	826•	634•	450 -	380 -	338.	74 -	45.	33.	24.
15 • 33	821	612.	433 •	368.	325•	72	48•	35.	24.
15.50	812.	580 +	411 •	348.	308. 292.	70 -	47.	34.	22. 24.
15.67 15.83	795. 791.	550 • 516 •	391 • 369 •	332. 312.	275.	70 • 71 •	46 • 46 •	35. 38.	20.
16.00	770.	485	346.	294.	258.		46.	34.	23.
16-17	768	453 .	324.	277.	243.	68.	47.	30 •	22.
16.33	750.	418.	299	253.	225.	64 •	42 .	30+	21.
16-50	732.	389 •	276	234	207.	63 •	45 •	31.	81.
16.67	714.	353 •	252.	213.	189.	63 -	47.	28.	£0.
16 -83	702 • 669 •	321 • . 285 •	229. 804.	194 • 173 •	170. 151.	58 • 63 •	45 • 44 •	29. 28.	19. 20.
17-17	637	244.	175	149.	132 •	59 ·	44.	27.	19.
17.33	608+	211.	152	131.	116.	57.	44.	26	16.
17.50	571	162 •	130.	112.	99.	55.	41 •	25.	17.
17.67	548.	151.	109.	96 •	84 •	48.	41.	23.	14.
17.83	505 •	119.	84	76 •	67.	46+	35.	80.	15.
18.00	449.	93 •	66	56•	50 •	41.	31.	20.	14.
18.17	367.	65.	46.	41 • 31 •	38. 27.	38. 38.	25-	16.	8.
18.33 18.50	311. 221.	43. 32.	22.	20.	17.	22.	21. 16.	14. .12.	10.
18-67	105.	20.	15	15.	11.	21.	11.	10	5.
18-83	18	11.	ß.	9.	8 •	6	8.	5 •	2 .
19.00	0.	0.	0.	n.	0.	0.	0.	0.	0.

DATE	26 AUG	1974 L	OCATION	85710	A			•	
TIME	DN	TH	THI	THE	TH3	SH	SHL	5 H2	SH3
5 - 67	٥.	0.	0.	0.	٠.	0.	0.	0 •	0.
5 - 83	8.	٥٠	1 • 6 •	5• 7•	4. 4.	6• 9•	4.	3.	2.
6.00 6.17	4. 96.	5. 9.	9.	10.	7 •	11.	9.	7. 11.	1 • · · · · · · · · · · · · · · · · · ·
6.33	198+	24.	18.	15. 25.	17. 23.	15. 23.	15. 17.	14.	8.
6 • 50 6 • 67	294. 375.	40 • 62 •	31. 45.	39.	33.	38 •	16.	13.	5 ·
6 - 83	444.	83 .	6Ô •	53 •	46• 59•	34. 36.	81. 20.	15.	10
7.00	502 • 549 •	111. 146.	79. 104.	67 • 59 •	77.	43 •	25.	20.	14.
7 • 1 7 7 • 3 3	573	1 60 •	127.		5054•	40 • 45 •	26. 29.	21 • 21 •	12.
7 • 50	625•	211 • 248 •	151 · 174 ·	130	114. 189.	48.	30.	23.	12.
7 • 67 7 • 63	656 • 687 •	283 •	198.	167.	148	48 •	32. 35.	23 • 25 •	13• 15•
6.00	706	315 - 346 -	223 • 246 •	190 · 211 ·	168• 184•	58 • 50 •	29.	24.	16.
6+17 5+33	735• 752•	387 •	272.	233.	203 •	56 •	35.	26 ÷ 26 •	17.
8 - 50	772.	420 •	296. 321.	248 • 272 •	219• 242•	51 • 60 •	38. 38.	28.	17.
₿•67 В•83	789. 803.	455 • 486 •	345-	291 -	256+	57	35.	27• 26•	17. 18.
9.00	817.	520 -	368-	312 · 326 ·	275 • 289 •	61 • 64 •	38• 36•	25.	19.
9-17	826 • 838 •	547 • 583 •	367. 413.	352+	309 •	65•	41 .	31 -	20 •
9 - 50	846 •	609+	431 •	367 •	324 -	67 • 65 •	41 • 39 •	5. 30.	21. 19.
9.67	854•	636 • 661 •	450 • 469 •	383. 399.	338• 351•	66+	39-	30 •	19.
9 • 83 10 • 00		686 •	486 •	413 •	363 •	65+	39.	32. 30.	20.
10.17	861 -	707	498•	424 • 43 B •	376 • 386 •	70 • 68 •	40 • 40 •	31.	20 •
10 •33 10 •50		729 • 753 •	515. 532.	453 •	400+	72•	43 •	33 • `	22. 22.
10 -67		766 •	542 .	464.	408	74 • 76 •	42 • 43 •	32• 33•	23.
10 83		779 • 801 •	552 • 566 •	473 • 483 •	417. 427.	77.	47.	36.	24.
11.00		813 -	57B.	492.	434 -	76•	47. 43.	33• 32•	22. 19.
1133	B90 •	625•	585 • 593 •	501 + 507 •	442 • 448 • *	70 • ·	46.	35.	23.
11.50 11.67		839+ 848+	599 •	511.	451 •	73.	44.	34.	21. 21.
11.8	894.	655•	605	516 •	455 • 459 •	73• 75•	44• 45•	33 • 35 •	22.
12.00			607 • 609 •	520 • 519 •	458	60 •	45.	35•	24.
12 • 11 12 • 33			612.	521 •	460 •	77 •	46. 49.	36. 37.	23 • 24 •
12.50	B90 •		613 -	524 • 521 •	463 • 462 •	78• 77•	48.	37.	25.
12.6°			613.	5 23 •	460 •	77 •	45 • 47 •	35. 34.	25. 21.
13.0	884		606 + 602 +	519· 514·	459 • 453 •	75+ 76+	45.	35	23 -
13 -1 13 -3			600 •	513.	451 •	72 •	45.	33. 35.	23.
13.5	0 898	834•	591 •	505• 496•	445 • 437 •	76• 74•	44. 43.	33 -	21.
13.6 13.8			579 • 574 •	491	432 •	70 •	42 -	31 •	55. 50.
14.0	0 881	790 •	562 •	482 •	424 • 412 •	78• 74•	45. 43.	33 • 33 •	22.
14-1			548• 533•	468 • 455 •	401 •	76 -	44.	34.	24.
14.3 14.5		. 733 -	521 •	447 -	394 •	71 • 69 •	44 • 42 •	32 • 34 •	20 - 22 •
14-6			506 • 490 •	434 • 421 •	380 • 369 •	72 -	42.	32.	55.
14.8 15.0			471 •	406+	354•	67 •	43 • 40 •	31 · 32 ·	21 • 18 •
15 - 1	7 839		452 • 434 •	385. 370.	339. 327.	70 • 67 •	37-	30 •	17.
15+8 15+8			415.	353 •	311 •	62 -	38-	29. 27.	19. 18.
15.6	7 622	552 •	392 •	337 • 316 •	293 • 279 •	60 • 61 •	39. 36.	28•	19.
15 • 0 1.6 • 0			369• 346•	298	260 •	59.	35+	25. 27.	18• 15•
16-1	7 787	457	324•	280 •	245 • 226 •	60 • 58 •	35. 34.	26.	14
16 -			300 • 300 •	257 • 257 •		58•	34•	26+	14 •
16 · 1			252•	216	191 •	50 • 51 •	31 + 29 •	23 • 22 •	16. 16.
16 -	83 730		506 • 550 •	198. 176.		52 •	31 +	22.	13+
17.			176.	156.	133 •	48.	20.	23 •	13 • 16 •
17 :	33 639	217.	155 •	133.		51 • 44 •	20 s	20.	14.
17. 17.			127 • 104 •	92	82•	42.	85+	18.	12. 13.
17.		7. 117.	• 23	75		40 • 34 •	24 • 21 •	18. 17.	11.
18.	00 466			57 ·		30•	18.	15.	7.
18			29	29	24.	23 •	15. 14.	14. 9.	6+ 4=
18.	50 88	4. 24.				19. 16.		7 •	6•
16. 16.		6. 17. 4. 6.	_	5	. 6-	4.	4 •	3. 0.	0 ·
19			, 0.		. 0.	0.	0.	0+	• •

OF POOR QUALITY

DATE	DUA OE	1974	LOCATIO	DN+ 857	104				
TIME	DÑ	TH	THI	THE	TH3	SH.	SHI	5 H2	SH3
5 - 67	0.	٥.	٥.	0.	٥.	0.	.0.	0.	0
5 • 83	1.	Q-	1.	3.	٠.	4.	3.	8.	. 0 •
6 • 00 6 • 17	71.	. Ś.	4. 15.	15.	1 ·	7• 82•	2. 13.	2. 12.	11.
6.33	169.	37.	27.	86.	17.	38.	82.	-99.	15.
6 • 50 6 • 67	260. 322.	54 • 73 •	40 •	37.	27.	45.	28.	25.	£1.
6 • 63	372.	65 •	51 • 63 •	45. 55.	36. 44.	49. 48.	34. 33.	26. 25.	22. 17.
	433 •	111.	79.	71.	56	54.	32.	25.	19.
7 • 1 7 7 • 3 3	506 • 550 •	138.	99. 122.	86 + 104 -	. 71 · B6 ·	53 • 54 •	32. 32.	25. 26.	18.
7 -50	589	203.	146	124.	104	61 +	38.	27.	19.
7 • 67	• 020	235.	170 •	144+	123.	60 •	37.	28.	22.
7 • 83 8 • 00	645 • 666 •	270 • 306 •	194. 218.	165 • 185 •	142. 157.	69 • 69 •	40 • 40 •	33. 32.	22. 83.
8 - 17	692.	341 .	244.	207.	178-	70 •	42 .	35.	24.
6.33	710-	373 •	267	227.	194.	71 •	45.	34.	25.
8 • 50 5 • 6 7	728. 743.	406 • 446 •	292 - 316 •	248. 270.	211. 232.	75 • 79 •	46 • 50 •	36. 37.	28. 26.
5 - 83	763 -	476 .	339.	290 •	249.	82 .	50 •	39.	28.
9.00 9.17	770 •	509.	364	312.	267-	83 •	51 •	39.	27.
9.33	787 • 808 •	540 • 572 •	387. 408.	329. 352.	302 •	83 • 79 •	50 • 50 •	37.	26. 26.
9 - 50	823 •	603 •	430 •	368.	317.	78.	47.	36.	25.
9 • 67 9 • 83	894	634 •	450 •	386.	333 •	60 •	48+	37•	25.
10.00	846 • 860 •	660 • 690 •	470 • 490 •	405 • 422 •	349 • 364 •	63 + 64 +	49. 52.	37. 39.	26. 28.
10.17	86A ·	712.	507	435•	376	83 •	50 •	39.	28.
10 -33	873 • 880 •	740	526	452 •	389	86 •	50 •	38.	88.
10.50 10.67	888 •	761 • 780 •	541 • 553 •	465. 474.	401 • 411	82 • 84 •	49. 51.	39.	28. 26.
10 -83	880%	794 •	563 -	486 .	419	87.	51	39.	28.
11.00	886 • 892 •	807	575 •	497 •	430 •	84.	53 •	39.	27.
11.33	891 +	826. 832.	588. 593.	506 • 511 •	438. 444.	83 • 81 •	50 • 49 •	38	27. 25.
11 +50	897 •	849.	604 •	519.	450	83 .	49.	38.	26.
11.67 11.83	888. 887.	856 v c 860 •	609. 613.	524 • 527 •	455.	84	53 •	38.	24.
12.00	894.	866 •	617.	530 •	456 • 460 •	86. 78.	51 • 52 •	40 - 40 -	28. 27.
12.17	890 •	865.	619 •	531 •	459.	81 •	51 •	37.	26.
12.33 12.50	890 . 887 •	673 • 870 •	622. 619.	536. 539.	464 • 461 •	86+	51 •	40 •	27.
12.67	B68 •	B69 •	619.	532.	462.	62 . 83 .	52 • 50 •	36. 39.	26. 27.
12 -83	893 •	865 •	617.	52B.	459	85 •	52.	39.	86.
13.00 13.17	890 • 891 •	662. 856.	614. 610.	529• 522•	458 - 454 -	83 • 66 •	50. 51.	39.	28.
13.33	888.	842 -	601	518.	447.	85•	51.	37. 40.	27. 26.
13 • 50	883 •	832	594.	512.	442	68+	54.	40 -	88.
13 • 67 13 • 83	862 • 85 9 •	816 • 801 •	583 • 574 •	503. 492.	435. 425.	93 • 93 •	57. 58.	43. 45.	30. 30.
14.00	849.	789.	561 •	483 •	416.	97.	59.	47.	34.
14-17	630 -	765	546.	471 •	406 -	101.	61.	48-	35•
14.33 14.50	827. 819.	745 • 726 •	534 - 51 B •	460 · 445 •	395. 386.	103 • 101 •	62 •	47. 49.	34. 33.
14.67	B10 •	700.	501 •	430 •	371 •	102.	61.	47.	33.
14 • 63 15 • 00	804 • 791 •	676 •	484 •	416.	360 •	97 •	62 •	48.	31.
15.17		648 • 624 •	465. 447.	400 • 383 •	344. 330.	98• 95•	60 • 59 •	46 • 45 •	32. 31.
15.33	781 .	597 -	428.	367.	318	94 .	60 •	46 •	32.
15.50 15.67	774• 766•	572. 539.	410. 386.	353.	303.	91 -	58+	44.	30 •
15.83	755 •	509 •	366.	332. 313.	287. 269.	86. 87.	57 • 54 •	44. 41.	29. 28.
16.00	740 -	475 •	341.	295.	253.	85 •	54.	40 -	28.
16 • 17 16 • 33	721 • 695 •	444. 404.	318. 290.	272. 851.	234.	81 •	52 •	40 •	26.
16.50	688.	373 •	268.	232.	213. 197.	80. 74.	51 • 47 •	40 • 37 •	27. 25.
16 - 67	675.	341 -	245.	211.	179.	70 .	46.	35.	24.
16 · 83 17 · 00	656. 625.	304 - 63 •	220. 191.	191 • 166 •	161.	67• 60•	ሳይ • 40 •	34. 29.	22. 20.
17.17	590.	32ء	166.	143.	121.	58.	36.	28.	194
17.33	.564	196 •	141.	165-	ŧ04 •	54.	37.	28.	19.
17.50 17.67	523 · 490 ·	162 ·	117. 97.	101 • 85 •	85 • 71 •	53 • 47 •	33. 31.	26. 23.	16. 15.
17 - 63	427 .	100.	73 •	66.	53	46.	29.	55.	14.
18-00	332 •	6B+	52.	44.	38+	36.	25.	19.	14.
18-17 18-33	870 • 804 •	50 ·	35. 23.	32. 23.	25. 15.	31 · ·	21. 17.	18. 16.	13.
18.50	133.	19.	14	13.	9.	20.	12.	11.	8.
16.67	58•	10 -	6.	9.	5.	11.	8.	7.	5 .

DATE	31 AUG	1974	LOCATI	ON: 857	10A				
TIME	DN	TH	THI	THE	TH3	SH	SHI	SH2	SH3
5 - 63	Q٠	0.	0.	0 •	Ō٠	Q.	0.	0.	0.
6.00	8	ō.	٥٠	8.	o.	7•	3. 5.	3.	8.
6-17	17.	. 5• 20•	5• 15•	5• 15•	2. 11.	12. 88.	5. 14.	5. 12.	5. 5.
6 • 33 6 • 50	61 • 805 •	37.	87.	23	19.	32.	21.	16.	13.
6.67	270 .	57.	43.	40 •	33.	44.	29.	84.	17.
6 +83	285	85 .	61.	57 •	44.	58.	39.	34 •	24.
7.00	392 -	124.	89•	76 •	62 ··	72 •	48.	38.	29.
7-17	447.	153 •	109.	93 •	77 •	71 •	49•	41 •	30 •
7 • 3 3 7 • 5 0	488 • 534 •	178. 215.	130. 152.	113.	92. 111.	81 • 83 •	51 « 52 •	42 • 45 •	30 • 31 •
7.67	569	236.	169.	144.	123.	74 •	49.	39.	26.
7.63	600 •	269.	190 •	163 •	139		49.	35.	25.
6.00	627.	295.	213.	188 .	154.	71 -	44.	36 •	25.
8,-17	658	338•	238.	203•	173 -	80 •	49.	37.	26.
8.33	670 •	367 •	260 •	221.	190 •	82 •	49.	36.	25. 27.
6∙50 8•67	695 • 716 •	403 • 435 •	287• 309•	242 • 261 •	208. 225.	84 • 82 •	53 • 52 •	39. 40.	26.
8+83	734.	471.	333 •	283	245.	67+	54.	40 •	27.
9.00	750 •	501	358	306.	262.	90 -	51 •	40 •	28-
9-17	762 •	534.	381 •	325.	278.	94.	53•	41 •	30 + .
9.33	775 •	561 •	398•	340.	294•	90 •	54 •	42 •	88.
9+50	780 •	589	420 •	360	310 •	95+	59.	45•	32 •
9 • 67 9 • 83	785 s 800 •	618. 646.	441 • 459 •	378. 394.	326. 341.	96• i04•	59. 61.	44. 47.	30. 34.
10.00	801 •	669.	475.	406	351 •	103	60 •	47.	33.
10.17	B05 ·	698 •	494 .	424	367.	103.	61 -	47.	34.
10-33	816-	716.	509•	437 •	380.	103+	63 -	47-	31 -
10.50	822.	737•	525•	452	389.	109	63 -	48.	35.
10.67	811.	751 •	536 •	457	398+	113.	-99•	53+	. 34.
10 +63 11 -00	799• 811•	765• 787•	544 • 556 •	465. 478.	404 • 417 •	124. 118.	76 • 72 •	57• 57•	39. 40.
11.17	819+	799.	569.	488	422.	116.	73 •	54.	39.
11.33	825.	816.	578.	497.	430 •	117.	71 .	54 •	36.
11.50	82B.	824.	566+	502 •	436.	120	71 .	55 •	37.
11.67	837 -	638+	595 •	510	445+	122.	71 •	56 •	36 •
11.63	827•	889.	597•	510 •	445.	118.	71	56•	36.
12.00	822 •	846 -	599+	514.	447.	127.	79 -	59•	43. 41.
12 • 17 12 • 33	813. 810.	844. 844.	599 • 600 •	513 · 513 ·	449 • 447 •	130 · 127 ·	80 • 80 •	61 •	41.
12.50	806	841 •	601 •	513.	447.	128	80 •	61 •	43 •
12.67	806.	640 •	597.	510		. 131 -	78.	62 •	43 •
12.83	810 •	840 •	596+	510 •	445.	128	77.	59 •	42 •
13.00	813 •	833 •	596+	510.	444.	131 •	79•	68+	42 •
13 • 17 13 • 33	8:2 · 807 ·	830 • 819 •	591 • 584 •	507 • 500 •	439. 435.	127• . 126•	77. 75.	59. 57.	39. 41.
13.50	604	811.	577.	493.	429.	121.	76.	58.	39.
13.67	600 •	793 •	565 •	485	422.	121.	73 •	57.	41 .
13.83	799.	784 •	557•	476.	415.	122.	73 •	56+	38 -
14.00	793•	764+	546+	467•	406 •	120.	73•	57.	40 •
14-17	763 •	735 •	522•	446.	369.	126.	76 •	59•	41.
14.33 14.50	773 • 774 •	725 • 701 •	515. 503.	443. 430.	385 ·	120.	73 +	58•- 54•	41. 37.
14.67	774.	679.	487.	418.	372 •	113.	70 • 68 •	53 •	37.
14.83	758.	655.	468	402	348.	112	67.	51 •	36.
15-00	761 -	634.	452 •	367•	336.	108.	66.	49.	32 •
15.17	751 -	606 •	432 •	372 •	320+	107.	66+	49.	34.
15.33 15.50	746. 737.	582 • 551 •	416. 392.	358. 338.	308. 290.	101 • 96 •	64. 61.	47 ·	33 • 32 •
15.67	727•	520 •	371 •	318.	274.	90 •	57.		30.
15.63	719.	489 •	350 •	301 •	860 •	91.	55.	43 • 42 •	27.
16.00	703.	459.	329.	281	242.	87 •	56.	42.	27.
16.17	694+	425.	305.	261.	226.	64 +	50 ▲	40 •	25 +
16+33	679.	391 •	262 •	2/2	207•	79 -	50 •	37.	23 -
16.50 16.67	657• 648•	357• 385•	257. 231.	219. 200.	188.	77. 72.	48. 43.	36. 34.	50 • 55 •
16-83	625+	266.	209.	180 •	153	70	43.	31.	20.
17.00	604+	858.	183 -	157.	135.	63 •	42.	32.	39.
17-17	566+	220 •	158.	135.	114.	63 •	38.	29.	20.
17.33	549.	191.	138.	120.	101 -	57.	37.	27.	17.
17.50	507 •	157+	113.	101+	84+	53 •	35+	25.	16.
17.67 17.83	464. 419.	129.	91 • 72 •	81 • 65 •	66. 53.	51. 47.	35. 33.	25. 24.	17.
18.00		78+	58.	51 +	41.	49.	34.	26.	17.
18.17	280	67.	48.	45.	35•	52 •	34.	29.	20.
18.33	208+	49.	37.	30 •	86+	42 .	31.	24.	20 •
18 - 50	121.	28.	55.	19.	14.	29.	21.	17.	12-
18.67	15+	16.	14.	13.	9•	20.	15.	11.	10.
16-83 19-00	0 ·	10 -	7 • 0 •	11.	5 • 0 •	9. 0.	7. 0.	8 + 0 +	7 • 0 •
	••		~ -		J.	₹r =	~ F		J.

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OFFIGINAL PAGE IN OUR OWNLING

DATÉI	OI SEP	1974	LOCATIO	ON: 657	IOA '				•
TIME	DN	TH	THI	THE	TH3	SH	SHI	SH3	5H3
5 • 83 6 • 00	0 •	9. 0.	0 • 0 •	0. 1.	0.	0.	Q.	o-	0.
6-17	3.	5.	8.	5.	0.	0 • 6 •	3. 4.	1 • 3 •	0 • 8 •
6 • 33 6 • 50	3.	13 • 18 •	9.	6. 15.	6. 9.	12.	10.	9.	5.
6 - 67	3.	40.	31.	25.	22.	24 • 42 •	16. 31.	14. 85.	22.
6 • 63 7 • 00	65 ·	60 -	39-	39.	30.	- 61 • 67 •	44.	36.	29.
7.17	7.	71 • 81 •	52 • 56 •	45 • 48 •	37 • 43 •	84.	47. 56.	38. 49.	30 • 37 •
7 + 3 3	33.	124.	90 •	74 •	66.	122.	84 -	69.	56.
7 • 50 7 • 67	382. 413.	242 ·	173. 212.	151 • 164 •	125. 152.	147. 171.	100 ·	57. 108.	68. 82.
7 - 63	172.	237.	169.	148.	125.	181 -	124.	106 •	85 -
8-00 8-17	14. 273.	174 • 262 •	122. 202.	102. 174.	91 • 149 •	169. 164.	117.	97• 96•	77. 76.
8.33	21.	178.	122.	102.	93 •	171.	115.	98.	75 ·
8.50 8.67	341 • 128 •	334 • 252 •	236. 182.	197. 152.	167. 139.	181 - 179 -	123. 125.	101.	52 . 60 •
8 - 83	197.	288.	204	171 -	150.	178.	121.	98.	77.
9.00 9.17	66• 556•	224. 478.	154. 339.	126. 284.	118 • 250 •	167.	125.	101 -	:9.
9.33	655•	557 •	394	391 •	292.	162. 160.	104.	61 • 78 •	ა0 • 58 •
9.50	459 -	451 •	316.	266.	240 -	161 •	101.	77.	57.
9.67	665. 677.	586 • 606 •	417• 429•	350. 362.	307. 320.	152 • 146 •	95 • 90 •	74. 71.	51 • 50 •
10.00	696 •	633 .	449.	378.	332.	145.	89.	70 •	47.
10.17	649. 714.	646 • 692 •	457 . 490 .	<381 • 444 •	338. 366.	179. 158.	113.	90. 77.	65. 54.
10.50	723.	707 •	501 •	423.	372 .	149-	95 -	71 •	49.
10 • 67 10 • 83	748. 757.	719. 738.	508. 522.	430 • 439 •	381 • 369 •	139. 134.	84 - 82 -	65 • 62 •	45. 42.
11-00	754-	754.	534.	450.	379.	144-	85 -	65.	46.
11-17 11-33	758• 772•	762 • 781 •	539. 552.	454.	403	141-	B5 •	66•	45 •
11.50	772.	790	560	465. 472.	413. 419.	139. 139.	83 • 85 •	64. 65.	43. 43.
11.67	767.	797 •	563 -	475.	423.	144-	87+	65•	46.
11.83 12.00	754. 789.	812 • 817 •	576. 579.	465. 489.	430 • 434 •	140 -	86. 83.	63 • 63 •	43 • 44 •
12.17	790.	824 -	582 •	493.	437.	137.	82 -	63 °	43.
12.33 12.50	781 • 789 •	822 • 81 8 •	580 • 579 •	489 • 489 •	436. 437.	142. 134.	86 • 82 •	64 • 62 •	44 • 41 •
12 - 67	799.	. 1SB	580 •	489.	436 -	130 •	78.	<u> </u>	36.
12.63 13.00	601 • 792 •	825 • 811 •	583 • 573 •	491. 484.	437. 431.	128. 130.	78. 78.	60 • 58 •	. 41 • 40 •
13 - 17	789.	604	569	480	427	130	78.	58.	40 •
13 • 33 13 • 50	803. 795.	826 • 797 •	585	493 • 478 •	440 •	144.	91 •	70 •	50 •
13.67	794.	760.	566 • 552 •	468+	424. 416.	134. 130.	53 • 79 •	64. 59.	44. 41.
13-83 14-00	795 •	765 •	540 •	456 -	407.	119+	72.	53 •	37.
14.17	784 - 781 -	741 • 720 •	524. 511.	442. 433.	392. 383.	115. 111.	69 • 67 •	53 · 51 •	34 • 34 •
4.3	786 •	708.	500	423.	378.	112.	66.	49.	33.
14.50 14.67	781 - 774 -	689 • 663 •	486. 471.	410. 398-	365. 352.	107. 107.	67. 64.	50 • 47 •	33. 31.
14 -83	768.	639.	451 -	381.	340 •	102.	61 •	46 -	31.
15.00 15.17	753 • 754 •	610 • 589 •	434. 417.	366. 352.	3/3•	99 •	62 • 63 •	46. 46.	31 • 30 •
15.33	740.	561 .	398.	337•	2.9.	101 -	63 •	45.	30 •
15.50 15.67	713. 711.	526 ·	374. 358.	316. 304.	260. 269.	100 •	62 ·	45+	31.
15 - 83	674.	461.	327.	277.	243	102.	68.	45. 50.	31 • 34 •
16.00 16.17	687. 632.	455 ·	384.	273 ·	240	104.	68•	48.	33 -
16 -33	577.	353	263. 251.	214.	214. 168.	101. 102.	67. 68.	46. 48.	32 - 34 •
16.50	562 •	337.	240 -	£03•	176.	103.	67.	46.	35.
16.67 16.83	584. 571.	308. 283.	220. 201.	187. 172.	164. 149.	94 • 89 •	65. 61.	44 - 41 •	31. 28.
17.00	546+	246.	176.	151.	131.	86 -	61 •	41 .	29.
17.17 17.33	513. 457.	212. 167.	151	102.	114. 91.	77• 68•	58. 50.	38. 31.	25. 21.
17.50	411.	136.	95 .	83 •	73.	59.	43.	87.	18.
17.67 17.83	403 • 156 •	115. 54.	53. 38.	71 - 32 -	62 • 29 •	56 • 39 •	42. 27.	27.	18.
18.00	241.	47+	34.	31.	25.	35.	22.	19.	11.
18.17 18.33	131.	31.	22.	22.	17.	27.	18.	14.	10.
16.50	1.	19. 9.	13. 8.	13.	10.	12.	14. 9.	12.	9. 4.
16-67	. 1.	5.	4.	7 •	4.	8.	5.	5 •	3 •
16-83	0.	0.	0.	0.	0.	0 •	0.	0+	. 0.

DATE	02 SEP	1974	LOCATI	0N: 657	10A				
'TIME	DN	ŤH	THE	THO	ŤH3	SH	5H1	SH2	5H3
5 - 53	0.	Ō.	0 •	0.	٥.	Q٠	۰.	0.	Q٠
6.00 6.17	2. 3.	2. 6.	1. 5.	2. 5.	1 • 5 •	11.	1 · 7 ·	3. 5.	0.
6.33	4.	14.	- 11.	14.	7.	18.	13.	18.	4.
6 - 50	3.	27.	18.	18.	13.	26.	21.	17.	13.
6 · 67 6 · 53	3.	38. 46.	25. 31.	25. 28.	21. 23.	41 - 45 -	25. 31.	24.	19.
7.00	3.	65.	45.	40 •	35.	65.	45.	29. 40.	21. 31.
7-17	4.	82 •	61 •	51 •	44.	85.	61 •	50 •	41.
7 • 33 7 • 50	5. 5.	100 •	73 • 79 •	60 • 65 •	53. 61.	101. 113.	71 • 80 •	60 • 67 •	49+
7 - 67	12.	128	91 •	76.	69.	128	88.	75.	54 • 60 •
7 - 83		156.	110.	76. 91. 168.	52.	147.	100 -	83 •	67•
5.00 5.17	279. 20.	265• 168•	192 • 116 •	168 • 95 •	140 • 88 •	164 162.	111.	90 •	73. 70.
Ē-33	362 •	315.	224.	185.	163.	157.	105.	86 •	66.
5.50 6.67		401 •	286.	236.	207.	176.	119-	94 •	74 .
	225. 260.	292. 329.	206. 232.	170 - 193 -	174.	176 • 185 •	116. 123.	94. 98.	74 • 77 •
9.00	597 •	503 •	357.	297.		170.	111.	85.	65 -
9~17 9.33	643	558 •	391 •	328.	259 "	178-	116.	91 .	68-
9·50	663 • 662 •	574. 615.	407• 436•	342. 366.	302.	182. 202.	117. 131.	92. 104.	68. 78.
9.67	665•	680 •	481 .	403 •	353.	-99.	164.	133.	-99.
9.83 10.00	56.	384 •	261 •		234.	309.	808	174.	138.
10.17	333. 384.	577 • 643 •	405 • 449 •	248. 336. 372. 182. 182. 359. 480. 495. 331. 140.	308. 336.	346 • 342 •	236. 232.	191.	151. 151.
10.33	4.	314.	219	182 -	167.	314	218.		145.
10.50 10.67	10. 534.	263.	180 •	148.	167. 138. 325.	254.	174 -	143.	113.
10 - 83	738.	575 • 808 •	415. 574.	480.	427.	233. 237.	154. 154.	122.	93 • 91 • 92 • 133 •
11.00	745.	827•	585.	495 •	437. 293.	236+	152.	188.	92 .
11.17 11.33	298. 12.	576 • 250 •	403	331.	293.	318.	216. 159. 157.	171 •	133 •
11.50	2.	273.	172 • 187 •	152 *	136. 148.	218. 239. 280.	157.		104. 119.
11.67		817.	360 •	431 •	444.	307.	157. - 204. 190. 197. 159.	161.	126.
11-83 12-00	765 • 764 •	935 • 949 •	662 • 673 •	558•	496.	268.	190 -	150 -	116.
12-17	760	939.	665.	560 •	503 • 498 •	296 • '	159.	157. 148.	121 • 114 •
12.33	708.	917.	656 •	556.	49R.				125.
12 • 50 12 • 67	741 • 711 •	894 • 866 •	632. 612.	534. 516.	474.	256. 237.	166.	131 -	98•
12.83	715.	854	607+	512.	452	217.	156. 142.	123. 109.	91 • 80 •
13-00	747.	833 -	586.	498 •	443 -	• 003	128.	97.	66.
13.17 13.33	708. 5.	842. 224.	586 • 153 •	488. 122.	427. 125.	243 • 233 •	159.	184.	92.
13.50	732.	865 •	614.	519.	460	262.	175	125. 135.	93. 102.
13-67	367.	639.	443 •	364. 347.	324. 314.	345.	239.	169.	150 •
13.63 14.00	186 • 164 •	584. 529.	412. 379.	347· 326·	299.	413. 369.	267. 255.	233. 204.	165 - 164 -
14-17	258.	560 •	401 4	343.	311.	339.	235.	185	148.
14.33 14.50	696 • 735 •	740 •	526•	441 •	393	217.	146.	109.	81 .
14.67	724.	647 •	484 461 -	408. 386.	363. 345.	155. 144.	104. 97.	69. 63.	49. 44.
14.83	722.	630 •	446 •	376.	334.	143.	97.	60 •	41.
15.00 15.17	727. 713.	607 . 581 •	429. 412.	360 •	323.	138.	95•	57.	40 •
15.33	698•	552	393.	344. 329.	308. 294.	135. 137.	94 • 97 •	57. 57.	40 . 40 .
15,50	691 •	522.	371 •	312.	278.	135.	96.	55•	39.
15 • 67 15 • 83	684 • 656 •	501 • 466 •	356 • 330 •	300 • 278 •	267. 247.	137. 136.	102.	57.	39.
16.CO	654.	443 •			235	138.	103. 106.	56 • 56 •	39. 39.
16-17	616.	406 •	289.		214.	139.	108.	59•	39.
16 • 33 16 • 50	608. 592.	371. 339.	262. 239.	223. 204.	196 ·	131. 124.	103. 101.	53 - 48 -	35.
16.67	577.	308 •		183 .	160	121.	98.	45.	35. 30.
16.03 17.00	546.	266 •	191 •	161.	141 •	112.	92.	44.	30•
17.00	505• 478•	229. 197.	163 • . 142 •	140 • 120 •	120 ·	105. 99.	88. 80.	39. 37.	27. 26.
17-33	441.	166 *	119.	101.	89•	91.	74.	33.	88.
17.50 17.67	405	134	97• 74•`	63 -	72 •	83 •	67.	31.	. 22 .
17-83	361. 311.	107. 52.	74. 57.	66 • 45 •	57. 45.	68. 61.	54 • 46 •	27. 24.	19. 17.
18 • 00	239.	55 •	41 •	34.	32.	49 -	34.	22.	13.
18-17 18-33	186. 101.	41 · 23 ·	28.	24.	23.	38+	Ē7.	17.	12.
16.50	29.	13.	18. 7.	17. 9.	12. 7.	24. 12.	18. B.	14.	8. 5.
16.67	5.	0 •	2.	1.	1 +	1.	1.	1.	1.
18.83 19.00	0.	0.	0.	3.	0.	1 •	0.	0.	0.
. 7 100	٥.	0.	0 •	. 0.	0.	G +	0.	6.	0.

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DATE	03 SEP	1974	LOCATIO	N: 6571	l OA				•
TIME	DN	TH	THI	THR	TH3	SH	\$H1	5 X 8	5H3
5 - 83	٥.	0.	Q٠	Q.	٥٠	٥.	Ç.	0.	ġ.
6-00 6-17	3. 3.	0 • 3 •	0 • 4 •	0. 3.	0 • 3 •	0. 5.	Qr.	٥٠	Ō.
6.33	5.	10.	5.	10.	7.	16.	3. 8.	2. 7.	3 - 6 •
6 - 50	35.	20.	16.	15.	10.	24.	16.	14.	8.
6 57 6 83	17. 206.	33 · 1	' 84. 45.	22. 41.	17, 32.	35. 50.	25.	81.	15.
7.00	225.	88 •	65.	58.	48.	71.	34. 45.	87. 37.	20. 29.
7-17	280+	116.	54+	74.	62 •	77.	53 -	48.	38 •
7 • 33 7 • 50	42 • 78 • •	101.	57 • 70 •	47. 57.	46-	76+	52 •	.42 •	89.
. 7 .67	6.	87 .	58.	A6.	57• 50•	92. 97.	61 • 62 •	48. 45.	34. 36.
7 - 83	365+	220.	158.	135.	113.	116.	74.	57•	43 •
8.00 8.17	11.	110. 155.	76 • 105 •	60 • 54 •	59. 83.	117.	76. 103.	68 •	47.
8.33	9.	181 .	129.	108.	97.	155. 182. 822.	126.	54. 105.	65 •
8.50	6+	228.	160.	131 -			158.	132.	104-
8+67 8+83	81 • 566 •	199. 458.	134. 320.	106. 267.	101.	178*	121. 109.	97 • 82 •	74 -
9.00	614.	471 .	332.	278		170.		67+	61 • 47 •
9-17	616.	493 •	350 •	292.	256•	1685	96.	66.	45.
9+33 9+50	644. 649.	528. 549.	374. 390.	314. 327.	275. 286.	173 -	97. 101.	67 • 67 •	46 •
9.67	683 •	590	418.	349	309.	178 • 183 •	103.	67.	45. 46.
9 • 63	693 •	611.	434+	364 -	321 •	193.	105.	65.	47.
10.00 10.17	702 • 71.4 •	635 • 659 •	449. 467.	375. 393.	332. 347.	196 • 202 •	107. 114.	69 • 70 •	48.
10.33	723.	685 •	484 •	407 •		203.	113.	70.	47. 48.
10.50	732.	700 -	497.	416.		210.	116.	68.	. 47.
10 •67 10 •83	745. 748.	782 • 743 •	509. 525.	428• 443•	381. 392.	210. 214.	118. 121.	69 • 70 • .	47.
11.00	755.	759	536 •	452	402.	216.	123.	71.	48 . 48 .
11.17	758•	773%	547 •	461 •	410,	219. 223.	186.	73 •	49.
11.33 11.50	761 • 753 •	784 • 793 •	555 • 561 •	466 • 473 •	420.	883.	129. 138.	73. 77.	51 • 52 •
11-67	754	803	566.	477 .	424	235.	139.	79.	54 •
11.83	742.	803 -	568•	480 -	426.	237.	143+	61 -	56.
12.00 12.17	736 • 720 :	607 - 821 •	573 • 580 •	483. 490.	426. 434.	249. 270.	153. 168.	87. 101.	59• 72•
12 -33	722.	837	593.	500		281 •	179.	109	78
12.50	728.	827 •	587•	497 •	439.	261 •	166.	99.	71 .
12.67 12.83	726. 729.	632 • 602 •	588 • 568 •	496 • 479 •	438. 423.	270 · 239 ·	174.	103. 87.	75 • 60 •
13.00	739.	797 •	565.	478	423.	236.	159.	83 -	57.
13 • 17 13 • 33	754.	795•	564 •	473 -		232.	155.	79.	55.
13.50	761 • 760 •	793• 779•	563 • 554 •	471 • 466 •		231 • 223 •	153 • 155 •	76. 73.	53 • 50 •
13 - 67	768+	772•	549.	463 +		223.	156.	73 .	50 .
13 • 83 14 • 00	768. 765.	756 • 742 •	537.	453 •		224.	161.	70 •	48.
14-17	747 •	714.	526 • 508 •	442. 427.	392. 379.	223 • 221 •	162 ·	70 ·	49. 49.
14.33	751 .	702 •	497.	420 .	370.	225.	171 -	67.	48
14.50 14.67	741 • 746 •	675 • 663 •	481 -	406.	358•	222.	168.	66.	46 -
14.83	724.	632 •	471. 448.	395. 377.	351. 334.	223 · ·	173. 176.	64. 64.	44. 45.
15.00	721.	611-	495+	367.	324.	227.	179.	65•	46 •
15 • 17 15 • 33	718. 715.	586 • 555 •	417. 397.	350. 335.	309. 295.	208.	176 • 165 •	51. 60.	32
15.50	702	530	378.	319	281.	228.	185 •	60 +	41. 43.
15.67	681 •	498+	355•	300 •	265.	232.	189.	61 .	43 .
15 - 83 16 - 00	669. 658.	468. 444.	333. 317.	201. 267.	246 • 235 •	231 • 231 •	187. 189.	59. 61.	43 • 42 •
16-17	635.	411.	294.	247.	217.	228.	186	60.	42
16.33	621.	388.	278.	235.	297.	233.	190 •	64 •	45 +
16.50 16.67	595 • 540 •	365. 334.	261. 238.	201 201	192. 174.	236. 225.	189.	69. 73.	50 • 55 •
16.83	155.	159.	111.	90 •	85	131 -	96	60 +	44 •
17.00	155.	149.	105	86+	76.	116.	87.	53 •	40 •
17.17 17.33	207. 157.	155. 133.	109. 95.	91. 79.	80 • 71 •	126. 118.	93• 86•	55. 57.	42 • 44 •
17.50	31.	88 •	63 •	51 .	45.	85 -	61 •	49.	37.
17.67	0.	47-	33.	- 68	58.	44.	32.	25.	20.
17.83 12.00	0 • 0 •	36. 25.	84. 19.	22. 15.	16. 13.	34. 25.	22 <u>-</u> 16-	20. 15.	14. 11.
18-17	0.	12.	7.	6.	4.	8.	8.	6.	3
16.33	0 -	٥.	0.	0.	0 •	Ö٠	0 -	0.	ō •

HOURLY AVERAGE FLUX

Headings correspond to flux data tables.

. 1		10N: 85		•			•			
*	TIME	DN	TH	THI	THE	THO	ŚН	SHI	SHR	SH3
•	5 (00)	•) •	0.	ú.	a) .	0.	1) •	0.	0.	ı) •
•	6.00	173.	33 •	80.	₽\$ •	17.	14.	К.	5.	5.
	7.00	677 •	gash .	161.	1.19.	119.	49.	સમ	20.	17.
• • · · •	8.00	798 •	430	304	256.	227.	60 • 66 •	35. 38.	25•\ 28•	20. 23.
	9.00 10.00	960 •	618. 766.	435. 539.	371 • 461 •	328. 408.	66.	39.	28.	21.
•	11.00	929	869	611.	583	463	65.	37.	86.	8Ò .
		933	910	639.	549	465	68.	40 •	29.	22.
•	13.00	936	888	485.	537.	174.	44.	40.	IA.	15.
	14.00	907.	808 *	565 •	485.	428.	76.	47.	33.	25•
· ·	15.00	570.	472 .	324.	.267.	889.	80 •	66.	46.	30 •
	15.00	374 •	310	550	188.	166+	117.	87.	59+	47.
	17.00	624.	252.	1817	156.	136.	94.	94	39.	31.
	18.00	453 - 28 -	72. 2.	55. 3.	47.	40 • 2 •	44 - 5 -	41 · 3 ·	14.	8.
•	19.00 TOTAL	9159	5651	4586.		3522	847.	603	371.	289.
•	IVIAL	,,,,,		-101.71	4,,0,,0	, 44664	,			
•		ION: 85 11 AUG			. • .		•		٠	
									***	***
	TIME 5.00	DN 0.	TH D.	TH1 0.	TH2	TH3	SH.	SHI	SHS	5H3
•	5.00	176 -	32.	23.	80 •	0. 17.	12.	0 . 7 •	٠.	0.
	7.00	683	224.	159.	137.	117.	48.	86.	5• 19•	4. 16.
	8.00	812.	430	303	258.	556.	54.	89.	21.	16.
•	9.00	875 .	619.	435.	373 -	328.	62	34.	24.	19.
•	10.00	902 •	770 •	541.	464.	409+	72.	41 -	29.	22.
•	11.00	922.	866.	609.	523•	462 •	73.	12.	28.	22.
	18.00	926•	912.	641 •	551.	486.	83 •	50 +	33.	26.
	13.00	910 •	875	615.	529.	466.	84.	54 •	33.	26.
	14.00	876 •	800 •	564.	485.	425.	116.	88.	49.	39+
•	15-00	848.	644	455+	391	344.	108.	107.	39.	31.
	16.00	746.	451	321		243 -	130.	147.	41 •	33.
	17.00	591 •	234	157.	145.	126.	118+	121.	33.	26-
	19.00	197. 21.	46.	35. 2.	30.	27. 2.	46 •	33.	16.	13.
	TOTAL	9484	6904	4870	4185	3679	5. 1042.	3. 780.	372.	2. 295.
					-1.5 17.57 4	0.7174	1012.	,,,,,	312.	673.
				_						
		10N: 85 DUA 31		- ,			:			
	DATE	IE AUG	1974	TXI	ŤH2	тиз	•	SHI	\$xi2	SH3
•	DATE	1& AUG DN	1974 TH	THI	ŤH2	тнз	SH	SH1	SH2 0 •	SH3
• • • • • • • • • • • • • • • • • • • •	DATE: TIME 5.00	IE AUG DN O•	1974 TH . 0•	0.	0.	0.	SH 0•	0.	0.	0.
•	TIME 5.00 6.00	DUA 31 00 00	1974 TH 0. 29.	0· 21·	0. 18.	0· 15·	5H 0• 12•	0. 6.	0 • 4 •	0 • 3 •
•	TIME 5.00 6.00 7.00	12 AUG DN 0. 173. 688.	1974 TH . 0. 29. 824.	21. 160.	0. 18. 138.	0. 15. 118.	5H 0. 12. 57.	0.	0.	0.
•	TIME 5.00 6.00 7.00 8.00	DN 0. 173. 686. 815.	1974 TH 0. 29.	0· 21·	0. 18.	0· 15·	5H 0• 12•	0. 6. 29.	0 • 4 • 19 •	0 • 3 • 16 •
	TIME 5.00 6.00 7.00	12 AUG DN 0. 173. 688.	1974 TH 0. 29. 224. 422.	0, 21, 160, 298,	0. 18. 138. 255.	0. 15. 118. 223.	5H 0. 12. 57. 70.	0. 6. 29. 32.	0. 4. 19. 21.	0. 3. 16. 17.
•	TIME 5.00 6.00 7.00 8.00 9.00 10.00	DN 0. 173. 688. 815. 873. 897.	1974 TH 0. 29. 224. 422. 616. 760. 658.	0. 21. 160. 298. 433. 531. 600.	0. 18. 138. 255. 373. 458.	0. 15. 118. 223. 328. 406. 459.	SH 0. 12. 57. 70. 94. 101.	0. 6. 29. 32. 45. 52.	0. 4. 19. 21. 31. 33.	0. 3. 16. 17. 26. 26.
	DATE: 5:00 6:00 7:00 8:00 9:00 10:00 11:00	DN 0. 173. 688. 815. 873. 897. 907.	TH 0. 29. 224. 422. 616. 760. 656. 900.	0. 21. 160. 298. 433. 531. 600. 629.	0. 18. 138. 255. 373. 458. 518.	0. 15. 118. 223. 328. 406. 459.	SH 0. 12. 57. 70. 94. 101. 114.	0. 6. 29. 32. 45. 52. 55. 71.	0. 4. 19. 21. 31. 33. 38.	0. 3. 16. 17. 26. 26. 29.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00	DN 0.173.688.815.873.897.922.907.	TH 0. 29. 824. 422. 616. 760. 656. 900. E67.	0. 21. 160. 298. 433. 531. 600. 629.	0. 18. 138. 255. 373. 458. 518. 543.	0. 15. 118. 223. 328. 406. 459. 481.	SH 0. 12. 57. 70. 94. 101. 114. 107.	0. 6. 29. 32. 45. 52. 55. 71.	0. 4. 19. 21. 31. 33. 38. 37.	0. 3. 16. 17. 26. 26. 29. 28.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00	DN 0. 173. 688. 815. 873. 897. 902. 907. 884.	1974 TH . 0. 29. 224. 422. 616. 760. 656. 900. E67. 773.	0. 21. 160. 298. 433. 531. 600. 629. 607.	0. 18. 138. 255. 373. 458. 518. 543. 524.	0. 15. 118. 223. 328. 406. 459. 481. 465.	5H 0. 12. 57. 70. 94. 101. 114. 107. 120.	0. 6. 29. 32. 45. 52. 65. 71. 97.	0. 4. 19. 21. 31. 33. 38. 37. 40.	0. 3. 16. 17. 26. 26. 29. 28. 30.
•	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00	DN 0. 173. 688. 815. 873. 897. 907. 922. 907. 884. 857.	1974 TH . 0. 29. 824. 422. 616. 760. 656. 900. 567. 773. 633.	0. 21. 160. 298. 433. 531. 600. 629. 607. 542.	0. 18. 138. 255. 373. 458. 518. 543. 524. 467. 384.	0. 15. 118. 223. 326. 406. 459. 481. 465. 413.	5H 0. 12. 57. 70. 94. 101. 114. 107. 120. 140.	0. 6. 29. 32. 45. 52. 55. 71. 97. 142.	0. 4. 19. 21. 31. 33. 38. 37. 40.	0. 3. 16. 17. 26. 29. 28. 30. 30.
•	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00	DN 0. 173. 688. 815. 873. 897. 907. 922. 907. 884. 857.	1974 TH 0. 29. 224. 422. 6160. 656. 900. 667. 773. 633. 449.	0. 21. 160. 298. 433. 531. 600. 629. 607. 542. 445.	0. 18. 138. 255. 373. 458. 518. 543. 524. 467. 384. 274.	0. 15. 118. 223. 328. 406. 459. 481. 465. 413. 340. 242.	5H 0. 12. 57. 70. 94. 101. 114. 107. 120. 140.	0. 6. 29. 32. 45. 52. 55. 71. 97. 142. 204. 221.	0. 4. 19. 21. 33. 38. 37. 40. 41.	0. 3. 16. 17. 26. 26. 29. 28. 30. 31.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00	DN 0. 173. 668. 815. 873. 897. 907. 922. 707. 884. 857. 812. 697.	1974 TH 0. 29. 224. 422. 616. 760. 858. 900. E67. 773. 449. 246.	0. 21. 160. 298. 433. 531. 600. 629. 607. 542. 445. 317.	0. 18. 138. 255. 373. 452. 518. 543. 524. 467. 274. 151.	0. 15. 118. 223. 328. 406. 459. 481. 465. 413. 340. 242.	SH 0. 12. 57. 70. 94. 101. 114. 107. 120. 140. 178. 208.	0. 6. 29. 32. 45. 52. 65. 71. 97. 142. 201. 152.	0. 4. 19. 21. 33. 38. 37. 40. 41. 35. 29.	0. 3. 16. 17. 26. 29. 28. 30. 31. 37. 20.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00	DN 0. 173. 688. 815. 873. 897. 907. 922. 907. 884. 857. 812. 697.	1974 TH 0. 29. 224. 422. 616. 760. 858. 900. 867. 773. 633. 449. 246.	0. 21. 160. 298. 433. 531. 600. 629. 607. 542. 445. 317. 174. 49.	0. 18. 138. 255. 452. 518. 543. 524. 467. 384. 151. 45.	0. 15. 118. 223. 328. 406. 459. 465. 413. 340. 242. 133.	SH 0. 12. 57. 70. 94. 101. 114. 120. 140. 178. 208.	0. 6. 29. 38. 45. 52. 65. 71. 97. 142. 204. 221. 152.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 29. 18.	0. 3. 16. 26. 26. 29. 28. 30. 31. 87. 20.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00	DN 0. 173. 668. 815. 873. 897. 907. 922. 707. 884. 857. 812. 697.	1974 TH 0. 29. 224. 422. 616. 760. 858. 900. E67. 773. 449. 246.	0. 21. 160. 298. 433. 531. 600. 629. 607. 542. 445. 317.	0. 18. 138. 255. 373. 452. 518. 543. 524. 467. 274. 151.	0. 15. 118. 223. 328. 406. 459. 481. 465. 413. 340. 242.	SH 0. 12. 57. 70. 94. 101. 114. 107. 120. 140. 178. 208.	0. 6. 29. 32. 45. 52. 65. 71. 97. 142. 201. 152.	0. 4. 19. 21. 33. 38. 37. 40. 41. 35. 29.	0. 3. 16. 17. 26. 29. 28. 30. 31. 37. 20.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00	DN 0. 173. 686. 815. 877. 907. 922. 907. 884. 857. 812. 697. 459. 25.	1974 TH 0. 29. 224. 422. 616. 760. 658. 900. 573. 449. 246. 70. 2. 6550.	0. 21. 160. 298. 433. 531. 600. 627. 542. 445. 317. 174.	0. 18. 138. 255. 373. 458. 518. 543. 524. 467. 384. 274. 151.	0. 15. 118. 223. 328. 406. 459. 465. 413. 340. 242. 133. 39.	5H 0. 12. 57. 70. 94. 101. 114. 107. 120. 140. 178. 208. 170. 58.	0. 6. 29. 45. 52. 65. 71. 97. 142. 204. 221. 152. 49.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 35. 29.	0. 3. 16. 26. 26. 29. 28. 30. 31. 27. 20.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00	DN 0.173.686.815.873.997.922.997.8844.857.812.699.35.9915.	1974 TH 0. 29. 224. 422. 616. 760. 658. 900. 573. 449. 246. 70. 2. 6550.	0. 21. 160. 298. 433. 531. 600. 627. 542. 445. 317. 174.	0. 18. 138. 255. 373. 458. 518. 543. 524. 467. 384. 274. 151.	0. 15. 118. 223. 328. 406. 459. 465. 413. 340. 242. 133. 39.	5H 0. 12. 57. 70. 94. 101. 114. 107. 120. 140. 178. 208. 170. 58.	0. 6. 29. 45. 52. 65. 71. 97. 142. 204. 221. 152. 49.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 35. 29.	0. 3. 16. 26. 26. 29. 28. 30. 31. 27. 20.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 10.00 1	DN 0. 173. 688. 815. 877. 907. 922. 907. 884. 857. 812. 697. 459. 25. 915.	1974 TH 0.29. 224. 422. 6160. 656. 900. 867. 773. 449. 246. 70. 6550.	0. 21. 1698. 433. 531. 600. 629. 607. 542. 445. 317. 174. 49. 10.	0. 18. 138. 255. 373. 458. 518. 543. 564. 467. 384. 151. 45. 2.	0. 15. 118. 223. 326. 406. 451. 465. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 114. 107. 120. 140. 170. 58. 1. 1429.	0. 6. 29. 32. 45. 52. 65. 77. 142. 204. 21. 152. 49. 2.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 41. 29. 18. 29.	0. 3. 16. 26. 26. 28. 30. 30. 31. 20. 12. 12.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 LOCAT DATE:	DN 0.173.688.815.873.907.922.707.884.857.8915.9915.	1974 TH 0. 29. 224. 422. 616. 656. 900. 867. 773. 449. 246. 70. 2. 6550.	0. 21. 1608. 433. 531. 600. 629. 607. 542. 445. 317. 174. 49. 10.	0. 18. 138. 258. 373. 458. 518. 543. 524. 467. 384. 274. 4152.	0. 15. 118. 223. 326. 406. 459. 465. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 114. 107. 120. 140. 170. 58. 1.	0. 6. 29. 32. 45. 52. 65. 77. 142. 204. 152. 49. 2.	0. 4. 19. 21. 31. 33. 36. 37. 40. 41. 29. 18. 29.	0. 3. 16. 26. 26. 28. 30. 30. 31. 20. 12.
	DATE: TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 TOTAL LOCAT DATE: TIME 5.00 6.00 7.00	DN 0.173.688.815.873.907.922.907.8857.857.459.25.9915.	1974 TH	0. 21. 160. 298. 433. 531. 600. 629. 542. 445. 317. 174. 49. 1. 4806.	0. 18. 138. 255. 373. 458. 518. 543. 524. 467. 384. 274. 151. 4152.	0. 15. 118. 223. 328. 406. 459. 481. 465. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 114. 120. 140. 178. 170. 58. 1. 1429.	0. 6. 29. 32. 45. 52. 65. 71. 97. 142. 204. 21. 152. 49. 2. 1167.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 41. 29. 18. 29. 5H2	0. 3. 16. 17. 26. 28. 30. 31. 20. 12. 12. 295.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 TOTAL LOCAT DATE: TIME 5.00 6.00 7.00	DN 0	1974 TH	0. 21. 1608. 433. 531. 6009. 607. 542. 445. 177. 177. 49. 10. 4806.	0. 18. 138. 255. 373. 452. 518. 543. 564. 467. 384. 451. 45. 2. 4152.	0. 15. 118. 223. 328. 406. 451. 465. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 120. 140. 170. 58. 170. 58. 1. 1429.	0. 6. 29. 32. 45. 52. 65. 142. 204. 21. 152. 49. 2. 1167.	0. 4. 19. 21. 31. 33. 36. 40. 41. 41. 29. 18. 29. 18. 29.	0. 3. 16. 26. 28. 30. 30. 31. 20. 12. 12. 295.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 TOTAL LOCAT DATE: TIME 5.00 6.00 7.00 8.00 9.00	DN 0.171.666.456.4594.	1974 TH 0. 29. 224. 422. 616. 760. 658. 900. 573. 449. 20. 650. 7104 TH 0. 318. 318. 316.	0. 21. 1608. 433. 531. 6009. 607. 542. 445. 317. 490. 1. 4806.	0. 18. 138. 255. 373. 452. 518. 543. 547. 384. 274. 151. 45. 20. 132. 132. 135. 135.	0. 15. 118. 223. 328. 406. 459. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 120. 140. 178. 170. 58. 1. 1429. SR 0. 16. 84. 84. 84. 84. 85. 86. 830.	0. 6. 29. 38. 45. 52. 65. 71. 97. 142. 201. 152. 49. 2. 1167.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 35. 29. 18. 29. 5H2	0. 3. 16. 26. 26. 28. 30. 31. 20. 12. 12. 15. 55.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 7.00 6.00 7.00 8.00 9.00 9.00 10.00	DN 0.173.686.815.873.997.922997.8844.857.812.697.459.25.9915.	1974 TH	0. 21. 160. 298. 433. 531. 600. 627. 542. 445. 317. 49. 6. 7. 4806. THI 0. 22. 153. 2187. 528.	0. 18. 138. 255. 373. 458. 518. 524. 467. 384. 274. 151. 4152. 4152.	0. 15. 118. 223. 328. 406. 459. 465. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 114. 107. 120. 170. 58. 170. 58. 1429. SR 0. 16. 84. 150. 236.	0. 6. 29. 38. 45. 52. 65. 71. 97. 142. 204. 21. 152. 49. 2. 1167.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 35. 29. 18. 20. 6. 22. 62. 92.	0. 3. 16. 26. 29. 28. 30. 31. 87. 295. SH3
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 17.00 18.00 17.00 18.00 17.00 18.00 17.00 18.00 17.00 18.00 17.00 18.00 19.00 19.00 19.00 10.00 11.00	DN 0.173.688.815.873.997.922.997.884.857.812.697.459.915.10N: 8513 AUG DN 0.171.666.894.890.990.	1974 TH	0. 21. 1600. 298. 433. 531. 609. 607. 542. 4457. 174. 490. 153. 218. 4174. 22. 218. 4174. 22.	0. 18. 138. 255. 373. 458. 518. 543. 524. 467. 384. 274. 151. 4152. TH2	0. 15. 118. 228. 406. 459. 465. 413. 340. 242. 133. 39. 1. 3663.	SH 0. 12. 57. 70. 94. 101. 120. 140. 120. 170. 58. 170. 58. 1. 1429.	0. 6. 29. 45. 52. 65. 71. 204. 221. 1529. 2. 1167.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 35. 218. 290. 5 H2 6. 22. 42. 43.	0. 3. 16. 26. 29. 29. 30. 31. 87. 295. 5H3 0. 5. 17. 50. 79.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 17.00 18.00 19.00 19.00 10.00 10.00 10.00 11.00 11.00	DN 0.173.686.815.873.897.9027.857.812.459.25.9915.	1974 TH 0. 29. 224. 616. 760. 658. 9007. 773. 649. 20. 6550. 710A TH 0. 318. 318. 576. 679.	0. 21. 1608. 433. 531. 6029. 607. 542. 445. 174. 49. 16. 4806. TH1 02. 153. 218. 617. 549.	0. 18. 138. 255. 273. 458. 518. 547. 384. 467. 384. 151. 4152. 4152. 4152. 4152. 4153. 4154. 4154. 4154. 4155. 4156. 4156. 4156. 4157. 4157. 4157. 4157. 4157. 4158. 4159. 415	0. 15. 118. 223. 328. 406. 451. 465. 413. 340. 133. 39. 1. 3663. TH3	SH 0. 12. 57. 70. 94. 101. 120. 140. 170. 58. 170. 58. 1.429. SH 0. 166. 230. 236. 236. 252.	0. 6. 29. 32. 45. 52. 65. 77. 142. 201. 152. 49. 2. 1167. SHI 0. 83. 83. 141. 100. 126.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 29. 18. 29. 18. 29. 582. 90.	0. 3. 16. 26. 28. 30. 30. 31. 295. SH3 0. 12. 295.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 19.00 17.00 18.00 19.00 10.00 10.00 10.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00	DN 0.171.666.456.477.906.913.406	1974 TH 0. 29. 224. 616. 658. 9007. 773. 6446. 7704 TH 0. 318. 318. 318. 756. 6859.	0. 21. 1608. 433. 531. 6009. 607. 542. 445. 317. 490. 10. 28. 218. 417. 528. 518. 618. 601.	0. 18. 138. 255. 373. 458. 518. 524. 467. 384. 274. 151. 45. 20. 1325. 1359. 450. 510	0. 15. 118. 228. 406. 459. 465. 413. 340. 242. 133. 39. 1. 3663. TH3	SH 0. 12. 57. 70. 94. 101. 1140. 120. 140. 1788. 170. 58. 1. 1429. SH 0. 166. 846. 2366. 2366. 2521. 263.	0. 6. 29. 38. 45. 52. 65. 71. 97. 142. 201. 152. 49. 2. 1167. SHI 0. 83. 141. 100. 125. 125.	0. 4. 19. 21. 31. 33. 38. 37. 40. 41. 35. 18. 29. 18. 29. 41. 41. 41. 41. 41. 41. 41. 41. 41. 41	0. 3. 16. 26. 28. 30. 31. 29. 12. 12. 15. 51. 579. 32. 34.
	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 17.00 18.00 11.00 11.00 11.00 11.00 12.00	12 AUG DN 0.173. 688. 815. 877. 922. 907. 8844. 857. 812. 697. 459. 25. 9915. ION: 85 13 AUG DN 0.171. 666. 4594. 877. 900. 913. 907.	1974 TH 0. 29. 224. 422. 616. 658. 900. 6673. 446. 702. 6650. 71974 TH 0. 31. 218. 3178. 556. 649. 6859. 759.	0. 21. 160. 298. 433. 531. 600. 627. 542. 445. 317. 40. 6. 7. 153. 218. 523. 618. 539. 611. 539.	0. 18. 138. 255. 373. 458. 518. 524. 467. 384. 274. 151. 4152. 4152. 4152. 4152.	0. 15. 118. 223. 328. 406. 459. 465. 413. 340. 242. 133. 39. 1. 3663. TH3 0. 17. 115. 165. 336. 405. 405. 405.	SH 0. 12. 57. 70. 94. 1014. 107. 120. 1478. 208. 170. 58. 16. 84. 1560. 236. 252. 2413. 309.	0. 6. 29. 38. 45. 52. 65. 71. 97. 142. 204. 21. 152. 49. 2. 1167. SHI 0. 8. 33. 83. 141. 100. 126. 126. 283.	0. 4. 19. 21. 33. 38. 37. 40. 41. 35. 18. 2. 390. SH2 6. 22. 42. 42. 44. 44.	0. 3. 16. 26. 29. 28. 30. 31. 87. 12. 12. 29. 31. 29. 31. 29. 31. 31. 31. 31. 31. 31. 31. 31. 31. 31
•	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.90 17.00 18.90 17.00 18.90 17.00 18.00 18.00 17.00 18.00 18.00 19.00 11.00 12.00 13.00 13.00 13.00 13.00 13.00	12 AUG DN 0.173. 688. 815. 8797. 922. 907. 884. 857. 812. 697. 455. 915. ION: 85 1974 TH 0.29. 224. 422. 6160. 658. 900. 673. 446. 702. 6550. 710A TH 0.31. 318. 318. 5766. 6859. 6859.	0. 21. 1600. 298. 433. 531. 609. 607. 542. 4457. 174. 4806. THI 0. 22. 153. 218. 457. 153. 218. 457. 4806.	0. 18. 138. 255. 2573. 4518. 5244. 3674. 3674. 151. 20. 1325. 4152. 4152. 4153. 4154. 4154. 4154. 4155. 4156.	0. 15. 118. 228. 406. 459. 465. 413. 340. 242. 133. 39. 1. 3663. 17. 115. 165. 405. 473. 405. 473.	SH 0. 12. 57. 70. 94. 101. 107. 120. 1408. 170. 58. 1. 1429. SR 0. 156. 236. 251. 263. 254. 269. 354.	0. 6. 29. 38. 45. 55. 71. 142. 201. 152. 42. 1167. SHI 0. 8. 33. 83. 140. 126. 153. 218.	0. 4. 19. 31. 33. 38. 37. 41. 35. 218. 290. SH2. 42. 42. 44. 47.	0. 3. 16. 26. 29. 29. 30. 31. 87. 295. SH3 0. 17. 59. 33. 33. 33. 33. 33.	
•	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 19.00	12 AUG DN 0 . 173	1974 TH 0.29. 224. 422. 6160. 656. 900. 7733. 446. 702. 650. 7104 TH 0.318. 3158. 749. 7549. 7549. 7629. 7629.	0. 21. 1600. 298. 433. 531. 6029. 607. 542. 445. 174. 49. 16. 806. THI 02. 153. 218. 618. 593. 618. 601. 5439.	0. 18. 138. 255. 273. 458. 518. 524. 467. 384. 4151. 4152. 4152. 4152. 4153. 4154. 4154. 4154. 4155. 4156. 4157. 4	0. 15. 118. 223. 328. 406. 481. 465. 413. 340. 242. 133. 39. 1. 3663. TH3 0. 17. 115. 165. 338. 4055. 473. 4055. 473.	SH 0. 12. 57. 70. 94. 101. 120. 140. 120. 140. 170. 58. 170. 58. 170. 58. 156. 230. 256. 261. 263. 256. 261. 263. 356. 261. 263. 356. 261. 263. 356. 356. 261. 263. 356. 356. 261. 263. 356. 356. 356. 356. 356. 356. 356. 3	0. 6. 29. 32. 45. 52. 65. 71. 97. 142. 201. 152. 49. 2. 1167. SHI 0. 83. 83. 141. 106. 126. 218. 219. 219. 219. 219. 219. 219. 219. 219	0. 4. 19. 21. 31. 33. 38. 40. 41. 29. 18. 29. 18. 29. 58. 44. 44. 44. 44. 44. 44.	0. 3. 16. 26. 28. 30. 31. 29. 12. 29. 54. 57. 50. 79. 32. 34. 35. 31.
ORIGINAL PAGE IS	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.90 17.00 18.90 17.00 18.90 17.00 18.00 18.00 17.00 18.00 18.00 19.00 11.00 12.00 13.00 13.00 13.00 13.00 13.00	12 AUG DN 0.173. 688. 815. 8797. 922. 907. 884. 857. 812. 697. 455. 915. ION: 85 1974 TH 0. 29. 224. 616. 658. 9007. 7733. 4460. 2576. 6550. 7104 TH 0. 318. 35766. 6759. 6859. 6859.	0. 21. 1698. 433. 531. 6009. 607. 542. 445. 317. 490. 10. 22. 317. 528. 417. 528. 601. 539. 431.	0. 18. 138. 253. 458. 518. 547. 384. 457. 4152. 4152. 4152. 4152. 4152. 4152. 4153. 4154. 4155. 4156. 4157.	0. 15. 118. 228. 406. 459. 465. 413. 340. 243. 39. 1. 3663. 715. 165. 405. 405. 405. 406. 411. 338. 405. 406.	SH 0. 12. 57. 70. 94. 101. 114. 120. 140. 178. 170. 140. 178. 170. 58. 170. 58. 18. 18. 18. 18. 18. 18. 18. 18. 18. 1	0. 6. 29. 32. 45. 55. 57. 142. 207. 152. 49. 2. 1167. SH1 0. 83. 141. 1253. 210. 218. 218.	0. 4. 19. 21. 33. 38. 37. 41. 39. 18. 29. 18. 29. 18. 29. 41. 41. 42. 42. 42. 44. 45. 48.	0. 3. 16. 26. 28. 30. 31. 29. 31. 29. 31. 29. 31. 32. 33. 34. 33. 31. 32.	
•	TIME 5.00 6.00 7.00 8.00 9.00 10.00 11.00 12.00 13.00 14.00 15.00 16.00 17.00 18.00 17.00 18.00 19.00 11.00	12 AUG DN 173. 688. 8153. 8977. 9227. 8577. 8577. 8577. 8577. 9013. 6977. 9013. 6977. 9013. 6995. 6995. 6995.	1974 TH 0.29. 224. 422. 6160. 656. 900. 7733. 446. 702. 650. 7104 TH 0.318. 3158. 749. 7549. 7549. 7629. 7629.	0. 21. 1600. 298. 433. 531. 6029. 607. 542. 445. 174. 49. 16. 806. THI 02. 153. 218. 618. 593. 618. 601. 5439.	0. 18. 138. 255. 273. 458. 518. 524. 467. 384. 4151. 4152. 4152. 4152. 4153. 4154. 4154. 4154. 4155. 4156. 4157. 4	0. 15. 118. 223. 328. 406. 481. 465. 413. 340. 242. 133. 39. 1. 3663. TH3 0. 17. 115. 165. 338. 4055. 473. 4055. 473.	SH 0. 12. 57. 70. 94. 101. 120. 140. 120. 140. 170. 58. 170. 58. 170. 58. 156. 230. 256. 261. 263. 256. 261. 263. 356. 261. 263. 356. 261. 263. 356. 356. 261. 263. 356. 356. 261. 263. 356. 356. 356. 356. 356. 356. 356. 3	0. 6. 29. 32. 45. 52. 65. 71. 97. 142. 201. 152. 49. 2. 1167. SHI 0. 83. 83. 141. 106. 126. 218. 219. 219. 219. 219. 219. 219. 219. 219	0. 4. 19. 21. 31. 33. 38. 40. 41. 29. 18. 29. 18. 29. 58. 44. 44. 44. 44. 44. 44.	0. 3. 16. 26. 28. 30. 31. 29. 12. 29. 54. 57. 50. 79. 32. 34. 35. 31.

DATE	5 AUG 1	974							
TIME	DN	TH	THI	THE	THO	SH	SHI	SH2	\$H3
5.00	1.	0.	1.	1 -	1 •	1 •	0. 13.	11.	7.
5 (11)	317.	47 •	36+	3:.•	QK.	211 m 42 m	26.	21.	13.
7 (1)()	633.	16.	153	246.	551. 110.	58 •	30 •	24.	17.
h-00	764.	47.	273. 423.	359.	320.	63 •	38.	29.	20.
9.00	823 • 842 •	784.	549.	464 •	410	118.	77.	63.	47.
10.00 11.00	890 •	843 ·	592	504	452.	66.	40 •	30 •	21.
12.00	888	879 •	617.	526 •	392•	61 •	37.	28+	19• 48•
13.00	579.	610 .	410	330 •	889 •	118.	77.	· 63 • '	62 •
14.00	597 •	631 •	4.42	376.	336 •	151 • 157 •	108.	83	64 •
15.00	562 -	537 •	379.	324 • 268 •	291 •	152.	113.	80 •	63 •
16.00	645	ሳ77 •	037. 95.	81.	72•	92.	58 •	58 •	42.
17.00	116.	134 • 0 •	0.	0.	0.	0 •	·o•	0.	0 •
18.00 19.00	0.	0.	ŏ.	Ö•	0.	0	٥.	· •	O+
TOTAL			4327 •	3666•	3184 -	1093.	730 •	564.	423.
LOCAT I	ON1 857	10A 1974	•					•	•
TIME	DN	ŢН	THI	THE	THE	SK 0•	5H1 0•	SH2 0•	\$ #3 • •
5.00	0 •,	0•	0.	0+	0 • 22 •	17.	12.	7.	4.
6.00	299.	37•	.98	24. 123.	108	32 •	20.	14.	B+
4.00	698•	205	144 • 289 •	246.	217.	41 •	25.	17.	11.
B+00	623 ·	411 - 603 •	424 •	362 •	320 •	44.	25.	15.	13 -
9.00	895 • 935 •	760 •	534.	458-	404 .	49.	29+	19.	14. 12.
10.00	960 •	864 *	607 •	522 •	460 •	45+	27.	19. 15.	12.
12.00	962 •	900 •	634.	544	481 •	46+	26. 42.	30 •	B1 •
13.00	943 .	866 •	623.	535	473 •	65 • 52 •	54+	40 ·	29.
14.00	612.	686	483 •	415 •	367 • 334 •	53 .	34-	23 .	16+
15.00	861 +	625 •	441 • 306 •	379 • 263 •	233 •	49.	32.	21 .	14.
16.00	820•	434 • 113 •	76.	67 •	60 -	43.	30 •	80.	13 •
17.00	348• 384•	57	40 •	37.	38•	30 •	23•	15.	10.
18.00	0.	i.	1.	1.	1 .	٤.	1.	1 • 262 •	179.
TOTAL	9553•	6583 •	.4630+	3977•	.3512+	597 •	385•	202-	
LOCAT DATE:	10N: 85	710A 1974	•		٠			£110	SH3
TIKE	DN	TH	THI	TH2	TH3	SH	SHI	5112	3ns
5.00	0.	1.	0+	1.	1 •	1.	1.	٠.	7.
6.00	278.	46+	32.	30 •	27.	24.	17. 29.	11. 20.	15.
7.00	635•	211.	147•	187•	112 • 218 •	46 • 51 •	34 •	25	17.
8∙00	773•	418+	291 •	246 • 358 •	319.	54 •	36.	28.	19.
9.00	846+	601 • 747 •	423 • 526 •	447 •	399.	57 •	39.	30+	20.
10.00 11.00	. 901 •	848+	596	508	452 -	63.	42.	32.	68 •
18.00	901	689 •	625	534 •	475 •		58•	41 -	29.
13.00	883+	891 •	628	536 •	475 •		79•	63 • 49 •	47 • 36 •
14.00	A1~	754.	535 •	456 •			62 • 77 •	63.	48.
15.00	825 •	658•	466+	397•	352 •		54.	42.	32 -
16 400		443 •	315	869. 137.	236. 121.		53 •	44.	35.
17.00		224 • 58 •	160 •		33 •	5 -	• 03	17.	11.
16.00		1	i.		1.			1.	0.
TÓTAL			4785		3632•	668•	596+	464•	340 •
LOCA DATE	B INOITA	5710A G 1974				•	•		
TIME		TH	THI			_	5H1 0•	5H2	5H3 0+
5+00								11.	7.
6 + 0 (21.	13-
7 •00						. 61 •	36.	28•	
9.00				_	316	. 73 •		31 •	25.
10.0				454	402				34 • 64 •
11.0			603						110
12.0	0 626	1008							106.
13.0	0 647								122.
14.0									122.
15+0					- 44 -			164-	87.
16.0							74.	59 •	
17.0					. 22	33			
19.0	-	_	. 0	. 0					
TOTA	=		4760	. 4068	. 3575	. 1777	1168	7001	
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LOCATIONS 65710A

•			10N1 65				٠	•	-		•
	·		23 AUG DN 0. 296. 645. 793. 860. 901. 918. 917. 911. 892. 437. 256. 87. 24. 0.		THI 0. 30. 145. 290. 424. 589. 597. 684. 609. 543. 304. 192. 62.	TH2 87. 128. 245. 248. 502. 502. 461. 164. 54.	TH3 1. 84. 108. 216. 317. 398. 451. 470. 460. 405. 834. 14548.	SH 1. 83. 41. 49. 56. 56. 70. 71. 189. 189. 56.	5H1 1. 13. 83. 85. 27. 36. A1. 44. 66. 90. 40.	SHR 0. 10. 17. 81. 82. 87. 31. 33. 70. 74. 32.	SH3 10. 15. 15. 13. 13. 17. 80. 84. 82. 55. 84. 84.
		TOTAL	7939.		4366•	3719.	3892.	640 •	521 •	412.	296.
			ION: 85 24 AUG					-	• .		• .
		TIME	DN	TH	THI	TH2	тна .	SH	SHL	SH2	SH3
		5.00 6.00	0. 294.	· 41 ·	1 • 89 •	1 • 27 •	0. 23.	20 •	l. 12.	0. 10.	0. 5.
	•	7.00	649	204-	145	123 -	108.	39.	23.	17.	10.
•		8.00	619+	348.	241 -	103	179.	66 •	40.	32.	55.
•		9.00	855. 897.	604 - 749 -	427 • 528 •	361 • 449 •	319. 398.	61 • 57 •	35. 33.	27. 24.	16. 15.
	· · ·	11.00	910	842 •	596	507	449.	62	36.	27.	17.
		12 -00	902.	876 .	619-	588.	468.	76•	44.	38 -	23 -
		13.00	868	861 •	611.	520+	460 •	110 •	69.	54.	38•
	-	14.00 15.00	864 • 840 •	742 • 600 •	526 • 426 •	448 • 363 •	396. 320.	66 • 60 •	38. 34.	28. 25.	17. 16.
		16.00	760	431 •	308•	263 •	231.	77.	48.	37.	26.
	•	17-00	684-	225.	161 •	139.	121.	64 •	40 •	31 •	•83
		18-00	. 315	56 •	40	37	31.	33.	23. 0.	18.	18 -
•		19.00 TOTAL	9369+	0 • 6575 •	0 • 4659 •	1 e- 3968 •	3505	0. 793.	478.	362	241.
		.0	70074	00,00	70271	0,000	00000	,,,,,		••••	
							٠.	•		,	
			10N: 85 25 AUG								
	•		***				v-sig	cu	cut	e uo	5H3-
		TIME	DH	TH	TH1	1H2	7.H3	SH 0•	SHI O.	5 H2	5 1€0-
•	•	5+00 6+00	0 • 269 •	- D -	29.	26.	23.	23.	13.	11,	6.
••		7.00	615	196 •	139.	117.	104.	41.	25•	19.	11.
		6.00	756•	399•	284	238.	210.	54	33.	24.	16. 18.
		9.00	828. 867.	587 • 736 •	415. 520.	350 • 442 •	310 ·	61 • 68 •	37. 49.	27. 31.	13.
•		1:.00	879	829	586 •	498	441.	75 •	45.	35.	24.
		12.00	678.	862 •	609•	519.	459	61 •	50•	39.	27.
		13.00	875	635•	589	503	445. 395.	80 • 74 •	50 ·	39. 35.	27. 25.
		14.00	857 • 81 4 •	739. 592.	524 • 420 •	446 • 357 •	315.	71.	46.		23.
	_	16.00	739.	403 •	286.	244•	215.	64+	45.	30•	21.
		17.00	593+	199 •	148 •	123.	108.	55 •	41.	25.	17. 8.
		18.00	249. 0.	44.	32.	29. • 0	25. 0.	86.	19.	13.	0.
	;· ·	TOTAL	9218.	6461 •	4579.	3894 •	3441 .	772.	493.	360.	242.
•								*			
			1 26 AU		•	-	•			•	
		TIME	DN	TH	THI	SAT	THS	SH	SHI	SH2	5H3
		5-00	0.	0.	0.	1.	1.	1.	.0.	.0.	٥.
	-	€ •00	835 •	37.	28. 139.	25. 117.	930.	21. 43.	14. 27.	10. 21.	5. 12.
	•	7.00 8.00	602 • 760 •	197 • 402 •	284	241	212.	54 ·	34.	56.	16.
		9.00	840 •	593•	420 -	357.	314.	65+	39.	25.	19+
	•	10.00	871 •	737 •	581 •	444.	392 •	71 •	41.	32.	21 +
		11.00 12.00	888• 690•	830 • 663 •	. 588 · 611 ·	502 • 522 •	443 • 460 •	74. 77.	45 • 47 •	34 • 36 •	22 • 24 =
		13.00	890	635	592.	506 •	446.	74	44.	34.	82.
/ TATE TA	A CUEN TO	14.00	869.	741 -	527.	451 •	397.	73 •	45.	33 •	• 33
ONIGINAL P.	WATE TO	15.00	833	593 -	422 •	361 •	317.	65.	39.	29.	19.
OF POOR QU	JALITY	16.00 17.00	762 • 61 4 •	410 • 198 •	292. 142.	251 • 124 •	220 • 108 •	56 • 46 •	33. 28.	25. 21.	15. 14. ~
		18.00	258.	40 4	29.	26.	24.	21+	14.	11.	7.

DATE	30 AUG	1974		·					
TIME	DN	TH	· THI	THR	THS	SH	SHI	5H2	SH3
5 -00	0.	0.	0.		0-	1.	0.	0.	0.
6.00	199.	46 •	33.	31.	82.	34.	22.	16.	15.
7.00	557.	188.	135.	116.	97.	58.	35.	28.	80.
8-00	717.	391.	279	238.	204 -	74 •	46.	35.	25.
.9.00	811.	586•	418	359.	308.	81 ·	49.	37.	26.
10.00	873 •	746.	530 •	456.	394.	64.	50 -	39.	88.
11 -00	890 •	836.	597.	514.	446.		51 •	29.	26.
18.00	890 •	665.		532.	461 -	88 •	51.	36.	27.
13.00	879.	835•	596.	512.	443 .	88.	53 •	41 •	28.
4.00	823 .	733.	524 •	451 • 358 • 242 •	389.	100 -	62 •	48.	33.
5.00	775 - 1	582 •	417	358.	308.	92.	58•	44.	30 •
16.00	696 •	390 .	281	248.	206.	76 -	49.	36.	25.
7.00		161 •	131.	114.	96 •	53 •	35.	26.	17.
B-00		30 •	28.	- 08	15.	20.	14.	12.	8 -
		0.	0.	٥.	o.		٥.	0.	
TOTAL	6815.	6411.	4583 -	3948.	a390 ·	928.	575.	440 •	308.
LOCAT	ION: 85	71.04		٠	•			•	
	31 AUG								
TIME	DN.	TH	THI	SHT	TH3	SH	SHI	SH2	SH3
5+00	0•	0.	0.	0.	0.	0.	٥.	0.	0.
6 - 00	140 •	35.	25.	24.	18.	29.	19.	15.	-11
7.00	505+	196.	140 •	120.	101.	76.	50 •	41	29.
8.00	662 -	384 -	273.	232.	199.	81 .	50.	38.	26.
9.00		575•	410	351 •	302.	95+	56 •	43 .	31.
10.00	ou 9 •	722.	514.	440	361 •	109-	54 .	50 •	35.
11.00	B24.	817.	580 ·	440. 498.	433.	119.	72.	55	38.
12.00		843.	599.	512.	446.	119. 129.	79.	60 +	42 .
13.00	806 •	815.	57 9 •	495.	-4014	1631	75.	58•	40 .
14.00	772.	710.	507	434 •	377.	118.	71.	55.	
15.00	740 •	564.	402.	346.	298.		61.	46.	
16.00	668.	374 •	509.	346. 230.	198.	78+ 1	48.	37.	
17.00	518	176.	150.	110.	92.		37-	27.	18.
18.00		41 •		28.	85.	33.	24.	19.	14.
19.00			0.	0.	0.	0.	0.	0.	0.
COTAL	8215.	6247.	4454	3820.	3298.	1147.	696.		

3820.

3298.

545.

696.

LOCATION: 85710A

13.00 14.00

16.00

17.00

18.00 19.00

TOTAL

Õ

Ü

	ON: 857 Ol SEP								
TIME	DN	TH	THI	SHT	TH3	SH	SHI	5112	5H3
5.00	0.	0 •	0.	0 •	0.	0.	0 •	0.	0.
6 • 00	3 •	23 •	16.	15.	11.	24.	18.	15.	11.
7.00	179.	175 •	125.	107.	91.	129. 174.	56. 115.	75• 99•	60 • 78 •
8-00	162. 512.	251 • 484 •	178. 342.	150 · 287 •	132 •	161.	103	60 •	59.
9.00 10.00	714.	689 •	468.	411.	363	151 •	94 •	72.	50 •
11.00	768	783	554	467.	415-	141 -	85 •	65.	44.
12.00	792 .	188	581 •	490 .	436 •	134.	81 .	61 -	42 •
13.00	795 •	797 •	564 -	477.	424.	131 -	80 •	61 •	42 .
14.00	779.	693 •	491 .	414.	368+	109.	66 •	49+	33 -
15.00	724.	541 •	385	325.	286. 189.	101 •	63 -	46 • 46 •	31. 32.
16.00	605	356 a 155 •	253. 110.	,215• 95•	63 •	99. 64.	66 • 47 •	30.	21.
17.00 18.00	414.	19.	14	14.	11	17.	11.	9.	6.
19.00	0.	ó.	ō.	0.	Ŏ.	0.	٥.	0.	0.
TOTAL	6512.	5787 •	4100	3466 .	3065.	1434.	921.	709.	KIA.
	10N; 65'								
				T180	THS	SH	Siti	SH2	SH3
TIME 5.00	DN 0 •	TH 0.	TH1 0.	SHT • 0	0.	0.	0.	0.	0.
6.00	3.	22	16.	4 5 -	12.	24.	17.	15.	11.
7.00	10.	107.	76 -	65 •	57•	106.	74.	63 •	51 .
8.00	273 .	295 •	209.	174.	154.	170 -	114.	92.	72.
9.00	548.	551 •	392.	331.	294.	174.	141 +	114.	70 •
10.00	334.	530 ·	373 •	313.	283 •	288.	195 •	158	124.
11.00	402+	613.	432	361	326.	278.	185 •	149	115.
12.00	733	903 •	641+	541 -	480.	265.	175.	138.	105+
13.00 14.00	458. 550.	664 • 631 •	466 • 449 •	390. 380.	349. 341.	226. 223.	190 • 156 •	151.	116. 88.
15.00	695•	538 •	382.	321.	286 •	136.	98•	57•	39.
16.00	599.	354.	252.	213.	187.	128.	101	51.	35.
17.00	417.	152 •	108.	93 •	81 -	85 •	68.	32.	22.
18.00	93 •	22.	16+	14.	12.	21.	15.	10 •	7.
19.00	0+	0 -	0+	0.	0 •	0.	0.	0	0.
TOTAL	5113.	5384	3813.	3210.	2861	2185.	1528.	1144.	853 •
	ION: 85							١	
***	70.11	тн	THI	TH2	тнз	SH	SRI	SH2	SH3
TIME 5.00	DN O+	1H	0.	0.	0.	0 •	0.	0.	0.
6.00	45	21.	16.	15.	12.	22.	14.	12.	9.
7.00	168	116.	82 •	69.	53 •	88•	58•	46.	34.
8.00	115.	221 •	154.	126.	i15.	173.	116-	94+	73 •
9.00	650•	540 •	383 -	320 +	282.	177.	99.	67.	46.
10.00	727	691 •	488+	410	363 -	207	115.	69•	47. 52.
11.00	754	786.	555 •	468•	416.	226.	133	76.	69 •
12.00	727•	821 •	562 •	491 • 467 •	434. 414.	558. 565.	166. 157.	98. 76.	52 •
13.00	758• 746•	782 • 688 •	555• . 488•	407	364.	223	169.	66.	47.
14-00 15-00	701 •	541 •	386•	325.	287	225.	184-	59.	41 -
16.00	534	350 •	250 •	210.	185 .	214.	172 •	64.	46+
17.00	92.	101 •	71.	59.	52 •	87.	63 •	43 •	33 •
18.00	0 +	6.	4.	3 •	3 -	5+	4 •	3.	8•
19-00	0.	0 •	0.	0.	٠.0	• 0	0.	777	0.
TOTAL	6016	5665•	4016+	3377	2989	2139.	1450 +	773 -	552 •
	•				•				

LOCATION: 85710A DATE:

HOURLY RATIOS

Ratios expressed as percentages

S/T: Scattered/Total

Spectral ratios for (T-H) total horizontal and (D-H) direct horizontal flux

- 1/T Flux with OG-1 filter/flux without filter
- 2/T Flux with RG-1 filter/flux without filter
- 3/T Flux with RG-8 filter/flux without filter

				,				
	LOCAT 10	NI 8571	oΑ					
		o aud i		+_U			D-H	
	- 125	5/T	1/1	T-H 8/T	3/T	1/T	2/T	3/T
	TIME	9,	13.	0.	0.	O •	0 •	0.
·	4.11	01.	70.	63.	***	24.	F/3.	5/4 -
	7 - 50	5814 ·	13.	641	53.	75 · 73 ·	67. 63.	56.
	t- +00	14+	70 •	60•	53 •	72.	62 •	55 •
	9.00 10.00	9.	70 •	60 •	53 •	71 .	62 •	55.
·	11.00	7.	70 •	60 •	53 •	71 •	62.	55.
	12.00	7.	70 •	60 4	53 •	71 •	58 •	55 • 54 •
•	13.00	5•	70 •	61	53 •	69· 71·	61 • 62 •	55 •
	10.00	9.	70 • 69 •	60. 57.	53 + 49 +	66	57.	51 • '
•	15.00 16.00	17. 38.	71 -	61 •	54 -	69.	67.	68 •
	17.00	37.	72.	62.	54.	55.	74.	56 •
	18.07	50 ·	75 •	45.	56.	47 •	115.	191.
	19.00	271 •	127.	137 - 60 -	K4+ 53+	70 •	53.	56 •
	TOTAL	13.	,	110	9.7-			
•	LOCATI	ON: 857	10A					
	DATE	11 AUG	1 3/1-4	T-H			D-H	
	TIME	5/T	1 /T	1\2	3/T	1/T	2/T	3/T
	5.00	o.	0 •	0.	0 •	0.	0.	0. 65.
	6.00	39.	72.	.64	53 • 52 •	82. 75.	79. 67.	58
•	7.00	55.	71 • 71 •	61 • 60 •	53 •	73 -	63 -	56 •
	8+00 9+00	13. 10.	70 .	60	53 •	72.	• E3	55 •
	10.00	9.	70 •	60.	53 •	72 .	48.	55 •
•	11.00	8 •	70.	60 •	53 •	72•	62 •	55 · 55 ·
•	18.00	9.	70 •	60 •	53 • . 53 •	71 ·	63.	56 •
	13.00	10.	70 • 71 •	61.	53•	70 •	64.	. 57•
	14.00	15. 17.	71	61.	53.	65 •	66 •	58 •
	16.00	29	71.	61.	54.	54-	73 •	65 • 86 •
	17.00	50 •	71 -	68.	5 :-	40.	96 • 0 •	0.
	18-00		76.	66. 170.	59. 108.	٥.	0.	ō •
	19-00	364 ·	135 ·	61 -	53 •	69.	65.	57•
	TOTAL	, 13.	,,			•		
		10N1 85'						
	DHTE	15 000		T-H			D-H	
	TIME	S/T	1/T	2/T	3/T	1/1	2/T	3/T
	5 • 0 • 0	0 -	0.	0.	0. 52.	0 • 93 •	86.	74.
•	6.00	43 ·	73 · 71 ·	62 •	53.	79.	71 •	61 +
•	7.00 8.00	17.	71.	60 •	53 •	76.	67+	59.
	9.00	15.	70.	61 +	53 =	74.	66.	58. 58.
	10 -00	13.	70 •	60 •	53 + 5/1 •	73. 72.	64 - 65 -	58+
	11.00	13. 12.	70 ·	60 • 60 •	53 •	70 •	64.	57•
	12+00 13+00	14.	70 •	60.	54	68.	65•	58+
	14.00	18.	70 •	60 •	53 •	63 •	67 •	61 - 68 -
	15.00	56.	76 •	61.	54	53. 39.	75. 99.	89.
	16.00	46 •	70 •	61 • 61 •	54 • 54 •	29.	159.	147.
	17.00 18.00	69 • 83 •	71 • 71 •	64.	56	1.	234.	238 -
	19.00	29.	57	81 •	57 •	-38•	11.	86.
	TOTAL	21.	70 •	61.	53.	67•	69.	62 •
-								
•	LOCA	TION: 85	5710A					•
	DATE	1 13 AU	3 1974	r-H			D~H	
	TIME	S/T	1 / T	2/1	3/T	1/1	1/2	3/T
	5.00	0.	0	0.	0.		0.	0.
•	6.00	52.	70 •	63.	55.	91 •	98 •	85 •
	7.00	39.	70 •	61 •	53 ·	90.	88 • 70 •	74 • 72 •
- "	8.00		69.	59. 64.	52. 59.	85; 79.	78.	75.
ORIGINAL PAGE IS	9 •00 10 •00	40 • 31 •	78 • 70 •	60+	54.	68 •	79.	72 •
	10.00	*	70 •	60+	54.	78.	78.	71 -
OF POOR QUALITY	48.00		70 •	60 •	53 •	72.	76 -	49. 72.
	+ 13+00	31.		40 ·	54. 54.	65. 54.	79. 91.	4;; .
	14.11			60 ·	54.	45.	183-	111 -
	15±00 14±00				54.	36.	203 •	189 •
	17.00			61 •	54.	94.	306.	318.
	1 0.00	1 11.	. 69.		57 •	-10+	150+	23. 232.
) 1. 17				7,6 c	70.	į Į⊢	к1 •
	1 0141	41.	. 70.	NU +	,	•	, -	

	10Nr 851 15 AUG						
TIME	S/T	1 / T	T-H 2/T	3/1	LZT	5/T	3/T
5 -1)()	378.	403.	717	798.	0.	0.	0.
6 -00	44.	76 •	58	59.	44.	и.	RI.
7 -0.3	19.	71 •	~1.	54.	74.	64.	59.
8 ±00 9 ±33	1:1.	70 • 70 •	59 • 60 •	53. 51.	7.3 •	61 •	56.
10.00	15.	70	57.	54.	72 ·	60.	54.
11.00	₿•	70 -	60.	54.	71.	61.	55.
12.00	7•	70 •	60 •	45 •	71.	61.	46.
13.00	19.	67•	54•	47.	68•	54.	49.
14.00 15.00	24. 29.	70 • 71 •	60 •	53 · 54 ·	71 • 71 •	62 •	57•
15.00	32.	71 .	60 -	54.	69.	64.	60 •
17.00	69.	71 •	61.	54.	66.	71 .	72.
18-00	0.	0.	0.	٥.	0.	0.	0.
19.00 Total	18.	0 • 70 •	0. 59.	58•	0. 71.	0. 61.	0. 54.
	ION: 857 20 AUG				·		
m 1 wrt	.		T-H			D+H	
T1ME 5.00	5/ 0.	1/T 0.	2/T 0•	3/T 0.	1/T 0.	2/T	3/T
6.00	45.	70	65	56.	70 •	0. 83.	0. 57.
7.00	16.	70 •	60 •	53 •	72.	63 4	58.
R • 00	10.	70 •	60 •	53 •	71 -	68 •	56.
9+00 10+00	7 · 6 ·	70 • 70 •	60 -	53 •	71 •	62•	55 ·
11.00	5.	70	60 •	53 · 、	71 • 71 •	62 •	55 • 55 •
12.00	5.	70 •	60 •	53 •	71	62+	55.
13.00	7•	70 •	60 •	53 .	71	62.	55 •
14.00	18.	70 •	61 •	53 •	71 •	62 •	56 •
15.00 16.00	9. 11.	71 • 71 •	61 •	54 ·	71 +	62.	56 •
17.00	38.	68.	59.	54 • 53 •	71 • 66 •	63. 67.	57. 67.
18.00	52.	70 .	65.	56 •	64.	82.	60.
19.00	147.	43 •	111.	49.	0 •	0.	0.
TOTAL	9.	70 -	60•	53 •	71 -	68•	. 56+
	778 4001 21 AUG		T+H	٠		D-H	
TIME	5/T	171	2/T	3/7	1/T	5/1	3/1
5 •00	91.	22.	64.	86 -	-572	271.	513.
6.00	53•	69•	64+	58.	68.	63 •	88.
7+00 8+00	·82.	70 • 71 •	60 •	53 •	72.	65.	59.
9.00	9.	70	60.	53. 53.	71 • 71 •	61. 61.	56 • 55 •
10.00	ö٠	70	60.	53.	71.	61.	55.
11.00	7.	70	60 •	53.	71 •	61.	55.
18.00	8.	70 •	,60 •	53 •	70.	60.	55.
13.00 14.00	13. 12.	70 • 71 •	60 •	53•	71 - 71 -	61 •	\$5.
15.00	17.	71.	60+	54. 53.	71.	62 • 61 •	56. 56.
16.00	17.	71 •	61.	54+	71 -	62 •	56.
17-00	33.	72.	61 -	54•	71 -	65 •	58.
18.00 19.00	44. 69.	71 • 90	65.	57-	64.	64 •	67.
TOTAL	13.	71 •	101 • 60 •	132 • 54 •	22. 71.	138. 61.	327. 56.
	LON: 657 22 AUG		т-н		•	.	
TIME	5/T	1/1	2/Y	3/T	1/T	₽-H 2/T	3/T
5 •00	0.	55 •	150	59.	-8	72.	36
6.00	45.	73 •	65.	57•	68+	67.	72
7.00 6.00	20.	71 •	60•	53.	72.	68 •	58*
6.00 9.00	15. 12.	71 · 71 ·	60 •	53 • 53 •	73 -	62 •	56.
10.00	18.	71	60.	53 •	73 • 72 •	62 • 62 •	55 • 56 •
1: •00	18.	71 .	60.	53.	72	62.	56 ·
2.00	25.	71 •	61 •	59 4	72 •	62 •	56.
13.60 14.00	30. 37.	70 • 71 •	60+	53 •	72 •	63 •	57.
15.00	44.	71 •	61.	53 • 53 •	73 • 73 •	63 4	58*
16.00	36.	71	62.	53 •	74.	65 • 65 •	57• 57•
17.00	50.	71 .	68.	53.	77.	71 .	62
18.00	85 •	72 •	66+	57.	107.	135.	82.
19+00 TOTAL	362. 26.	66 • 71 •	58. 61.	51 ·	0.	0.	0.
1 0 11187	20.		01+	53 •	73.	6 3 •	57.

	F10N i 85 I 23 AUG						
TIME 5 • 00 6 • 00	5/T 150+ 57+	1/T 35• 74•	T-H 2/T 103• 67•	3.7T 134 • 59 •	1/T 0. 100.	H-Q T\8 • 0 • 101	3/T 0. 78.
7.00	80.	71 •	60.	53 -	75.	65 •	57.
8.00 9.00	12. 9.	71 ·	50 • 60 •	53 • 53 •	73 •	62 •	56.
10.00	7.	γi.	60 •	53.	73 • 78 •	61 • 61 •	56. 55.
11.00	7.	71.	60 •	59.	7Ž.	61 •	55.
12-00	٩.	71 •	60 •	53 •	78 •	61 -	55•
13.00 14.00	9. 9.	71 : 71 •	60 . 60 •	53 • 53 •	78 • 72 •	68.	56 •
15.00	30.	72 .	61.	55 ·	74.	68 • 64 •	56.
16.00	48-	71 •	61 •	54.	73 •	65.	62
17.00 18.00	66 • 90 •	70 •	68.	55	75.	73 •	ėi.
19.00	70.	77.	76 • 0 •	60 .	120.	208.	
TOTAL	14.	71.	60.	53 •	72.	62.	
	10N: 851 24 AUG						
TIME	S/T	1/T	T-H 2/T	3/1	1 47	D-H	
5.00	163.	121	134	71.	1/1	2/T	3/T 0.
6+00	49.	71 .	66.	56	80 •	83 .	87.
7 +00	19.	71 •	60 •	53 •	74 •	64.	60.
8+00 9+00	19. 10.	70 • 71 •	59 • 60 •	52 • 53 •	73• 72•	61 • 62 •	57. 55.
10.00	8.	70 •	60.	53 •	72.	61 •	55 ·
11.00	7.	71 -	60 •	53 •	72.	61 •	55.
12.00 13.00	9. 13.	71 .	60 •	53 •	72.	62•	56.
14.00	9.	71 ·	60 .	50 • 53 •	72• 72•	62 • 62 •	56 • 56 •
15.00	10.	71 •	61.	53 •	73.	63 •	56.
16.00	18.	71 •	61.	54.	73 •	64.	58.
17.00 18.00	29. 60.	72 •	62 • 66 •	54 • 56 •	75 • 77 •	68+	6Ř •
19.00	105	73.	267		0.	84+ 0-	86+ 0• ·
TOTAL	12.	71 •	60•	53 •	72.	62.	56.
LOCAT	ION: 657 25 AUG		T-H				
TIME	S/T	1/1	2/1	3/T	1/1	D-H 2/T	3/1
. 5.00	97.	51 •	92.	69.	460.	2446	
6.00 7.00	56. 21.	72.	65.	57.	89.	89.	95.
8.00	13.	71 • 71 •	60 •	53 • 53 •	74. 73.	64 •	60 •
9.00	10.	71 .	60.		72.	61 •	56 • 56 •
10.00	9.	71 •	60 -	53 •	72.	61 -	55.
11.00 12.00	9. 9.	71. 71.	60 •	53 • 53 •	72.	<u> 61.</u>	55.
13.00	10.	71 .	60.	53 • 53 •	72. 72.	62 •	55. 55.
14.00	10 •	71 -	60•	53	78.	62	56.
15.00 16.00	12. 15.	71. 71.	60+	53 +	72.	62 •	56.
17:00	28.	72.	61.	53. 54.	71 ·	63 • . 68 •	57• 63•
18.00	59+	72 •	66.	58	69.	20	97.
19.00 TOTAL	0. 12.	0. 71.	0 • 60 •	0 • 53 •	0.	0.	0.
			000	33.	72.	62.	56.
	10N: 657 26 AUG		т-н	-	,	D-H	· .
TIME	5/T	1/1	2/1	3/1	1/1	2/1	3/1
5.00	2907	681 •	2359.	1938.	0	0.	0.
6 •00 7 •00	57•	75•	69.	59.	90 •	95•	104-
8.00	22. 14.	71 • 71 •	60 • 60 •	473 • 53 •	73. 72.	63 • 62 •	599.
9+00	11.	71 •	60 •	53 •	78.	63 •	56. 56.
10.00	10.	71 -	60 •	53 •	72.	62 •	56.
11.00 12.00	9• 9•	71 · 71 ·	60 • 60 •	53 •	72 •	68+	56.
13.00	9•	71 .	61 •	53 • 53 •	72. 72.	62 •	56. 56.
14-00	10.	71 .	61.	54.	72.	63 •	56.
15.00	11.	71 •	61 •	53 •	73 •	63 •	56.
16.00 17.00	14. 23.	71 •	61. 63.	54. 55.	73 •	64 .	58.
18+00	53.	72 .	65 •	60+	75 • 76 •	68. 79.	62. 92.
19+00' FOTAL	.0.	0+	0 •	Ü •	0.	0.	0.
e vieth.	11.	71 •	61.	6 6•	72 •	63.	71.

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	ON: 857						
DATEL	30 AUG	1974					
			T-H			D-H	
TIME	S/T	1/T	2/T	3/T	1/1	8/T	3/T
5.00	0 •	0.	0 •	0.	0.		0.
6+00	74•	73•	67•	49.	96•	126.	68 •
7.00	31.	72 •	68 • •		77•	68.	60•
B • 00	19.	71 •	61 •	58.	74.	64 -	57•
9-00	14-	71 -	61 •	53 •	73.	64 •	56•
10.00	11.	71 •	61 •	53 -	72.	63 •	55 •
11.00	10.	71 •	61 •	53 •	72.	63 •	56•
12.00	9.	71.	61.	53 •	72.	63 •	55•
13.00	11.	71 -	61 •	53 •	73 •	63 •	56•
14.00	14.	72.	61 •	53 •	73 •	64.	56.
15.00	16.	72.	62•	53 -	73 -	64•	57+
16.00	19.	72.	68•	53•	74.	65•	58•
17.00	29.	72.	63•	53 •	75•	68.	61.
18.00	69.	73 •	68•	52 •	85.	91.	78.
19.00	0+	0 •	۰.	0.	۰.	0.	0.
TOTAL	14.	71 .	61•	53 •	73 .	64 •	56 •
	10M1 857 31 AUG						
			T-H			D-H	
TIME	S/T	1 / T	2/T	3/T	· 1/T	7\S	3/1
5.00	Ö	0 •	0.	0.	0.	0.	0-
6.00	84 •	72 •	68.	52.	116.	147.	121
7 -00	39.	71 -	61 •	51 .	75 ∘	67 -	60 •
8.00	21.	71 -	61 +	' 52 ·	74.	64.	57•
9.00	16.	71 •	61 •	53 •	74.	64.	57•
10.00	15.	71 •	61 •	53 -	75•	64.	57.
11.00	15.	71 .	61 •	53 •	73 •	63.	57.
12.00	15.	71 •	61.	53•	73•	63•	57•
13.00	15.	71 •	61 •	53 •	73 -	64 •	57•
14.00	17.	71 •	6i.	53 •	74.	64.	57
15.00	16.	71 -	61.	53 •	73•	65.	57+
16.00	£1•	72 •	62 •	53 •	74-	66 •	59•
17.00	32 •	72 •	62.	52 •	74.	69+	62.
16.00	B1 •	75 •	67•	53 •	94.		96 •
19.00	· O »	0.	0.	0.	0.	0.	0.
TOTAL	18.	71 -	61.	53.	74.	64 •	57.

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LUCATION: 85710A
  DATE: 01 SEP 1974
                              T-H
                                                         D-H
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                      1/1
                              2/T
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  LOCATION: 85710A
  DATE: 02 SEP 1974
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5.00
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TOTAL.
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 LOCATION: 85710A
 DATE: 03 SEP 1974
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17.00
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TOTAL
                    71 .
                             60.
                                      53.
                                               73 .
                                                        74.
                                                                69.
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ENERGY VS FLUX

FHI FLO = High and low flux limits in units of watts/m²

EDN = Direct normal energy in units of watt-hrs/m²

ETH = Total horizontal energy in units of watt-hrs/m²

LOCATION: B5710A

DATES	1.0	ΔUG	10.	7 /

DATE: 11 AUG 1974

FHI	FLO	EDN	ETH	•		FHI	FLO	EDN	ETH
1000	980	O •	0.			1000	980	0 •	0 •
980	960 -	0•	0 •	. '	•	980	960	0.	0•
960	940	473 •	0 •		•	960	940	0 •	0 •
940	920	3106 •	O •			940	920 -	1697•	307•
920	900	3865•	,1060 •			980	900	3213 •	912.
900	880	4903 •	8097.			900	880	4546 •	1507 •
660	860	5193 •	2386 •	•		880	850	5125 •	2232.
860	840	5622 •	2669•			ଞ୍ଚଠ	840	6260 •	2514
640	688	6038•	2808•			840	880	6674 •	.2931 •
820	8:D0	6173 •	3349.			820	800	7079 •	3800 •
800	780	6702 •	3481 •	,		800	780	7343 •	3729
780	760	6959•	3869•		•	7.80	760	7473 •	3857 •
750	740	7208•	3994•			760	743	7722.	3981 •
740	720	7208	4238.			740	720	7954	4104 •
720.	700	7328•	4356 •			720	700	8200 •	4342 •
700	5.80	7673 •	4/172 •		,	700	6 <i>8</i> 0	6316 •	4571 •
680	660	8006 •	4582 •			680	660	8488*	4688
660	640	8113 •	4798 •		1	650	640	8535	4791 • .
640	.620	8219.	4903 •			640	520	8535	5002 •
680	³ 600	8321 🗸	5107•			680	600	8839·	5204 •
600	580	8520 ·	5107•			600	5.80	8938•	5204
·580	560	• 0828	5298•		•	5.80	560	8938•	5395
560	540	8704.	5480 •			550	540	9153 •	5576 •
540	530	8704	, 54 <i>8</i> 0 ∙			540	520	9123.	·5576 •
520	500	8790 •	· '5650 •			520	500	920K •	5748
500	<u> </u>	8871 •	5730•			5.00	4(4)	19257.	5828•
480	460	8949•	5 7 30•			480	460	9283.	5428• - J77•`
460	440	8549	5805•			450	440 40	9359+	6048 •
	· 480	9019.	5805 ·			440	430	9359• 9359•	5116
420	400	9019.	5874 -			420	4()!)-	9009•	6309
400	3 80	9019.	5874			400	3 80 - 3 60	9 79.	6309
380	350	9080•	5937 •	-		3.80	340	9359•	6425
350	340	90 8 0 •	5995			360 340	320	9359•	5425 •
340	320	90,80 •	6051 •		<i>*</i>	380	300	9410	6589
320	300	9080.	6103			300	280	9410 •	4529
300	2.80	90 KO •	6151	•		270	260	9410 •	6575 •
280	260	9124.	6196		•	250	240	9410 •	4575
260	240	9124	63.1			240	880.		6615 •
240	880	9124	6321 •	•		380	200	9448	5549 .
220	200	9124	6391 • 6391 •			800	180	9448.	6714 •
800	1.80	9124.	6449 •		:	1.80	160	9448 •	6801 •
180	160	9124				160	140	94/15	6849 .
160	140	9150 -	6496 •			140	120	9448.	6849
140	120	9150 •	6496 • 6550 •		•	120	100	9468.	6868
120	100	9150 •	6607•			100	80	9481.	6868 •
100	60	9150 •	4631 •			80	_	9481 •	6880 •
80	60	9150 •				70		9481 •	6880 •
60		9150 •	6.6.4.600	COUNTAT.	PAGE I	zio zio		9481	6900 •
40		9150 •	909 9M		QUALIT	X I 80		9484 •	6904 •
80	0	9159•	$-$ on $\mathfrak{I}_{\mathcal{L}}$	FOOV	450 T	:,	~		•

LOCATION: 85710A

DATE:	12	AUG	197	14

DATE: 13 AUG 1974

FHI	FLO	EDN	ETH			FHI	FLO	EDN	ETH
1000	980	0 •	O	•		1000	980	0 •	0.
980	960	0 •	0	•		980	960	0.	0 •
950	940	0 •	0	•		940	940	0 •	0.
940	920	463 •	0	•		940	920	0 •	0 •
920.	900	2737•	452	•		920	900	2726.	0 •
900	880	4668+	1342	•		900	880	4059 • 1	1032•
1880	860	5395•	1'925	•	_	880	860	4782 •	1613.
850	840	16528•	2209	•		860	840	5349.	2180 •
840	820	70원1 •	2625	•		840	088	5625 •	2457 •
820	800	7350•	3030	•		880	800	5761 • -	2864.
800	780	7615.	3555	•		የ ሳሳ	780	6687.	3258 •
780	760	8001 •	3548	• .		7.80	760	6687	3642.
760	740	8127.	379 8	•		760	740	6936.	3767 •
, 740	720	8250•	4040	• .		740	720	7180 •	4130 •
ູ7ຂາ	700	8607 •	4393	•	•	720	700	7416.	4247.
700	680	8723 • •	4393	•		700	680	7531%	4475 •
680	660	8946•	4505	•		580	560	7754.	4586.
660	640	8946•	4723	• .		660	. 640	7754.	4803.
640	620	9158•	4828	•		640	520	7954 •	4603 •
680	600.	9359•	5031	•		680	500	2067 .	4905 •
600	580	9359•	5130	•		600	580	88244	5002 •
580	560	9452•	5317	• **	•	580	540°	83 64 +	5002。
560	540	- 9543 •	5317	•		550	5/10	8445 •	5186 •
540	520	9543•	5496	•	-	540	520	とりとう。	5186.
520	500	9630•	5663	•		520	500	8531 •	5359 •
500	480	9712.	5663	•	1	500	480	8611 •	5441 •
480	460	9712.	5819	•		480	450	8611 •	5441 •
460	440	9787 •	5893			450	440	8688	5517
440	420	9787•	5965			440	420	8888 •	5 589•
420	400	9787•	6100			950	400	8688	5658•
400	3 80	9787 •	6100			400	3,80	8688	5854
380	3 50	9787•	6888			· 380	350	8688	5914 •
360	340	9846 •	6222			350	340	8688	5974•
340	320	9845 •	6334	-	•	340	320	8688	6089•
320	300	9846	6385			320	300	8688	6080 •
300.	280	9846 •	6434			300	280	8735 •	6127 •
280	260	9890 •	6523			8.80	860	8735.	6171 •
560	240	9890 •	6523			960	`\$ 4 0	8777 •	6813 •
240	220	9890•	6601			840	880	8777•	6891 •
820	800.	989U •	6635			880	200	8845 •	6361 •
200	180	9890 •	6668			. 800	1.60	8845 .	6425 •
1 80	160	`9890 •	6723			, 180	160	8873 •	6483 •
1 5Q	140	9915.	6749		,	160	. 140	8873 •	5507 •
. 140	120	9915•	6771			140	120	8873	6551 • .
120	100	9915•	6807	•		0SI	100	8873 •	6568 •
100	80	9915	6807	URIGINAL	, PAUL	m3100	80	8873 •	6584·
89	60	9915•	6830	OF POOR	QUALIT	LXI RO	60	8897	6597•
60	40	9915•	6839	•		50	40	`89 13 •	6607 •
40	80	9915•	6844			40	80	8916+	6621 •
80	Ο.	9915•	6850	•		20	0	8917 •	6523 •

DATE:	15	AUG	1	97	4
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DATE: 20 AUG 1974

DHI		HUU .	, . .		• .				
FHI	FLO	EDN .	ETH	•			FLO	EDN	ETH
	980	. 0 •	0 •	•			980	0 •	O•.
1000	960	0.	0 •	•				1607•	0•
1980	940	0'•	.0•	1		960		3031 •	0•
960		0.	0 •	-		940		3956•	0 •
940	920	0•	152 •			920	•	4715.	452 •
980	900	1928•	593 •			900	680	5605 •	1936 •
900	689 860	2947	1760 •	• .		880	860	•••	2515.
880	840	3230 •	2186			860	840		2656 •
860	880 883	3785	2599•			840	320	7027 •	2794
840	ოგნ 800 .	4598	2735.	•	:	820	800	7566 •	3198.
' 820	ິດບ⊍ . ຸ 7 80	5856 •	3001			800	780	7566 •	3330 •
800	760	5898	3388•			780	760	7952 •	3456.
*780	740	6728•	3514 •		• • •	760	740	8075 •	370 °
760	720	6022 •	3514.			740	720	8195 •	3829 •
740	700	6378	3631 •			720	700	8195 •	4067 •
720	680	6722 •	3976 •	1		700	680	8310 •	4297
700	660	6834 •	4088•			680	660	8310 -	4409
680 660	640	6943 •	4302 •			660	640	8526 •	4516
660	680	6943 •	4308 •	•		640	620	8631 •	4727 •
640	600	7046 •	4405 •			620	600	6732 •	4828•
- 620 - 620	580	7143 •	4601 •	•.		600	580		\4927• .
600		7143	4788 •			5 80	560	6927 •	5116.
580	540	7237 •	4788.	*		560	540	9018.	5208• 5296•
560 560	520	7237	4966 •		× .	540	520	9105 •	5362•
540	500	7322.	5050 •			520	500	9105 -	5547 •
520 500	480	7388 •	5133 •	•		500	480	9105	5624• °
480	450	7322•	15289 ·		•	480	460	9261 •	5699•
460	440	7398•	5362 •			. 460	440	9261 • 9261 •	5771 •
440	420	7398.	5434 •			440	420	9261	5840
420	400	7398 •	5501 •			420	400	9261 •	5969 •
400	3 80	7461 •	5501 •			400	3 60	9387•	6030
380	360	7461 •	5563 •			360	360	9387 •	6087•
360	340	7461	5563•			360	340	9387•	6141 •
340		7461	5618.		•	340	. 320	9387 •	6141 •
320			5618.			320	300	9387•	6190 •
300		7511 •	5714 -		•	300	280	9432	6190 •
2.80			5805•			280	269	9473 •	6233•
260			5805 •			260	240	9473 •	6270 •
240						240	£20 200	9473 •	6304
880			5877 •			220	180	9473 •	6335
200			5944 •			200		9502	6392•
1.80			6084 •		•	180			6443 •
160			60.84 •			160	100		6464
140			6128•			140	100		
180			6145 •	RIGINAL E POOR	PAGE	יים גיעבן חרו "שחח	89		
100			61.45 0	RIGINAL OF POOR	OUAL	NA TOO		_	
80)E	, =	ውሀ ድስ	40	_	
60				,	•	40	20		
40						20			
ટા		7654	√ 6176 ±	,					

LOCATION: 85710A

DA1	re: 21	AUG 19	74			DATE	: 55	AUG 197	14
FHI	FLO	EDN	ETH -			EHI	FLO	EDN	ETH
1000	980	0.	0 •			1000	980	. 0.	682•
980	960	0.	0.			980	960	0 •	1004.
960	940	6.	0.			960	940	0.	1791 •
940	920	0.	0.			940	920	0 •	1791 •
920	900	1204.	304 •	1 .		920	900	0 •	2242.
900	880	2697•	1492 •			900	880	0.	2242 •
880	860	4585 •	1928.			880	860	577•	2386•
860	840	5010 •	2353 •	•		860	840	1855 •	2810•
840	820	5699.	2631 •		× 1.	840	683	2689•	3089•
830	800	6236 •	2902•			820	800	3635•	3225•
800	780	6367 •	3166 •			800	780,	4029.	3488•
780	760	5881 •	3296•			780	760	4414.	3742 •
760	740	7256.	3549.			760	740	4665•	3990•
. 740	720	7500 •	3913•			740	720	4906.	4110 -
720	700	7725.	4033•			720	700	5259•	4230•
700	680	7849.	4265 •	•		700	680	5719.	4346
680	660	7849.	4491 .			680	660	5942•	4456 •
660	640	5068 •	4705 •			660	640	6265•	4456 +
640	620	8173.	4705•		•	640	620	6476 •	4563•
620	600	8275 •	5010•			620	600	6579•	4767 .
600	580	8471 .	5207•			600	580	6677 •	4865
580	560	8471 .	5207•			580	560	6771 •	5053 •
560	540	8563 •	5300 •			560	540	6956•	5146.
540	520	8743 •	5477 •			540	520	7043•	5409•
520	500	8743 •	5477 •	-		520	500	7213.	5409 •
500	480	3906•	5641•			500	480	7213•	5491 .
480	460	8985 •	5795•			480	460	7213.	5648.
460	440	8985•	5795 •			460	440	7286 •	5648.
440	420	9055 •	5938•			440	420	7356 •	5718.
420	400	9124.	5938•			420	400	7356•	5787
400	380	9124.	6069•			400	380	7356 •	5917
3 60	360	9124.	6189•		•	380	360	7480 •	5917•
360	340	9239.	6189			360	340	7460 •	5977• 603 0 •
340	320	9239.	6299•			340	320	7480 •	6132•
320	300	9239•	6299•			320	300	7533 •	6229
300	280	9239•	6348•			300	280 260	7533 • 7577 •	6320 •
280	260	9239.	6482 •			280	240	7577 •	6403 •
260	240	9279	6482 •			260	220	7654	6482 •
240	220	9318•	6520			240	200	7654	6517•
220	200	9318•	6557•			220 200	180	7654	6548
500	180	9318.	6589 •		í			7654	6548
1 80	160	9318•	6618			180	160 140	7654	6622•
160		9342	6645			160	120	7654	6622•
140		9364	6688•			140	100	7689	
120		9364 •	6688.			120	80	7717.	6676
100		9364	6719			100	60	7717.	6686 •
80		9364	6742 •			60 60	40	77240	6636
60		9364				40	20	7724°	6714
40		'9368 _*					0	7728.	6721
80	0	9370。	67540			50	U	1100+	01614

DATE:	23	AUG	1	97	4
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DATE: 24 AUG 1974

FHI	FLO	EDN	ETH	•	FHI	FLO	EDN	ETH
1000	980	0.	0.		1000	980	0 •	0 •
980	960	0.	0 •		980	960	0 •	0 •
960	940	0.	0.		960	940	0 •	0•
940	920	767•	0.	•	940	920	0 •	154 •
920	900	3351 •	0.	•	920	900	1816.	154 •
900	880	4540	739•	•	900	880	2855•	450 ·
880	860	5121	1754 •		880	860	4448.	1322.
860	840	5685 •	2179		860	840	5442.	2031 •
840	820	5962	2455		840	820	5995•	2444 •
820	800	6231 •	2727 •		820	600	6399•	2579•
800	780	6362•	3252 •	-	800	780	6532•	2975 •
780	760	6619.	3378		780	760	6914.	3104.
760	740	6870 •	3630•		760	740	7165.	3356•
740	720	6991 •	4118.		740	720	7407.	3723•
720	700	6991	4237•		720	700	7643,	3841 •
700	580	7107•	4353 •		700	680	7757.	4071 • 1
680	660	7218.	4464.		680	660	7981.	4293 -
66Q	640	7218.	4572		660	640	8089•	4400 +
640	620	7323.	4678		640	620	8195•	4506•
620	600	7323	4781 •		620	600	8297•	4711 •
600	580	7423 •	4878	•	600	580	3495.	4907.
580.	560	7423 •	4878 •		580	560	8495.	5001.
560 560	540	7515.	5154 -		560	540	8678•	5186.
540	520	7515.	5243 •		540	520	8678 •	5275 •
520	500	7684	5243 •	~	520	500	8847 •	5360•
500	480	7684	5325 •		500	480	8930 •	5443 •
480	460	7684	5402		480	460	8930•	5602 •
460	440	7758•	5402 •		460	440	9080•	5602 •
440	420	7758•	5473 •		440	420	9080•	5673•
420	400	7758	5473		420	400	9080 •	5741.
400	360	7758.	5539		400	380	91/44	5805•
380	360	7620.	5539•	•	3 80	360	9275•	5867 🕶
360	340	7820	5598	_	360	340	9205.	586 7 •
340	320	7820 •	5653 •	•	340	320	9205•	5978•
320	300	7880	5653 +	,	320	300	9205•	6031 -
300	280	7820.	5701 •		300	280	9308 •	6128.
280	260	7867	5701 -		280	260	9302 •	6173 -
260	240	7867.	5743 .		260	240	9302•	6215.
240	220	7867	5819.		240	220	9302•	6292•
220	200	7867 •	5855•	\ \ \	220	200	9302 •	6326•
200	1 80	7867 •	5886 4		200	1 80	\$ 9333•	6357•
1 80	160	7896 •	5940 .	1	. 180	160	9360•	6385•
160	140	7896•	5966 •		160	140	9360。	6435•
. 40	120	7896 •	5966 •		140	120	9381 •	6457•
120		7896 •	6023 •	·	120	100	9381 •	6494 •
1 70		7912	6054		100	80	9381 •	6509
80		7924	6089•		80	60	9381 •	6532•
60			6132.		60	40	9385.	6557•
40			6154.		40	50	9388•	6557•
20			6162 -		20	O	9389.	6575 •
	9	, , , , ,	·	DAGE	No.			

LOCATION: 85710A

DA	TE: 2	s AUG 1	974		, '	DAT	E: 26	AUG 19'	74
FHI	FLO	EDN	ETH		,	FHI	FLO	EDN	ETH
1000	980	0.	Q •			1000	980	0 •	0 •
980	960	0 •	0.			980	960	0 •	0 •
960	940	0.	0.	•		960	940	0 •	0•
940	920	ō.	9.			940	920	0 •	0•
920	900	0.	0.			920	900	0 •	0 •
900	880	588•	6 •			900	880	2668•	0 •
880	860	3787.	576 •	•		880	860	4407•	720•
860	840	4636 •	1569 -			860	840	4976 •	1572 •
840	820	5327 •	1986 -			840	083	5809•	1988•
820	800	5732.	2392 •			820	800	6213•	2528•
800	780	6128.	2767			800	780	6608+	2660•
7 80	760	6642 •	3043 •			7 80	760	6865 •	3046•
760	740	6893 •	3294 •			760	740	7240 •	3297•
740	720	7137.	3537•		*	740	720	7484。	3541•
720	700	7492 .	3773 •	1		720	700	7719.	37 77 •
700	6 50	7607.	3887.			700	680	7833•	4006 •
680	660	7829.	4001 •			680	660	7945 •	4227•
660	640	7829.	4220 •			660	640	8054•	4227.
640	620	8042.	4430 •			640	680	8265 •	4439.
620	600	8244.	4633 •			620	600	8265 • j	4641 •
600	580	8343。	4633 •			600	5 80	8463 •	4835•
580	560	E437 ·	4825.			5 60	560	8557•	4835•
560	540	8529.	5007.			560	540	8648•	5018.
540	580	8616.	5007 •			540	520	8648•	5105•
520	500	8700 •	5179.			520	500 .		5192.
500	480	8700 •	5340 •	,		500	480	8618.	5354.
460	460	8779.	5340 •			480	460	8895 •	5354 .
460	440	8854•	5491 •			460	440	8969•	5506 •
440	420	8654 •	5491 •			440	420	8969 •	5576*
420	400	8923•	5630•			420	400	9038•	5716+
400	380	8987•	5759•			400	380	9038•	5730 ·
3 80	360	8987 •	5759•			380	360		5780 •
360	340	8987•	58 75 •			360	340	9100 •	5897•
340	320	9044•	5929•			340	320	9154.	
320	300	9095•	5932 •			320	300	9154.	6004,
300	580	9095•	6029•			300	280	9203 •	6098.
280	260	9095•	6076 •			280	260	9203•	6098•
260	240	9136 -	6158•			260	240		6180 •
240	550	9173 •	6158•			240	550	9241.	6180 •
220	200	9173 •	6228•			850	500	9241 •	6252 •
200	1 60	9173 •	6259 *	1		200	1.80	9274	6312+
180	160	9173 •	6888 •			1 80	160	9274	
160	140	9197.	6338•			160	1.40	9274	
140	120	9197.	6338•			140	120	9274	6361•
120	100	9214.	6377 •			150	100	9291•	6359•
100	80	9214.	6407 •			100	80	9307.	6427•
80	60	9214.	6429.			80	60	9307 •	6448 •
60	40	5514.	6443 × 6452 OF		DACE I	60	+ 40	9307 -	
40	80	9814.	64.52 M	SIGINAL.	TATITY	40	80	9307•	
20	0	9218-	6661 0	RING 7	QUALITY	8 0	O	9311 *	6475.

LOCATION: 85710A

DA	TE: 3	O AUG 1	974	`		DAT	E: 31	AUG 19	74
FHI	FLO	EDN	ETH			FHI	FLO	EDN	ETH
1000	980	0 •	0.		•	1000	980	0 •	0 •
980	960	0 •	0 •			980	960	0 •	0 •
960	940	0.	0.			960	940	0 •	0 •
940	920	0.	0.		1	940	920	0.	.0 •
920	900	0.	0.	1		920	900	′ 0.	0 •
900	880	2666 •	0.	•		900	880	0 •	0 •
880	860	3246.	1012.			880	860	0.	0 •
860	840	3815.	1722 .			860	840	0 • -	
840	820	4367 •	2137.			840	820	827 •	1537.
820	800	4907	2541 •		•	820	800	2851 •	1944 •
800	780	5431 +	2805 •			800	780	3647.	
780	760	5943.	3189.			780	76C	4674 .	2726.
760	740	6193 •	3436 •		•	760	746	5175 •	2851 •
740	720	6558.	3557•			740	720	5541 •	3218.
720	700	6676 •	3676 •			720	700	5897 •	3454 •
ູ 700	680	7022.	3908.			700	680	6129.	3569 •
680	660	7245.	4020.			680	660	6354 •	3794 •
660	640	7462 +	4238.	•		660	640	6680•	4010 •
640	620	7670 .		• ,		640	620	6888•	4116.
620	600	7670 •	4548.		-	620	600	6989.	4320 •
600	580	7868.	4648.			600	580	7089 •	4515.
5 80	560	7962 .	4839.			580	560	7278.	4609 •
560	540	8053 •	4839.		44	560	540	7370 •	4701 .
540	520	8140 •	5018.		•	540	520	7459 •	4790 •
520	500	8225.	5188.			520	500	7543 •	4960 •
500	480	8306 •	`5188•			500	480	7625.	5041 •
480	460	8306•	5347.		-	480	460	7702 •	5120 .
460	440	8306•	5495.			460	440	7777•	5196 •
440	420	8450.	5495,			440	420	7777 •	5339•
420	400	8450 •	5630•			420	400	7846 •	5406•
400	380	8450 •	5630•			400	380	7918.	5472 .
380	360	8512.	5754.		•	380	360	7912.	55 3 3 •
360	340	8512·	5868•			. 360	340	7971 -	5592 •
340	320	8621.	5868•			340	320	7971 -	5702 •
320	300	8621.	5969•			320	300	7971 •	5702 •
3 00	280	8621 •	5969•			300	280	8065•	5799•
280	\$60	8666 •	6058.			280	260	81 i O •	5844 -
260	240	8709.	6058•	1	•	260	240	8110.	- 588 7 •
240	220	870 9 •	6136.			240	550	8110 •	5926•
880	200	8743.	6170 •	,		220	200	8179.	5998•
200	1 80	8743•	6203 •			200	1 80	,8179 •	6030 •
- 1 80	160	8771 ·	6258.			1 80	160	8179.	6060 🔹
160	140	8771 .	6258.	•	·	160	140	8179.	6112 *
1 40	120	8793 •	6303•			140	120	8199.	6154 +
120	100	8793.	6338∻		•	120	100	8199.	6171 -
100	80	8793 -	6353•			100	80	8199.	6185 •
63	60	8605.	6376 •	ı		80	60	\$210·	6209•
60	40	8815.	63 93 📲			60	40	8210.	6227•
40	50	8815.	6405。		II.	40	50	8810.	6241 •
20	0	8815.	6414 .			20	Ô	8215.	6247 •

DATE: 01	SEP	15	974
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DATE: 02 SEP 1974

	51.0	EDM.	ETH	•		FHI	FLO	EDN	ETH
FHI	FLO	EDN			÷ -·	1000	980	. 0.	0 -
1000	980	0.	0•			980	960	. 0.	0•
980	960	0 •	0 •		, .	960	940	0 •	156•
960	940	0 •	0 •			940	920	0•	470 •
940	920	0 •	0•			920	900	O •	623•
920	900	0.	0 •		•	900	830	0 •	772•
900	880	0 •	0•			088	860	0 •	1061 -
880	860	0 •	0.		•	360	840	. 0 •	1343•
860	840	G •	0 •	•		840	° 088	0.	1620 •
840	820	0 •	686 •	•		620	800 .	0 •	1891 •
820	800	267•	1363 •		•	800	780	0 •	1891 •
800	780	2239•	1891 •	•		780	760	255•	1891 •
780	760	2881 •	2275 -		•	760	740	754•	1891 • •
760	740	3635•	2524		• 7	740	720	1483 *	2014.
740	720	3879 •	2768.	,		720	700	2075 •	2014
720	700	4235•	3123.			700	680	2537.	2128.
700	680	4465 •	3353	•	,	680	660	2868*	2241 •
. 680	660	4801 •	3464•			660	640	3194	2456 •
660	640	5019•	3571 •			640	620	3194 •	2668•
640	680	5124.	3783•		•	620	600	3398.	2871 •
620	600	5124.	3986 •			600	580	3694 .	3065 •
600	580	5318•	4182 •			580	560	3790 •	3449 •
580	560	5510•	4275.		. •	560	540	3881 •	3726.
560	540	5693 •	4368.	•		540 ·		3970 •	3501 •
540	520	5693•	4456 •			520	500	4054。	4069 .
520	500	5779。	4540 🕶	• • •		500	450	4136.	4069•
500	480	5779•	4540•			480	460	4216.	41460
480	460	5779	4696 •	,		460	440	4289 •	4220 .
460	440	5930 •	4847 •			440	420	4289.	4220 •
440^{1}	420	5930 •	4547•			420	400	4357.	4355 •
420	400	6135.	4847.			400	380	4421.	4419 .
400	380	6198.	4914•	•		380	360	4603 •	4480 •
3 80	360	6198•	4914.			360	340	4503 •	4480 -
360	340	6255•	4972•			340	320	4658.	4592 .
340	320	6255 •	5034•			380	300	4710.	4747 .
320	300	6255•	5136 •			300	280 \	4760 •	4796 .
300	280	6255 ·	5327.			280		4850 •	4974 •
280	260	6301 •	5327•			260	240	4893	5016 -
260	240	6341 0	5450。			240	230	4970	5091 •
240	550	6341 •	5527•			220	200	4970	5091 •
220	200	6341 .	5562•		•	200	180	5032	5184.
200	180	6374 •	5562 •		1	180	160	5059•	5180.
180	160	6402 •	5649.			160	140	5059	5205.
160	140	6428 *	5649•			140	120	5059	5249.
140	120	6471 •	5692•		•	120		5076	5286 •
100	100	6471 .	5711.	•		100		5076	5330 •
100	80	6471 .	5725·		•			5076 e	5340 *
80	60	6493 •	5736 •	1		60 60		5086 •	5364
60	40	6493 •				40		5099•	5379 •
40		6502 •						5113.	5354
80		6512.	5787.		ACE I	ខ្ ឧ០	U		<u> </u>
2.0	•			Y JAMES	TATIT	XI			
			O.E. O.E.	GINAL P	معدوط لرا				
			,' 						

LOCATION: 85710A

DATE: 03 SEP 1974

1000 980 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	FHI	FLO	EDN	ETH
960 940 0 0 0 0 940 920 920 900 0 0 0 0 900 880 0 0 0 0 0 0 0 0 0	1000	980	0.	0 •
940 920 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	980	960	0 •	0 •
920 900 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	960	940	0 •	9.5
900 880 0 0 0 0 9 880 880 860 0 0 0 0 0 860 840 0 0 0 553 840 820 0 1088 800 780 0 1088 800 780 764 2136 760 740 2263 2636 740 720 3596 2756 720 700 4188 3109 700 680 4531 3223 880 660 4642 3446 660 640 4268 3556 640 620 5177 3767 620 600 580 5481 4167 580 560 5575 4167	940	920	0 •	0 •
880 860 0 • 0 • 860 840 0 • 0 • 840 820 0 • 553 • 820 800 0 • 1088 • 800 780 0 • 1749 • 780 760 764 • 2136 • 760 740 2263 • 2636 • 740 720 3596 • 2756 • 720 700 4188 • 3109 • 700 680 4531 • 3223 • 680 660 4642 • 3446 • 660 640 4968 • 3556 • 640 620 5177 • 3767 • 620 600 5382 • 3971 • 600 580 5481 • 4167 • 580 560 5575 • 4167 •	920	900	0 •	
860 840 0 0 840 820 0 553 820 800 0 1088 800 780 0 1749 780 760 764 2136 760 740 2263 2636 740 720 3596 2756 720 700 4188 3109 700 680 4531 3223 680 660 4642 3446 660 640 4968 3556 640 620 5177 3767 620 600 5382 3971 600 580 5481 4167 580 560 5575 4167	900	880	0 •	O •)
840 820 0 • 553 • 820 800 0 • 1088 • 800 780 0 • 1749 • 780 760 764 • 2136 • 760 740 2263 • 2636 • 740 720 3596 • 2756 • 720 700 4188 • 3109 • 700 680 4531 • 3223 • 680 660 4642 • 3446 • 660 640 4968 • 3556 • 640 620 5177 • 3767 • 620 600 5382 • 3971 • 600 580 5481 • 4167 • 580 560 5575 • 4167 •	880			
820 800 0 • 1088 • 800 780 0 • 1749 • 780 760 764 • 2136 • 760 740 2263 • 2636 • 740 720 3596 • 2756 • 720 700 4188 • 3109 • 700 680 4531 • 3223 • 680 660 4642 • 3446 • 660 640 4968 • 3556 • 640 620 5177 • 3767 • 620 600 5382 • 3971 • 600 580 5481 • 4167 • 580 560 5575 • 4167 •				
800 780 0 • 1749 • 780 760 764 • 2136 • 760 740 2263 • 2636 • 740 720 3596 • 2756 • 720 700 4188 • 3109 • 700 680 4531 • 3223 • 680 660 4642 • 3446 • 660 640 4968 • 3556 • 640 620 5177 • 3767 • 620 600 5382 • 3971 • 600 580 5481 • 4167 • 580 560 5575 • 4167 •				
780 760 764 2136 760 740 2263 2636 2636 740 720 3596 2756 720 700 4188 3109 700 680 4531 3223 680 660 640 4968 3556 640 620 5177 3767 620 600 580 5481 4167 580 560 5575 4167				
760 740 2263 2636 740 720 3596 2756 720 700 4188 3109 700 680 4531 3223 680 660 4642 3446 660 640 4968 3556 640 620 5177 3767 620 600 5382 3971 600 580 5481 4167 580 560 5575 4167				
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